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# **Circum-Troodos Limestone Succession**

# of South and West Cyprus:

# A magnetic fabric and magnetic mineralogical study

by Thomas Hamilton

Submitted as partial fulfillment of the requirements for the degree of

#### **Master of Science**

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#### Abstract

Calcite petrofabrics align easily with weak strains, possibly being the most sensitive classical petrofabric indicator. Thus, calcareous sediments may reveal stress trajectories in neotectonic environments. Calcite aligns by crystal-plastic deformation and pressure solution to produce corresponding alignments in accessory clay minerals and magnetite (possibly fossil-bacterial). Their alignments are rapidly and precisely detected by anisotropy of low field magnetic susceptibility (AMS). These net magnetic fabrics blend diamagnetic contributions from matrix calcite (diamagnetic bulk susceptibility  $\kappa \sim$ -14  $\mu$ SI), accessory clay minerals ( $\kappa = 100$  to 500  $\mu$ SI) and trace magnetite ( $\kappa > 2$  SI). Considering their relative abundances and different anisotropies, their orientation distributions of AMS axes are sensibly interpreted as paleostress trajectories in Neogene and Quaternary strata at the regional and sub-area level (each  $\sim 400 \text{km}^2$  and  $\sim 30 \text{km}^2$ respectively). The AMS axes may be correlated with the orientation of faults, platemotion vectors and seismic solutions. A large sample (1090 specimens from 419 sites) was treated by different statistical approaches ("standardization") to emphasize or suppress the contribution of sub-fabrics with anomalous mean susceptibility. A subsample of 254 specimens from 219 sites, from different sub-areas was also investigated by anisotropy of anhysteretic remanence (AARM), which isolates the orientation distributions of magnetite. AMS and AARM magnetic fabrics are mostly of the L-S kind with the magnetic lineations compatible with gravitational stretching of the sedimentary cover away from the Troodos massif and orthogonal to the strike of principal faults and graben. The L-direction (k<sub>MAX</sub>) shows a smooth variation in orientation, through the subareas, directed radially from the Troodos massif and the S-components of the magnetic

fabrics are inclined gently to the bedding, compatible with vergence toward the Cyprean Arc that lies offshore to the South and South-West of Cyprus.

From the original set of 1090 specimens, two smaller sets of samples were further studied using different magnetic techniques to examine differences in magnetic mineralogy and granulometry in different lithologies and through time.

The first set of 100 specimens was divided into pelagic and non-pelagic sub-sets and microhysteresis showed that these samples contained magnetite in the appropriate size ranges for simply interpretable AMS fabrics ("normal fabrics") and also exhibited possible contributions from titanomagnetite ( $TM_{60}$ ) in the non-pelagic samples.

A sub-set of 55 samples in stratigraphic sequence with approximately known age determinations (54-6 Ma) shows systematic variations in bulk susceptibility ( $\kappa$ ), anhysteretic susceptibility ( $\kappa$ ARM), saturation isothermal remanence (SIRM), and thermal demagnetization unblocking temperatures ( $T_{UB}$ ). Some combinations of these magnetic parameters have demonstrated that  $TM_{60}$  is present in appreciable amounts in the youngest of the Cyprus limestones (due to uplift and early erosion of the Troodos massif), and in some of the oldest rocks (due to distal submarine volcanism). Furthermore, the lack of  $TM_{60}$  in the middle of the sequence and the magnetic granulometry shows that magnetotactic bacteria dominate the chalk units of Cyprus.

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#### **Chapter 1 - Introduction**

Originally, basalts were the first choice of rock types for paleomagnetic studies, but with the advent of equipment like the high sensitivity spinner-magnetometer and SQUID (super-conducting quantum interference device) magnetometer, the equally precise measurement of weakly magnetized rocks like limestones, has been possible. Although limestones have < 0.02% of the remanence intensity of basalts (a common target for paleomagnetists), limestones have many other attributes that make them appealing.

First, calcite petrofabrics are sensitive to weak strains, possibly being the most sensitive classical petrofabric indicator. Thus, calcareous sediments may reveal stress trajectories in neotectonic environments. Calcite aligns by crystal-plastic deformation and by pressure solution that produces corresponding alignments in accessory clay minerals and magnetite (possibly fossil-bacterial). Their alignments are rapidly and precisely detected by anisotropy of low field magnetic susceptibility (AMS) with net magnetic fabrics, which blend diamagnetic contributions from matrix calcite (diamagnetic bulk susceptibility  $\kappa \sim -14 \mu$ SI), accessory clay minerals ( $\kappa = 100$  to 500  $\mu$ SI) and sometimes trace magnetite ( $\kappa > 2$  SI).

Second, limestones are of wide-spread stratigraphic importance accounting for approximately 10% of the sedimentary record exposed on land (Blatt et al., 1980) and limestone sequences may have excellent temporal continuity. Therefore, in places of thick limestone sequences one can take numerous samples and have a continuous set of data covering many millions of years.

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Third, limestones are common in the biostratigraphically documented part of the Geological Time Column, which may be bracketed geochronologically and by different paleontological techniques. Furthermore, the precision of age determination using geochronologically calibrated paleontological techniques is quite refined, for example <1 Ma in the Mesozoic and Cenozoic eras. This attribute makes the correlation of paleomagnetic vectors and paleopoles between sites easier and more significant. It also permits a chronological assessment of rock magnetic properties.

#### 1.1 - The purpose of this study

- The main goal of this study was to examine a large sample of anisotropy of magnetic susceptibility (AMS), and anisotropy of anhyteretic remanent magnetism (AARM) data from post-Palaeogene strata in Cyprus. These should correlate with the orientations of neotectonic structures or events such as faults, rifts, Tertiary uplift, and even recent seismic events. This allows a investigation as to whether AMS/AARM fabric axes are consistent with stress trajectories inferred from those structures and from recent plate motion trajectories. Sampling at two density-levels has the potential to verify the homogeneity of the regional domains and the validity of the regional conclusions. Local sub-areas (I-VI) were structurally homogenous and sampled with as little lithological variation as possible over areas ≤ 30 km<sup>2</sup>. The regional-scale domains (I- V) have an average area of ~ 400 km<sup>2</sup>.
- 2. The second objective of this study was to determine different magnetic contributions of minerals in Cyprus limestones by comparing the magnetic

properties of Cyprus limestones through time. Given the proximity and location of the Troodos ophiolite on Cyprus in relation to the overlying limestones (Fig. 1-1 and Fig. 1-2), it is likely that the ophiolite contributed some clastic material to the limestones in the form of titanomagnetite, titanomagnetite or magnetite.



Figure 1-1. Cyprus from Space. Satellite photo of Cyprus demonstrating lithological and topographical changes. Note the dark ophiolite sequence emerging through the limestone cover. Small white spot in ophiolite sequence is snow on Mt. Olympus.



Figure 1-2. Troodos in snow. Although situated in the Mediterranean, Cyprus weather can fluctuate greatly due to dramatic changes in elevation (0-1951m)over short distances .

#### 1.2 - Background

To understand the topic of magnetic mineralogy and fabrics in Cyprus limestones and their relation to Cyprus tectonism and stratigraphy, there are some necessary background topics that have to be covered: basic limestone magnetic mineralogy, and a cursory theoretical background in magnetics. More detailed examination of specific magnetic methods and procedures will be covered in the later chapters, together with a review of Cyprus tectonics. For the non-paleomagnetist, a glossary of some of the magnetic and tectonic terminology can be found in Appendix 1.

#### 1.2.1 - Background Limestone Magnetic Mineralogy

Limestone primarily consists of calcite with minor clay and trace amounts of numerous other minerals including ferromagnetic minerals. The most common ferromagnetic minerals found in limestone include magnetite, goethite, hematite, maghemite, and Fe-Ti oxides. These ferromagnetic minerals may have various provenances but can be grouped basically into one of six main groups: biogenic, clastic, exhalative (in the broadest sense), extraterrestrial, chemical-authigenic, and some derived from seafloor-metamorphosed basalt. Biogenic sources include (in order of importance): magnetotactic bacteria, dissimilatory iron reducing bacteria, and in rare circumstances chiton teeth. Clastic sources are more varied but are predominantly present as a finegrained wind blown fraction from different continental sources or as inclusions in fluvial clay minerals. Exhalative processes may also contribute a significant fraction of mostly fine-grained material from terrestrial and submarine volcanic sources. Extraterrestrial and chemical authigenic sources are minor and difficult to verify in most instances.

Distinguishing different minerals and phases of magnetic minerals in limestone can be difficult using traditional mineralogical techniques such as optical mineralogy or SEM analysis because of small grain sizes, low abundances, and similar characteristics of some ferromagnetic minerals. The best way to look at magnetic mineralogy is to measure, examine and compare different magnetic properties of different samples. This is possible because every mineral has different magnetic properties and even the magnetic properties of the same mineral may differ due to grain size, shape, or internal stress. Moreover, magnetic properties have a wider range of values than most other physical properties.

#### **1.2.2 - Theoretical Background Magnetics**

All materials have common fundamental magnetic properties due to electrons rotating around their spin axis and also around a nucleus. Materials can be classified as diamagnetic, paramagnetic, or ferromagnetic (*sensu lato*) depending on how they react in the presence of a magnetic field and after subsequent removal of the applied magnetic field (Fig. 1-3).

Diamagnetic materials will acquire a small negatively induced magnetization when in the presence of an applied field, and lose their induced magnetism once the applied field is removed. All substances possess a diamagnetic response but may be masked by their paramagnetic or ferromagnetic properties.

Paramagnetic materials will acquire a small positively induced magnetization in the presence of an applied field, and lose their induced magnetism once the applied field is removed.

Ferromagnetism can be defined in two ways: ferromagnetic senso lato (s.l) and ferromagnetic senso stricto (s.s). Ferromagnetic (s.l) materials will acquire a small to large positively induced magnetization in the presence of an applied field, and retain an amount of their induce magnetism once the applied field is removed. Ferromagnetic (s.l)include ferromagnetic (s.s), antiferromagnetic, and ferrimagnetic materials. Ferromagnetic (s.s) materials will acquire a large positively induced magnetization in the presence of an applied field and retain its induced magnetism once the applied field is removed.



Figure 1-3. Types of Magnetization showing alignments of spin moments schematically. Different responses of (A) diamagnetic, (B) paramagnetic. (C-E) shows hysteresis during cycling through large fields -H to +H, initial slope  $\varkappa$  is the low field susceptibility. (Slope  $\varkappa$ = magnetic susceptibility)

#### Chapter 2 – Magnetic Fabric Studies (AMS & AARM)

#### 2.1 – Anisotropy of Magnetic Susceptibility (AMS)

Magnetic fabric analysis, most commonly using anisotropy of low-field magnetic susceptibility (AMS), is now well established as a non-destructive technique to isolate the mean orientation-distribution of crystals in an anisotropic rock. AMS blends contributions from different minerals that have different magnetic responses, i.e., paramagnetic, diamagnetic or "ferro"-magnetic (Rochette et al., 1992). In turn, the principal AMS axes may proxy for the principal axes of the orientation distribution ellipsoid of crystals (Borradaile, 2001; Henry, 1989), which, in turn, may reveal the finite strain axes in tectonically deformed rock (Borradaile & Henry, 1997; Tarling & Hrouda, 1993). In deformed calcite matrices, interpretation is somewhat complicated by an intrinsic counterintuitive arrangement of crystallographic and AMS axes, a so-called "inverse fabric" (Rochette, 1988), which nevertheless still permits sensible interpretations of their finite strain axes (Ihmlé et al., 1989; de Wall et al., 2000).

However, recent studies show that in neotectonic environments, with imperceptible penetrative strain, AMS axial orientations may be sensibly related to the orientations of joints or faults, for which stress-axes are reliably inferred (Sagnotti, et al.1994, 1998; Mattei et al., 1999; Cifelli et al., 2004). In some instances, AMS axes may correlate with modern seismic solutions and plate movements (Kissel et al., 1986; Mattei et al., 1999; Borradaile & Hamilton, 2004). Thus, AMS may proxy for stress trajectories under limited circumstances.

#### 2.2 - Tectonic Background

This study concentrates on the limestone and marl sedimentary cover to the Cretaceous Troodos ophiolite. Excluded from this discussion are the juxtaposed older allochthonous Mamonia and Kyrenia Terranes, which include exotic formations as old as Triassic and perhaps even Carboniferous (Robertson, 1990) (Fig. 2-1a). The Troodos Terrain exposes an integral ophiolite sequence with mantle harzburgite and lherzolite at the base overlain by layered gabbros and dunite, sheeted dykes, a transitional sheeteddike-to pillowed unit and a thick pillow basalt sequence (Malpas et al., 1990). Supra-Troodos sedimentation commenced in the Maastrichtian (~ 68 Ma) with a pelagic chalk blanket, and forms a relatively continuous sequence to the present (Lord et al., 2000). Northwards subduction stalled in the Eocene, with southward thrusting of the Kyrenia Range. Subduction then retreated southwards to its present location off the south shore of Cyprus in the Miocene, initiating the present stress regime (Fig. 2-1b). Miocene extensional basins, most prominently the Polis graben, formed in response to changing stress trajectories during the retreat of the subduction zone's hinge away from the Troodos microplate. Subduction continued during the Pliocene, until the Eratosthenes Seamount reached the trench in the Pleistocene when serpentitization-driven diapirism continued to uplift the Troodos dome (Robertson, 2000). These events drastically changed the neotectonic regime in the last 5 Ma, which is evident from studies of structure (Robertson et al., 1995), earthquake distribution and fault systems (Arvidsson et al., 1998; Ben-Avraham et al., 1988; Borradaile & Hamilton, 2004; Papazachos & Papaioannou, 1999) and geodetically determined plate motion (Reilinger et al., 1997).

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Figure 2-1 Geology of Cyprus. (a) Major lithological units of Cyprus (Geological Survey Department, Cyprus, 1979). (b) Major Tectonic features of Cyprus (Robertson, 1990; Arvidsson et al, 1998; Borradaile & Hamilton, 2004)

The tectonic events, their principal plate-geometrical consequences and the reasonably inferred principal tensile or compressive stress trajectories are summarized in Table 2-1.

Δαο	Periode	Formations	Tectonic Events	
nge	I CHOUS		Principal Stresses	Troodos Microplate Rotations
0.01	Holocene	Alluvium	Pegia	
0.01	Pliestocene	Terrace Deposits	Polis	
		Fanglomerate		Final $\sim 30^{\circ}$ slow rotation
2.0	Pliocene	Athalassa		(50 Ma - 10 Ma) distant rotation-axis
50		Nicosia	Polis	
5.2	Messinian	Kalavasos		
	ម្ម Tortonian	Koronia	Mesaoria	
	ဗွီ Serravallian	Pakhna		
	E Langhian		Yeresa	·
	Burdigalian	Terra		
23.3	• Oligocene			
35.4	en subsection			
	g Eocene	Lefkara	(Kyrenia)	
56.5	ala	LUINAIA		$\sim 60^{\circ}$ rotation
	A Palaeocene			intra-plate axis
65.0				\$
	Maastrichtia	Moni		
	Campanian	Kannaviou		
		Perapedhi		
88.0	Cre	Troodos Ophiolite		and the second

Table 2-1. The major tectonic events of Cyprus through time and formations.

Previous studies indicated the potential for AMS (anisotropy of low field magnetic susceptibility) to indicate very weak strains and weak orientation distributions of minerals, like those accompanying calcite-crystal plastic mechanisms in neotectonic environments (Borradaile & Jackson, 2004; Borradaile & Henry, 1997; Rochette et al, 1992). AMS shows neotectonic potential in the limestone cover from the Palaeogene Lefkara Formation through the Neogene Pakhna Formation to the localized Pleistocene cover. Without regard to detailed stratigraphic level within the Troodos Cover sequence, Lagroix and Borradaile (2000) showed that the AMS principal axes correspond to kinematic patterns. k <sub>MAX</sub> defines down-slope gravitational stretching away from the Troodos dome and locally into tectonic/depositional basins. In the Polis Rift Valley, AMS and AARM (anisotropy of anhysteretic remanent magnetization) axes correlate with principal stress trajectories inferred from Miocene and younger fault-orientations and from modern seismic fault-plane solutions (Borradaile & Hamilton, 2004; their fig. 6).

#### 2.3 - Neotectonic interpretation of AMS

The presence of consistently oriented AMS axes unrelated to depositional fabrics in young sedimentary rocks, itself argues for some subtle tectonic imprint (e.g., Sagnotti et al., 1994). In such environments, AMS axes may be oriented consistently and simply with respect to faults or joints. These structures have orientations uniquely associated with their co-genetic stress trajectories and thus by induction, the AMS axes may proxy as *stress* trajectories. Of course, AMS axes may proxy for stress trajectories in ancient rocks too, but their recognition requires fortunate circumstances (e.g., Borradaile & Kehlenbeck, 1996). Usually, in ancient or severely deformed rocks, the association of AMS with finite strain axes with earlier tectonic events will mask any young and feeble AMS overprint associated with late stress increments. *Note that this study uses Flinn's L-S scheme (1965) equally to describe tensor magnitude ellipsoid shapes, whether they are for strain, AMS, stress, or mineral ODs (Orientation-Distributions or "petrofabrics").* 

Calcite twinning and other crystal-plastic deformation have long been used in petrofabrics as sensitive indicators of *incremental* strain axes, which are essentially parallel to the causative *palaeostress*-axes. Indeed, the association of calcite petrofabrics, their causative stress axial orientations and magnetic fabrics have been shown in some other studies (Jackson et al., 1989; Borradaile et al., 1989; Owens & Rutter, 1978; Owens & Bamford, 1976). The Neogene and Quaternary limestone and marl that covers the Troodos microplate shows evidence of weak to moderate strain, expressed by calcite twinning and, rarely, a feeble stylolitic cleavage. Calcite, accessory clay and magnetitetraces are aligned and readily detectable in the AMS signal (Lagroix & Borradaile, 2000). These minerals contribute quite differently to AMS and to bulk susceptibility. Calcite is diamagnetic (usually quoted as  $\kappa \sim -14 \mu SI$ ) but it has a large anisotropy and comprises >97% of the rocks' volumes. Its crystal-plastic deformation aligns the paramagnetic accessory clay minerals (100-500  $\mu$ SI,  $\leq$  3% by rock volume) and the scarce traces of magnetite. However, the latter may contribute significantly to AMS due to magnetite's high bulk susceptibility ( $\sim 1.0$  to 5.7 SI) (Hunt et al., 1995); and the grains may align either as overgrowths or inclusions associated with clay grains or as independent grains. Magnetite grains may be of clastic or bacterial origins; their hysteresis properties are

compatible with the latter hypothesis (Borradaile & Hamilton, 2003; Borradaile & Lagroix, 2000). Specific hysteresis data for these rocks will be discussed in later sections.

The specimen's bulk susceptibilities [ $\kappa = \sqrt[3]{(k_{MAX}k_{INT}k_{MIN})}$ ] are a first guide to the mineralogical controls on AMS. These are presented in rather homogenous sub- areas (~40km<sup>2</sup>) (Fig. 2-2a), which justifies the subsequent interpretation of larger sampling schemes in regional domains (~400km<sup>2</sup>) (I-V) (Fig. 2-2b). The positive susceptibility sections of the histograms are scaled logarithmically and, to a first approximation, it appears that the weakly positive  $\kappa$  specimens have susceptibilities with a lognormal distribution, with most sub- areas and regional domains having modal  $\kappa$  in the range +15  $\mu$ SI  $\leq \kappa \leq +35 \mu$ SI. Very low concentrations of accessory clay ( $\leq 1000 \mu$ SI) and trace magnetite (>2.0 SI) suffice to raise the specimens'  $\kappa$  from the level of a pure calcite diamagnetic matrix ( $\sim$  -14 µSI) to the levels of the positive  $\kappa$  specimens shown in Fig.2-2a,b. In the complete absence of magnetite, only 3% by volume of clay would be required to justify the positive  $\kappa$  values. Many specimens are truly diamagnetic and the linear scale for the diamagnetic part of the histogram clarifies the frequency distributions. For calcite,  $\kappa$  is commonly quoted at ~ -14  $\mu$ SI (Voight & Kinoshita, 1907) or -7.5 to -39  $\mu$ SI. (Hunt et al., 1995). Whereas there are fairly modern high precision torque measurements for anisotropy (i.e., k<sub>MAX</sub>-k<sub>MIN</sub>; Hellwege & Hellwege, 1967; Owens & Rutter, 1978) there are apparently no recent high-precision measurements for the bulk value ( $\kappa$ ), which hinders modelling and interpretation of AMS. Values for synthetic calcite would be preferable for modelling work whereas measurements from natural calcite are contaminated by non-diamagnetic impurities. Our instrument has a low-drift environment (<0.05  $\mu$ SI) and is calibrated with MnO<sub>2</sub> (~1654  $\mu$ SI). Due to the small range of



Figure 2-2. Frequency-distribution of bulk magnetic susceptibility ( $\kappa$ ) for (a) sub-areas (each~ 30 km<sup>2</sup>) and (b) regional domains (each~400 km<sup>2</sup>). Data in the shaded box on the left represent diamagnetic specimens and their scale is linear. Data with  $\kappa$ >0 represent paramagnetic specimens and are shown with a logarithmic scale.  $\kappa$  is calculated as the mean of the seven measurements made in 7 different directions during AMS determination.

diamagnetic susceptibilities there may be some slight bin boundary bias in that part of the histogram.

The susceptibility frequency-distribution indicates that paramagnetic limestone is more common and it confirms that the rocks' susceptibilities, whether paramagnetic or diamagnetic are mostly bi-mineralic in origin. Interpreting AMS axes in such rocks necessitates the evaluation of the balance between weak paramagnetism and weak diamagnetism in the same specimens, and between weakly dia/paramagnetic specimens within a sample of several different specimens, for example from a sub-area.

A new plot of fabric anisotropy parameters, introduced by Borradaile & Jackson (2004), simplifies the interpretation in this context. Jelinek's (1981) anisotropy parameters (Pj, T) are usually presented on Cartesian axes. Consequently, for weak degree of anisotropy (low-eccentricity ellipsoids with Pj~ 1.0) the difference between T-values that describe ellipsoid shape is exaggerated. In the extreme case, the sphere (isotropic case, Pj=1.0), which should plot at *one point* on the diagram actually spread along the entire axis from T=+1 (prolate) to T= -1 (oblate). This biases the presentation and interpretation of all low-Pj anisotropies that are essentially near-isotropic, a matter of considerable relevance here where specimens straddle the diamagnetic-paramagnetic boundary. The new polar plot presents Pj radially and T along arcs; thus, all spheres plot uniquely at the origin and the difference in shape between weak anisotropies is not exaggerated. Moreover, the plot facilitates the simultaneous presentation and comparison of positive and diamagnetic susceptibilities (Fig. 2-3).



Figure 2-3. Polar plots (see Borradaile & Jackson, 2004) of four select sub-areas (a-d) and two select regional domains (e-f). Shaded area represents diamagnetic specimens and white area represents paramagnetic specimens. Fabrics are apparent from Jelinek's (1981) Pj (radial) and T (arc) parameters calculated from the principal susceptibilities. Different patterns reflect the degree and type of deformation. (T=shape, Pj=eccentricity)

When working with anisotropies of diamagnetic rocks and weakly paramagnetic rocks it is also important not to overlook some non-trivial issues, which software must be carefully manage:

- Anisotropy is indeterminate for a specimen if some axes have positive susceptibility and others have negative susceptibility (Borradaile, 2003). This occurs in some limestone specimens.
- (2) k<sub>MAX</sub> is obviously the largest absolute value for a paramagnetic material but for a diamagnetic material the most negative value represents the long axis of the magnitude ellipsoid.
- (3) Regardless of the convention for defining the ellipsoid in (2) above, the common diamagnetic minerals, quartz and calcite have the idiosyncrasy that under most metamorphic conditions their c-axes tend to align parallel to the shortening axis (however, see Borradaile & Jackson, 2004). Thus, c-axes are parallel to the most negative susceptibility, which may be perpendicular to the rock's S-fabric. Calcite exhibits a strong prolate diamagnetic anisotropy with (κ<sub>MAX</sub>- κ<sub>MIN</sub>) estimated at 1.39 µSI (Krishnan et al., 1933; Hellwege & Hellwege, 1967, p.143) or 1.172±0.028 µSI (Owens & Rutter, 1978). If we accept the much less certain but commonly quoted bulk susceptibility κ ~ -14 µSI, these precise anisotropy determinations indicate a large anisotropy of ~ 10%.
- (4) Since most deformation mechanisms align calcite with its c-axis (most negative susceptibility) parallel to shortening it produces an "inverse fabric" (Rochette, 1988; Ihmlé, 1989).

Examples of the anisotropies of both local-scale samples (Fig. 2-3a-d) and regional domains (Fig. 2-3e, f) indicate that the anisotropy degree (Pj) is similar for diamagnetic and paramagnetic limestones and that ellipsoid shape tends slightly toward the oblate case (T > 0) for both diamagnetic and paramagnetic specimens. Anisotropies are remarkably similar for the diamagnetic and paramagnetic fields and diamagnetic limestones are only absent in marl Formations in the Omodhos and Lefkara subareas (Fig. 2-3c, d).

#### 2.4 - Interpreting AMS

AMS orientations and magnitudes would reflect the orientation distribution of a monomineralic rock with a unique petrofabric. However, for rocks with multiple minerals with similar contributions to the net susceptibility or with multiple subfabrics some care is required in evaluating the influence of mineral abundances and subfabrics (Borradaile, 1988; Borradaile & Henry, 1997). For rocks of high mean susceptibility ( $\kappa$ ),AMS axes may be controlled by one of two or a few minerals (Borradaile & Mothersill, 1984; Borradaile & Kehlenbeck, 1996; Borradaile & Lagroix, 2001; Henry, 1983; 1990; 1992; Nakamura & Borradaile, 2001). In these limestones however, sub-equal competition from the diamagnetic matrix and paramagnetic clay complicate the issue. To illustrate the argument with hypothetical but not unrealistic values chosen for arithmetic simplicity; disperse a concentration of 5% clay (assume  $\kappa = 266 \ \mu$ SI) in a calcite matrix (assume  $\kappa = -14 \ \mu$ SI). The limestone's net susceptibility is approximately zero and the specimen may also be isotropic. It is for this reason that some AMS data from limestone must be examined carefully because the AMS directions are simply too unstable; their anisotropy

is too low to define stable orientations of principal axes as itemized in the list above (Borradaile & Jackson, 2004). In worse cases, the principal susceptibilities may not all be of the same sign so that the AMS tensor may not be represented by any magnitude ellipsoid.

Although it is now realized that the magnitude ellipsoids of individual specimen tensors have little kinematic significance due to the complex blend of multiple mineralogical responses, specimen magnitudes do affect the calculation of the orientation of the mean-tensor. The mean-tensor's orientation may be strongly deflected toward the orientation of a few large-magnitude specimen tensors. However, high susceptibility specimens need not be considered as outliers in the disparaging statistical sense. They may provide useful information from a subfabric or second population of grains with a different orientation-distribution. That is the case in this study where specimens with larger concentrations of paramagnetic accessory clay minerals may strongly influence the orientation of the mean tensor for a sub-sample. By recalculating the mean tensor using standardized specimen-tensors, the influence of high susceptibility specimens and kinematically distinct subfabrics may be isolated, or emphasized (Borradaile, 2001; 2003). Specimen-tensors are standardized by dividing each of the principal magnitudes for a specimen (k<sub>MAX</sub>, k<sub>INT</sub>, k<sub>MIN</sub>) by κ; this weights all specimens equally, regardless of their bulk susceptibility. Consequently the contribution high- $\kappa$  subfabrics to the orientation-distribution will be subdued in the net-AMS. On the other hand, the meantensor for non-standardized specimens emphasizes the role of such subfabrics (Borradaile, 2001; 2003).

The following comparison of mean-tensors for standardized *versus* nonstandardized specimens in regional-scale and local-scale samples, display different AMS axes that reveal a rapidly changing tectonic regime, especially in the last 5 Ma. Sample mean-tensors for standardized and non-standardized specimens are also compared profitably to previously determined AARM tensors.

#### 2.5 - Processing AMS data from low-ĸ specimens

The tectonic significance of AMS data in limestone having weak susceptibilities depends on a careful assessment of the mineralogical origins of AMS and the effects of specimen-variation within the sample-suite. Jelinek (1978) showed that the orientation distribution (OD) of a suite of tensors ("AMS ellipsoids") must be treated by a special statistical procedure so that the sample's mean tensor retains orthogonal axes, just like individual specimen-tensors. Applying Jelinek statistics permits us to characterize a sample of AMS tensors much more effectively than with density contours, although the latter still have their use (Borradaile, 2001; 2003). The shape and symmetry of the 95% confidence regions around the mean-tensor's principal axes define the orientation-distribution of specimen tensors in the L-S fabric scheme (Flinn, 1965); thus regional suites of AMS ellipsoids define the regional variation from S through L tectonites (Fig. 2-4).

Confidence cones for the mean-tensor's principal axes reflect the shape of the orientation-distribution (OD) ellipsoid for the sample, not of individual tensors. For example, individual prolate ellipsoids scattered with their long axes in a plane define a sample with an orientation-distribution described by an oblate ellipsoid (e.g., Borradaile,

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2003; p.286-287). Thus in AMS studies, if the mean Tj>0 for specimens, it does not necessarily mean that their orientation distribution, described by the mean-tensor is also prolate (Borradaile, 2001).

The sample's mean tensor and its confidence cones may be biased toward the orientation of specimens of anomalous  $\kappa$ . In this study, the anomalous specimen may be a diamagnetic one or a paramagnetic one in a contrasting matrix. The standardization technique described (dividing  $k_{MAX}$ ,  $k_{INT}$ , and  $k_{MIN}$  each by  $\kappa$ , etc.) suppresses this bias. Whereas it may change the orientation of the mean tensor, it may also change the shape of the confidence regions about the mean tensor's axes. Thus one may re-evaluate the OD of the mean tensor as an L>S rather than S>L fabric.



Figure 2-4. Idealized symmetry of confidence cones about the mean orientations of the principal axes of the mean tensor for a petrofabrically homogeneous group of specimens. The shapes of confidence cones for tensor-mean principal axes may be used for other petrofabrically significant axes (as in orientation-distributions of crystals), for finite strain axes and for principal stresses. The shape of the confidence cones may also related to the relative magnitudes of the three principal mean-axes: (a) elongate confidence ellipses in the maximum-intermediate plane define an ellipsoid with oblate symmetry (S>L) whereas (c) elongate confidence ellipses in the plane perpendicular to the maximum axis are associated with prolate symmetry (L>S). Flinn's (1965) L-S notation was initially introduced to describe finite strain ellipsoids or fabric ellipsoids but it is a useful shorthand for any anisotropy

#### 2.6 - AMS measurements

AMS was determined using a Sapphire Instruments SI2B device operating at 19,200 Hz and ~ 0.1 mT. The anisotropy measurement utilized the seven-orientation system (Borradaile & Stupavsky, 1995), which includes four body-diagonal measurements, improving precision over the more commonly used orientations confined to coordinate axes and their symmetry-planes (e.g., Girdler, 1961). Instrument control and real-time data processing were performed using the SI2B01 software package developed by G.J.B. A complete AMS determination and analysis requires less than four minutes per core. The low-field AMS was determined on 360 cores from 121 specimens of the local sampling campaign (Appendix 2 & 3) and remeasured on 730 cores from 298 specimens of the regional sampling campaign (Appendix 4 & 5) of Lagroix and Borradaile (2000). Sample holder correction is particularly critical in the case of specimens with near-zero susceptibility. In the seven orientations of measurement, the holder calibrates approximately -18, -18, -18, +30, +30, +30, and +30  $\mu$ SI, respectively.

#### 2.7 - AARM: Anisotropy of Anhysteretic Remanent Magnetization

AARM was determined using the same seven-axis anisotropy scheme as for AMS measurements. The specimen is fully demagnetized and then the seven differently oriented ARMs are applied and measured, in a sequence such that each ARM is inclined at 45° or 35.3° to the previous one. For many rock types, this effectively cleans the ARM acquired in each preceding treatment. This tested technique greatly reduces the measurement time because 3-axis AF cleaning between each ARM application is no longer necessary (Werner & Borradaile, 1996). However, the success of this short-cut

must be verified with each new measurement campaign and each new lithology. ARMs were imposed with a Sapphire Instruments three-axis Alternating Field (AF) demagnetizer outfitted with a supplementary DC coil applying a bias field of 0.05mT. The AF decayed from a peak field of 80 or 100 mT to zero while the DC bias field was turned on from 60 mT to zero. The imposed ARM was measured in a JR5a automatic spinner magnetometer (sensitivity 0.03 mA/m). Instrument control, measurement and simultaneous data-reductions were performed using the SPIN01 software package developed by Borradaile. Complete AARM determination and analysis requires 18 minutes per core. We have only included AARM results from regional scale sampling suite in this study. Of the original sample (n = 1170, Lagroix & Borradaile, 2000), 201 cores were rejected for AARM determination. The criteria for accepting or rejecting the AARM results occur during measurement; results were rejected if intensities were < 1mA/m when measured in position 1 of the AARM scheme or if the AMS ellipsoid for the sample had a negative  $\kappa$ . In the present study, for AARM we selected and re-measured 254 cores from 229 specimens from the original suite published by Lagroix and Borradaile (2000).

#### 2.8 - Sampling Strategy

The first level of sampling focussed on structurally and lithologically homogenous subareas  $\leq 30 \text{ km}^2$  that were densely sampled (Fig. 2-5). They include the Polis Rift Margins, Polis Basin, Galataria, Omodhos-Pakhna, Lefkara, and Lymbia, designated subareas I – VI, respectively, yielding n = 360 cores from N = 121 sites. These areas include Formations from the Lefkara up to the Athalassa Formation.

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Figure 2-5. Sub-areas of Cyprus (I-VI) and their magnetic fabrics as discriminated by standardization (specimen tensors standardized dividing by each specimen's  $\overline{\kappa}$ ). (a) Non-standardized AMS orientation distributions are biased by anomalously oriented subfabrics, especially with anomalously high- $\overline{\kappa}$ . (b) Standardized AMS fabrics usually suppress the contribution of specimens with anomalous orientations.


Figure 2-6. Regional domains of Cyprus (I-V) and their magnetic fabrics. (a) Non-standardized AMS. (b) Standardized AMS. (c) Standardized AARM. AARM isolates the magnetite sub-fabric and when standardized, and standardization subdues the contribution of anomalously oriented specimens.

The homogeneity of fabrics in these subareas justified the larger scale interpretation from the next level of sampling.

The second level of sampling was a diluted regional-scale campaign. The limestone specimens covered a wide age-range of the sedimentary cover, from the Lefkara Formation up to the Nicosia Formation (Lagroix & Borradaile, 2000). Of the original sample suite (cores n = 1170, sites N = 434), a sub-sample (n = 730, N = 298) was analyzed in five regional domains of similar tectonic style and trend (Fig. 2-6), each with an area of ~ 400 km<sup>2</sup>.

All hand-specimens were oriented in the field and three to six cores (25 mm in diameter and 22 mm high) were drilled in the laboratory from each specimen, restored to geographic coordinates.

## 2.9 - Localized sampling: Polis Rift Region (subareas I, II, III)

Non-standardized AMS in this, the Polis Rift region, differs from the other areas (Fig. 2-5a). From the faulted margins they exhibit an S>L fabric as shown by the elongate confidence cones for  $k_{MAX}$  and  $k_{INT}$ , and a small  $k_{MIN}$  confidence cone (Fig. 2-5a, sub-area I). The AMS axes are symmetrically compatible with stress directions of the last 5 Ma verified from fault orientations and from seismic data (Payne & Robertson, 2000; Borradaile & Hamilton, 2004).

In the basin, non-standardized data permit straightforward fabric interpretations (Fig. 2-5a, sub-area II). These younger strata have S>L depositional fabric as shown by the elongate confidence cones for  $k_{MAX}$  and  $k_{INT}$  in the foliation and a tight, near-vertical  $k_{MIN}$  confidence cone. The magnetic foliation is parallel to the bedding.  $k_{MAX}$  and  $k_{INT}$  lie

within the bedding plane and  $k_{MAX}$  is possibly a flow-alignment, since it is parallel to the rift axis (*cf.* Sagnotti et al., 1994). Raw, non-standardized AMS data demonstrates the effects of higher susceptibility specimens in which depositional-controlled AMS fabrics dominate.

In the Galataria region, non-standardized specimens exhibit an L $\approx$ S fabric, which appears nearly isotropic from its large, overlapping confidence cones (Fig. 2-5a, sub-area III). Nevertheless, the mean-tensor axes are similar to the other two preceding localities in this region.

How are these low- $\kappa$  samples affected by relativily high- $\kappa$  specimens? Standardizing the specimen AMS to  $\kappa$ , reveals similar susceptibility directions overall but demonstrate different confidence cone shapes (Fig. 2-5b, sub-areas I-III). All show L>>S ODs. The progressive increase in size of the confidence cones from west to east may be due to the smaller sample sizes (n = 152 to n = 25). The NE-trending k<sub>MAX</sub> L>>S fabric agrees with the crustal tension-axis required for the paired normal faults defining the Polis Graben and the normal fault zone defining the Pegia fault system (Payne & Robertson, 2000). The L>>S fabric of the AMS data is also symmetrically compatible with the current tectonic stress regime deduced from earthquake data (Borradaile & Hamilton, 2004; their fig. 2).

## 2.10 - Localized sampling: Southern slopes of Troodos (subareas IV, V, VI)

The three eastern-most detailed sub-areas show little difference between standardized and non-standardized samples (Fig. 2-5, sub-areas IV-VI). The Omodhos-Pakhna subarea (IV) displays an L $\approx$ S OD fabric with a shallow northward dipping

'foliation'. The Lefkara and Lymbia (sub-areas V and VI) localities display an S>L OD fabric as shown by the elongate confidence cones  $k_{MAX}$  and  $k_{INT}$  and a tight  $k_{MIN}$  confidence cone with a shallow NNE dipping foliation. These OD fabrics in the eastern localities represent a dominant sedimentary fabric with some secondary tectonic control. However, all are compatible with a south-directed movement (southerly *vergence*) within the limestone cover.

#### 2.11 - Regional scale AMS

Non-standardized AMS data of the five regional scale domains (Fig. 2-6a, subareas I-V) exhibit similar OD's for all areas. All five groups exhibit an S>>L fabric as shown by the elongate confidence cones for  $k_{MAX}$  and  $k_{INT}$  and a tight  $k_{MIN}$  confidence cone near vertical (Borradaile, 2001). This OD is similar to the results exhibited in the *density-contoured* data in Lagroix and Borradaile (2000). The S-component of the fabric is bedding-controlled and  $k_{MAX}$  is kinematically compatible with N-S extension, parallel to the aligned phyllosilicates caused by the stretching of the sedimentary cover (Lagroix & Borradaile, 2000).

But how are these low susceptibility samples affected by relatively high susceptibility samples that may be considered as statistical outliers? Standardizing the specimen ellipsoids to  $\kappa$ , AMS data of the five regional scale groups (Fig. 2-6b) reveals similar overall AMS axes but different confidence-cone shapes and, thus, different fabric ODs in the L-S range. These differences change progressively from L $\approx$ S in the east to L>S in the west. This corresponds to the increasing tectonic strain from east to west, inferred from earthquake data (Borradaile & Hamilton, 2004; Arvidsson et al., 1998; Ben-

Avraham, et al.,1988; Papazachos & Papaioannou, 1999) and overall structural trends (Robertson, 2000; Borradaile & Hamilton, 2004). In contrast, raw data (non-standardized) are weighted by higher susceptibility depositional subfabrics, rather than the weak tectonic ones compatible with supra-subduction SW-directed shortening (Lagroix & Borradaile, 2000).

#### 2.12 - Regional scale AARM

Only standardized data are presented for AARM to avoid the spurious effects due to the large variance in remanence intensity. Domains I, II &V (Fig. 2-6c) show similar overall AARM axes to standardized AMS (Fig.2-6b). This verifies the important contribution of magnetite to some AMS fabrics. They show an L $\approx$ S OD similar to the eastern-most standardized AMS, perhaps due to a near-uniaxial shape of magnetite, which when arranged in a weak planar fabric has a strong A<sub>MIN</sub> zone-axis girdle. Thus, the N-S extensional trend (seen in the AMS) is less effectively expressed but the fabric axes are kinematically compatible with movement directed toward the SW (or subduction to the NE). AARM fabrics for the other two sub-areas (Fig. 2-6c, sub-areas III & IV) exhibit S>>L fabrics; AARM axes indicate a more southerly directed movement. The AARM fabric may be a composite of the stylolitic cleavage incompletely overprinting the bedding fabric (Lagroix & Borradaile, 2000).

## Chapter 3 – Magnetic Mineralogy

## 3.1 - Introduction

As seen in previous chapters, understanding the magnetic mineralogy can be an important fact when interpreting magnetic fabrics. Therefore at least a brief introduction into some of the theories and background is necessary. Definitions of some of the more relevant terminology can be found Appendix 1, and a more in depth discussion of magnetic theory is provided in O'Reilly (1984).

Most magnetic measurements and techniques are based on the Néel equation:

which is  $\tau = 1/C \exp[Kv]/[KT]$  (for magnetite).

Relaxation time (remanence to decay) is related proportionally to coercivity, volume and inversely to temperature. Therefore by measuring remanence or coercivity one can investigate magnetic volume (grain size and concentration).

From the Néel equation and other magnetic theory equations one can determine which magnetic properties/measurements or combinations of measurements are dependent on concentration and which are dependent on composition (Table 3-1).

Table 3-1. Different Magnetic Techniques and their dependence on concentr	ation,
composition, and microstructure. Modified from (O'Reilly, 1984).	

<b>.</b>	Intensive	Extensive
	(independent of concentration)	(dependent on concentration)
Intrinsic (Dependent on composition)	Curie Temperature (T <sub>C</sub> )	Magnetic Saturation ( $M_S$ ) High-field Susceptibility ( $\kappa_{HF}$ )
Extrinsic	Coercivity (B <sub>C</sub> )	Saturation Remanence (M <sub>RS</sub> )
(Dependent on	Coercivity of remanence $(B_{CR})$	-and other remanence
composition	M <sub>RS</sub> /M <sub>S</sub>	measurements
and	Verweij Transition	(KARM, pARM)
Microstructure)	Temperature $(T_V)$	Low-field Susceptibility ( $\kappa$ )
	Konigsberger ratio (Q)	
	Unblocking Temperature $(T_{UB})$	

From Table 3-1 it can be seen that due to their intrinsic nature, Curie Temperature is an excellent property to assess magnetic composition whereas Magnetic Saturation is useful for determining concentration. The measurements in the extrinsic section of Table 3-1 can also be useful but usually involve either a combination of measurements or set assumptions about the rock in question. These magnetic assessments maybe more complicated because of the added dependency of Microstructure, which may include grain size, shape, internal stress and interactions, but added variables also mean added information in the process.

Magnetic granulometry determines either the actual or effective magnetic grain size of a mineral. Effective magnetic grain size refers to magnetic domain state or behaviour of a magnetic particle, regardless of the actual grain size dimensions of the particle. Domain states change from superparamagnetic (SP), to single domain (SD), to pseudo-single domain (PSD), and to multidomain (MD) with increasing grain size. Magnetite has been the most extensively studied magnetic mineral due to its dominance in both volume and magnetic contribution. Hence, most conventional magnetic granulometric studies focus only on converting domain states to effective magnetite grain sizes, although there are exceptions (Hunt et al, 1995, their table 2 for references).

- Multi-domain (MD) Containing several magnetic domains, each with a domain wall that can usually move when a weak magnetic field is applied (>2 μm)
- Pseudo-single domain (PSD) A magnetic domain that behaves as a singledomain particle (usually between 2 to 0.1 μm)
- Single domain (SD) A grain containing only one magnetic domain (usually between 0.1 μm & 0.02μm)

Superparamagnetic (SP) - A ferromagnetic grain that has strong paramagnetic properties, but loses any remanence over a few minutes (usually < 0.02µm;</li>
Borradaile & Jackson, 2004)

For titanomagnetites, it may not be possible to define universal magnetic domain sizes because of microstructural variations from grain to grain and rock to rock. However, the boundaries for PSD probably lie between 0.5 and a few  $\mu$ m (O'Reilly, 1984)

There are basically two types of magnetic measurements that can be used for magnetic granulometry. The first method is the use of magnetic hysteresis loops, and the second involves the analysis of different types of remanent magnetization (Banerjee et al., 1981).

In the most simplistic terms, magnetic hysteresis measures a sample's standardized coercivity and remanence properties at a constant temperature to deduce information about the samples magnetic mineralogy and magnetic volume or grain size.

Remanent magnetization studies also compare remanence measurements with different components of the Néel equation to deduce a sample's magnetic volume.

## 3.2 - Purpose

Studies of the magnetic mineralogy of marine sediments tend to fall into a number of categories; commonly related to continuous sequences, hence "magnetostratigraphy".

 Investigations to determine different mineralogical contributions to AMS and ARM (Borradaile, 2001; Rochette et al., 1992; and succinctly reviewed by Jackson, 1991).

- Investigations of biogenic (mainly bacterial) contributions of magnetic material to marine sediments (e.g., Kirschvink & Chang, 1984; Chang & Kirschvink, 1989; Vali & Kirschvink, 1989; McNeill, 1990).
- 3. Investigations to determine core correlation and as an indicator of variations of terrigenous sedimentation (e.g., Mead et al., 1986; Hall et al., 1989).
- Investigations studying diagenesis, authigenesis, or oxidation of magnetic minerals (e.g., Karlin & Levi, 1985; Karlin, 1990a,b; Wang & Van der Voo, 2004).
- Investigations examining the origin of the sediment NRM, in order to assess the reliability of NRM data for the determination of the geomagnetic paleopolarity and relative paleointensity (e.g., Kent & Lowrie, 1974; Lowrie & Heller, 1982; Tauxe & Wu, 1990).

The present study examines:

- Hysteresis to determine grain sizes and some magnetic mineralogy (Borradaile & Hamilton, 2003; Dunlop, 2002a,b; Wang & Van de Voo, 2004)
- 2. κ and κARM to determine concentration and mineralogy
- SIRM and thermal demagnetism in various ways to determine composition and concentration
- 4.  $\kappa$ ARM/ $\kappa$  (grain size and volume)(King et al., 1982; Banerjee et al, 1981)
- κARM/SIRM and SIRM/κ to determine relative grain size (Vigliotti et al., 1999).

#### 3.3 - Hysteresis

A rock's remanence-bearing properties are characterized by saturation isothermal remanence (SIRM =  $M_{RS}$ ) after exposure to a large field or magnetic saturation ( $M_S$ ) *in the presence* of a large field. Similarly, the tenacity of remanence is important, measured by coercivity ( $B_C$ , in the presence of a field), coercivity of remanence ( $B_{CR}$ , required to remove  $M_{RS}$ ) or the ease of demagnetation in an alternating field (AF) (Fig. 3-1). Wasilewski (1973) plots  $B_C$  against  $B_{CR}$  to infer magnetite grain size; and similarly, Day et al. (1977) plots  $M_{RS}/M_S$  against  $B_{CR}/B_C$ . The "Day plot" has been most popular, until recently, when plotting hysteresis data.

The success of the Day plot lies in its reasonable success in separating behaviour according to the presence of single-domain (SD), pseudo-single domain (PSD) or multidomain (MD) magnetite, especially where the specimens contain magnetite in just one of these categories. However, SP magnetite is difficult plot due to its highly variable magnetic properties, which overlap other domains in some instances. These categories are traditionally shown as rectangular fields with the data from sample sets plotting clusters in one or more of the domain sizes (Fig. 3-2). Unfortunately, although these plots are highly functional and user-friendly, they fail to discriminate the reality of mixed grain-size distributions that encompass more than one grain size, or more than one magnetic mineral or those that include SP magnetite. Dunlop (2002a,b) addressed these issues with the addition of domain-state mixing lines to the Day plot and studies of theoretical and actual mixing lines of magnetite with titanomagnetite (Fig. 3-2).



Figure 3-1. (a) An example of a hysteresis loop and the magnetic properties used in a Day Plot (1977); MS = saturation magnetization, BC = coercivity, MRS =remanent saturation at zero applied field. (b) in a separate demagnetization experiment, BCR = coercivity of remanence.



Figure. 3-2. Day Plots (Day et al. 1977) with the effective grain sizes (magnetic domains) and some relevant mixing lines of these domains (Dunlop, 2002a). (a) Pelagic limestone samples (n=43) plotting along SD-MD mixing lines (Dunlop, 2002a) in PSD domain of Day et al. (1977). (b) Non-pelagic limestone samples (n=57) mostly plotting along TM60 + magnetite linear mixing theory line (Dunlop, 2002a) in the PSD domain (Day et al., 1977).

#### Recently, Wang & Van der Voo (2004) have modified the Day plot by

eliminating the variable B<sub>CR</sub> and plotting only M<sub>RS</sub>/M<sub>S</sub> (or hysteresis squareness) against

B<sub>C</sub> to investigate differences in magnetic mineralogy of Mid-ocean ridge basalts (MORB)

whose main magnetic minerals include titanomagnetite  $Fe_{3-x}Ti_xO_4$  with x = 0.6 (TM<sub>60</sub>),

titanomaghemite (TM<sub>60</sub> low-temperature alteration product), and magnetite. They

demonstrate that the theoretical linear relationship between these variables essentially

show  $M_S$  differences and since magnetite has a  $M_S$  about 3.8 times greater than  $TM_{60}$ , differences in MORB magnetic mineralogy can be and have been assessed experimentally (Fig.3-3). Furthermore, Wang & Van der Voo (their fig. 6, 2004) demonstrate that samples with titanomaghemite plot at different point between the  $TM_{60}$ and magnetite trend-lines, confirming progressive oxidation of  $TM_{60}$  over time perpendicular to the ridge axis.

Other progressive hysteresis plots examine  $M_{RS}/M_S$  versus  $B_C$  versus  $B_{CR}$  in three-dimensional projections and use either regression surfaces (Borradaile & Lagroix, 2000) or confidence regions in two-dimensional planes (Borradaile & Hamilton, 2003) to assess differences in sample sets. Spectral methods using the entire hysteresis curve instead of just four points, have also been employed successfully and have given insight into the magnetic behaviour of bimodal mixtures (Jackson et al. 1990; Carter-Stiglitz et al., 2001). Unfortunately, these techniques are unfeasible in the present study due to their rather involved statistics and procedures.

An alternating gradient force magnetometer (MicroMag) was used to determine the parameters of the hysteresis loop. The instrument was developed commercially by Princeton Measurements Corporation (Princeton, NJ, USA). The specimen required has dimensions of no more than 2mm x 2mm x 1mm and its mass cannot exceed much more than ~100 mg. Thus it is difficult to make representative measurements for rocks that are heterogeneous, at that scale.



Figure 3-3. (a) Squareness ( $M_{Rs}/M_s$ ) versus coercive force ( $B_c$ ) for young unoxidized MORB (closed symbols) and low-Ti or Ti-free magnetite with different grain sizes (open triangular symbols). (b) Day-plot of same samples showing no diagnostic differences between TM60 and low-Ti magnetite (data and graphs reproduced from Wang & Van de Voo, 2004). (c) Squareness ( $M_{Rs}/M_s$ ) versus coercive force ( $B_c$ ) for Cyprus limestones with ti-poor magnetite (slope=0.01) and TM60 (slope=0.38) trend-lines (Wang & Van de Voo, 2004). Pelagic (n=43, slope=0.0112, R2=0.8473), Lefkara non-pelagic (n=39, slope=0.162, R2=0.863), and Polis non-pelagic (n=13).

The main limitation of this method is the size of the standard rock-magnetic core specimen being tested. The average mass of the limestone cores for this study is  $\sim 23$  g (10.55 cm<sup>3</sup>), therefore, at the most the Micromag hysteresis specimen represents  $\sim 0.04\%$  of the core from which it was taken (Borradaile & Lagroix, 2000). If any heterogeneity is present within the core then the hysteresis data from the small sample may not represent the core sample's magnetic properties accurately. Fortunately, the limestones of this study are relatively fine-grained and nearly homogeneous at that scale, so the hysteresis data of the smaller specimens is representative as replicate measurements show. That being said, hysteresis was only used as a somewhat preliminary magnetic study to look at the samples as a whole to assess overall grain sizes and possible magnetic compositional variations. Hysteresis was not examined in a stratagraphic context because intra-sample variation may obscure the inter-site variation in the stratigraphy.

A selection of specimens from early sample sets (before stratigraphic sampling was performed) was chosen randomly to examine some of their magnetic characteristics by use of hysteresis plots. These samples were grouped based on locations and basic lithology/facies (i.e., pelagic and non-pelagic) (Appendix 6). Pelagic limestones (chalks) (n = 43) were characterized by aphyric grain size and visible skeletal and non-skeletal debris and other visible detritus characterized non-pelagic limestones (n = 57). Although this classification scheme is not as detailed as others (Borradaile et al, 1993), it is appropriate for the purpose of this study. The hysteresis data was plotted on Day Plots with the addition of selected mixing lines to assess both grain-sizes and possible compositional differences (Fig. 3-2.) also as Mrs/Ms (or hysteresis squareness) versus Bc to investigate possible differences in magnetic mineralogy (Fig. 3-3c.).

In Figure 3-2a all samples plot on or near the magnetite SD-MD mixing line in the PSD range with the Polis samples cluttering closer to the SD range than the Lefkara cluster of samples. The tight clustering of samples seen in the Polis and Lefkara pelagic samples attest to the homogeneous nature and similar depositional environment of these fine-grained samples. The non-pelagic samples (Fig. 3-2b.) exhibit a much wider distribution on the Day plot due to either the more heterogeneous nature of these coarser grained samples or differences in depositional environments. These samples mostly plot to the right of the SD-MD mixing line near the right boundary of the PSD range. Unfortunately the constitution of these samples is more difficult to interpret due to the many mixing possibilities that could cause the samples to plot in this area and the fact that coercivity parameters do not behave linearly as a function of mixing ratios (Carter-Stiglitz et al., 2001). For this reason, theoretical mixing curves of data with bimodal mixtures usually fail to completely explain data from natural mixtures (Dunlop, 2002a). When comparing our samples to experimentally derived mixing lines (Dunlop, 2002a), the majority of non-pelagic samples of Cyprus tend to plot between the SD-MD mixing line for magnetite and the SD-MD mixing line for  $TM_{60}$ . Therefore, these samples could represent mixtures of magnetite and TM60 but this is inconclusive due to other possibilities that could have similar effects, such as the presence of other minerals like titanomaghemite, minor hematite or SP grains of magnetite.

By plotting  $M_{RS}/M_S$  (or squareness) versus  $B_C$  (Fig. 3-3c.) it is hoped that more insight into differences in magnetic mineralogy will be evident. On examination of the pelagic samples it is noted that they have a well-defined trend-line near that of magnetite. In contrast, the non-pelagic Lefkara samples form a well-defined trend line between the magnetite trend-line and  $TM_{60}$  trend-line, where as the non-pelagic Polis samples do not form a well-defined trend-line due to their small sample set (n = 13), but do tend to plot near the magnetite trend line. There are two main possibilities for the well-defined trend line of the non-pelagic Lefkara samples. First, these samples magnetic mineralogy may be dominated by titanomaghemite of some intermediate oxidation state, such as that found in oxidized pillow basalts (Wang & Van der Voo, 2004). Second, these samples may have a relatively uniform bimodal mixture of magnetite and  $TM_{60}$ . The non-pelagic Polis samples probably represent non-uniform mixtures of different magnetic minerals within a small size range, but the small sample set (n = 13) and the wide age range (55-0 Ma) that the Polis rocks cover, interpretations are somewhat uncertain.

#### 3.4 - Sedimentary sequence and Sampling Strategy

Omodhos-Pakhna, Lefkara, and Lymbia (subareas IV-VI from AMS section, Fig. 2-5, N = 55) were sampled with special attention to stratigraphic sequence for examination of stratigraphic changes in magnetic mineralogy (Appendix 2 & 7). These three subareas cover a relatively continuous sequence of samples from lower Lefkara formation (54 Ma) to upper Pakhna Formation (6Ma) (Figs. 3-4 & 3-5). Although their biostratigraphy is unknown, numerous previous studies have been conducted on the sections (Mantis, 1970; Eaton and Robertson, 1993; Eaton, 1987; Kahler, 1994; Kahler and Stow, 1998; Lord et al., 2000). Unfortunately, the distribution and development of different lithological units within the Lefkara Formation is not uniform due to tectonic events, paleotopography, and redeposition of sediment (Lord et al., 2000). Therefore, the ages for the sections in this study are most precise at the identifiable stratigraphic



Figure 3-4. Geological map of South and West Cyprus showing locations of stratigraphic sampling.



Figure 3-5. Circum Troodos Sedimentary Succession and ultramafic basement (Geological survey department of Cyprus 1979) with biostratigraphic ages for relevant limestone units.

boundaries from the from the most proximal and accepted biostratigraphic study. Samples not taken near stratigraphic boundaries have their ages estimated by stratigraphic order and estimated sedimentation rate. Samples that have overlapping age determinations or are less than 0.5 Ma apart in age are averaged. The continuous nature of our sample set is punctuated by an approximately 15 million year hiatus between 35 Ma to 20 Ma. This hiatus corresponds to the start of major glaciations in the Southern Hemisphere (Haq et al., 1987) and is thought to be caused by subsequently enhanced bottom current erosion (Vali et al., 1980; Miller et al., 1987). Therefore, this Cyprus hiatus does not reflect the effects of tectonic uplift as proposed by Robertson et al. (1991) but represent more global sedimentological effects (Kahler and Stow, 1998)

## 3.5 – Methods for Magnetic Mineralogy

As shown in the chapter on AMS, the specimen's bulk susceptibilities  $[\kappa = \sqrt[3]{(k_{MAX}k_{INT}k_{MIN})}] \text{ can be a first guide to the magnetic mineralogy.}$ 

By examining  $\kappa$  in relation to a sample's stratigraphic sequence it is possible to see changes in mineralogy through time and in different formations (Fig. 3-6).  $\kappa$ ARM can also be examined in the same way as  $\kappa$  (Fig. 3-6), but since it measures remanence, variation between samples are completely due to ferromagnetic minerals and are not affected by a sample's diamagnetic or paramagnetic minerals. Therefore,  $\kappa$ ARM is a better indicator of stratigraphic variation of magnetite than  $\kappa$ .



Figure 3-6. KARM and K versus stratigraphic sequence, demonstrating differences in magnetic mineralogy through time.



Figure 3-7. SIRM versus stratigraphic sequence, demonstrating differences in magnetic mineralogy through time.

The examination of SIRM results should reveal magnetic contribution better than  $\kappa$ ARM and  $\kappa$  because it is not affected by a sample's diamagnetic or paramagnetic minerals (like  $\kappa$ ) and, compared to  $\kappa$ ARM values, grain size has very little affect (for the size range present in these samples) (Peters & Dekkers, 2003). Therefore SIRM is primarily a function of ferromagnetic mineralogy and concentration (Fig. 3-7). The SIRM data demonstrates a slight overall decrease in remenance with fluctuating values in the Pakhna formation and the Chalk & Chert section of the Lefkara formation similar to the  $\kappa$ ARM data.

As seen in the previous chart of magnetic properties (Table 3-1), Curie temperature ( $T_C$ ) is the only intrinsic property, which is dependent only on ferromagnetic mineral composition. Therefore by comparing Curie Temperature data with SIRM data one can infer the different magnetic contribution of minerals. By thermally demagnetizing a specimen to 200°C, one essentially randomizes the SIRM intensity caused by the TM<sub>60</sub> fraction of the specimen. Therefore by subtracting the SIRM intensities after thermal demagnetization of 200°C from the original SIRM, the SIRM caused by the TM<sub>60</sub> fraction can be isolated (SIRM<sub>TD200</sub>). Furthermore, to minimise the effects of differing sedimentation rates one can normalize it to the original SIRM by the following equation:

SIRM<sub>TD200</sub>/SIRM x 100 = % of SIRM intensity after TD200 = % of SIRM *not* caused by TM<sub>60</sub>. The SIRM<sub>TD200</sub>/SIRM data (Fig. 3-8) exhibits a general trend to increasing TM<sub>60</sub> contribution with the exception of the Chalk Unit. The low TM<sub>60</sub> contribution of SIRM but overall high SIRM intensity of the Chalk unit may represent a lack of clastic input with the major magnetic contribution due to fossil magnetotactic bacteria.



Figure 3-8. SIRM200°C/SIRM versus stratigraphic sequence. SIRM values after thermal demagnetization to 200°C/SIRM values before thermal demagnetization versus stratigraphic sequence demonstrating differences TM60 contributions through time.

Many factors may complicate the combination of SIRM data with Curie temperatures. First, the use of SIRM<sub>TD200</sub>/SIRM ratio to analyze TM<sub>60</sub> contribution assumes that no other high remanence/low T<sub>C</sub> minerals are present (such as goethite). This possibility can be assessed quite easily by examination of the hysteresis data. Second, oxidation of TM<sub>60</sub> increases T<sub>C</sub>, SIRM<sub>TD200</sub>/SIRM only isolates TM<sub>60</sub> with low oxidation coefficients. This in turn, means that fluctuations in SIRM<sub>TD200</sub>/SIRM ratios may represent fluctuations of TM<sub>60</sub> contribution *or* fluctuation rates in the oxidation of TM<sub>60</sub> (or both). This complication could possibly be assessed by performing thermal demagnetization on the same samples at 300°C and examining SIRM<sub>TD300</sub>/SIRM ratio versus the SIRM<sub>TD200</sub>/SIRM ratio. The difference in ratios should be equivalent to TM<sub>60</sub> with an oxidation coefficient of 0.2 (Ozdemir and O'Reilly, 1982a). Higher oxidation TM<sub>60</sub> components of these specimens would not be possible to assess in a similar fashion due to the titanomaghemite inversion temperature at 350°C, which would change the mineralogy.

#### 3.6 – Methods for Magnetic Granulometry

Both  $\kappa$  and  $\kappa$ ARM, dependent variably on magnetic domain size;  $\kappa$  values increase through the SD PSD-MD range whereas  $\kappa$ ARM exhibits the reverse trend through the same range. Therefore, ratios of  $\kappa$ ARM/ $\kappa$  can show grain size differences with higher ratios of  $\kappa$ ARM/ $\kappa$  indicative of finer magnetite sizes (Banerjee et al, 1981). Experimental verification of this relationship between  $\kappa$ ARM and  $\kappa$  lead to a simple phenomenological model, which can be used to detect changes in either the relative grain-size or amount of magnetite in natural materials (Fig. 3-9)(King et al., 1982).



Figure 3-9. King et al. (1982) Plot. KARM versus K, and relative grain-size or amount of magnetite in natural materials using experimental models.



Figure 3-10. KARM/KLow Field versus stratigraphic sequence demonstrating ferromagnetite grain size changes through time. Grain size from King et al. (1982) assuming pure magnetite in low concentrations.

It must be stressed that several complications have to be considered when using the King et al., (1982) model quantitatively. First, the presence of SP magnetite would only affect the  $\kappa$  value and not the  $\kappa$ ARM value of a sample, making the sample appear to have coarser magnetite than actually present. Hysteresis data from the present study shows that SP magnetite is probably not a contributing factor in these samples. Second, the effect of magnetic interactions with varying concentrations of magnetite may affect  $\kappa$ ARM/  $\kappa$ differently. Again this is not a problem for this study due to the extremely low concentrations of ferromagnetic minerals in these samples as seen from the bulk  $\kappa$  values mentioned above. Third, an increase in the shape anisotropy of magnetite from 1 to 1:1.5 (axial ratio) may increase the  $\kappa$ ARM/  $\kappa$  value slightly. Fourth, complications arise due to the shifting of the abscissa by the  $\kappa$  of the non-magnetic matrix. This final complication may be the most likely to affect the effectiveness of the King model for the samples in this study since minor amounts of clay may switch a limestone sample from diamagnetic to paramagnetic. The abscissa is shifted to larger values by a paramagnetic matrix and to lower values by a diamagnetic matrix.

Due to the extremely low  $\kappa$ ARM/  $\kappa$  values found in the limestone samples (and therefore low magnetic mineral concentration values), the standard King model cannot be used. Instead, the  $\kappa$ ARM/  $\kappa$  ratios and their corresponding grain-size are plotted on a stratigraphic column with the corresponding specimen's  $\kappa$ ARM/  $\kappa$  value (Fig. 3-10). From this data, it can be seen that the majority of the specimens (with the exception of the Lower Marl) have magnetite in the PSD size range (PSD ~ 0.1µm to 20µm), which corresponds acceptably with the hysteresis data. In fact, most of the upper chalk unit plot in the 0.2µm to 0.1 µm range, which corresponds with the size of magnetotactic bacteria

(Kirschvick, 1983) showing that these rocks have had little or no contamination from clastic or exhalative processes.

In addition to  $\kappa$ ARM/  $\kappa$  ratios, relative grain size may also be examined using SIRM/  $\kappa$  ratios (Fig. 3-11) and  $\kappa$ ARM/ SIRM ratios (Fig. 3-12) (Vigliotti et al., 1999). Similar to  $\kappa$ ARM/  $\kappa$ , lower values of SIRM/  $\kappa$  ratios and  $\kappa$ ARM/ SIRM ratios *should* correspond to larger magnetite grain sizes, but  $\kappa$ ARM /SIRM contradicts this. The simple reason for these discrepancies is that these ratios are dependent on composition as well as grain size. Since different minerals have different  $\kappa$ ARM,  $\kappa$ , and SIRM values their ratios will differ accordingly.

# 3.7 - Stratigraphic Interpretation of Magnetic Mineralogy and Granulometry

#### Lower Marl (56 to 53.5 Ma)

The lower marl represents the oldest unit of the Lefkara Formation overlying pillows at the section sampled (Lymbia) and umbers at some other locations (Fig. 3-5). These samples consist of pink marl, chalky marl and chert (Fig. 3-13). The samples of this formation are characterized by relatively high KARM/ $\kappa$  representing very fine grain sizes, relatively high SIRM representing above average magnetic concentrations, and relatively low SIRM/SIRM<sub>TD200</sub> ratios representing low TM<sub>60</sub> content (Fig. 3-14).

These magnetic properties and the pinkish hue of the samples indicate that the main magnetic carriers in these rocks are probably accumulations of very fine-grained Fe from hydrothermal exhalations of a nearby active vent system.



Figure 3-11. SIRM/ $\kappa$  versus stratigraphic sequence.

**KARM/SIRM** 



Figure 3-12. KARM/SIRM versus stratigraphic sequence.



Figure 3-13.Lefkara Lower Marl Unit. Lymbia highway section demonstrating the characteristic pink hue of the Lefkara Lower Marl unit.

## Chalk and Chert (53.5 to 46.2 Ma)

The Chalk and Chert unit of the Lefkara formation is comprised of chalk marl, and chert and directly overlies the lower marl unit (Fig. 3-15). The samples of this section are characterized by fluctuating low  $\kappa$ ARM/ $\kappa$ , fluctuating SIRM, and fluctuating high SIRM/SIRM<sub>TD200</sub> ratios (Fig. 3-14).

These large fluctuations in magnetic properties can be attributed to the presence of abundant pelagic calciturbidites (Robertson, 2000), which would rework and redeposit differing amounts of coarser pelagic sediments with finer pelagic sediments of different mineralogies. These sediments were later partially replaced by chert.



Figure 3-14. Amalgamation of Figures 3-10, 3-7, and 3-8 for ease of comparison.



Figure 3-15. Chalk and Chert Unit. Close-up of chert nodule in typical Chalk and Chert Unit from Lefkara formation.



Figure 3-16. Chalk Unit. Example of Chalk Unit from Lefkara type location near Upper Lefkara Village.

#### Chalk (46.2 to 36.3 Ma)

The Chalk unit of the Lefkara Formation is comprised of chert-free chalk with occasional marl and directly overlies the Chalk and Chert unit (Fig. 3-16). These samples are characterized by high  $\kappa$ ARM/ $\kappa$  ratios representing small grain sizes (mostly in the 0.1 –0.2 µm size range), large smooth changes in SIRM representing gradational changes in concentration, and decreasing SIRM/SIRM<sub>TD200</sub> ratios from intermediate (bottom of unit) to very low (top of unit) representing increasing contributions of magnetite (Fig. 3-14).

The smooth changes of this unit represent gradational changes in sedimentation rates best seen in the SIRM data, which represents magnetic concentration. The decreasing SIRM/SIRM<sub>TD200</sub> ratios and high  $\kappa$ ARM/ $\kappa$  ratios attest to the increasing contribution of magnetite from magnetotactic bacteria. The decrease in SIRM/SIRM<sub>TD200</sub> ratios and increase in SIRM values in the upper part of the unit can either be attributed to a decreasing sedimentation rate of calcareous material or an increasing productivity of fossil magnetotactic bacteria.

## Upper Marl (20.4 to 15.4 Ma)

The Upper Marl unit of the Lefkara Formation is comprised of marl and marly chalks and overlies the Chalk unit unconformity. These samples are characterized by high  $\kappa$ ARM/ $\kappa$  ratios representing small grain sizes, decreasing SIRM values, and increasing SIRM/SIRM<sub>TD200</sub> ratios (Fig. 3-14).

Although the  $\kappa$ ARM/ $\kappa$  ratios still show a pelagic grain-size distribution, the decreasing SIRM and increasing SIRM/SIRM<sub>TD200</sub> ratios attest to decreasing input of magnetotactic bacteria to the magnetic contribution of the unit. This decrease in

magnetotactic bacteria can be attributed to a gradual increase in sedimentation rates from the pelagic chalk units below to the more detrital nature of the Pakhna Formation above.

## Pakhna (15.4 to 5.5 Ma)

The Pakhna Formation is comprised of alternating chalks, marls, marly chalks, chalky marls, and arenites forming a gradational contact with the underlying upper marl unit of the Lefkara Formation (Fig 3-17). These samples are characterized by fluctuating/decreasing KARM/K ratios, fluctuating SIRM values, and fluctuating high SIRM/SIRM<sub>TD200</sub> ratios (Fig. 3-14).



Figure 3-17. Pakhna Formation. Ideal sampling section North of Pakhna type section.

The fluctuating high SIRM/SIRM<sub>TD200</sub> ratios and fluctuating/decreasing  $\kappa$ ARM/ $\kappa$  ratios can be attributed to fluctuation input of detrital TM<sub>60</sub> in these samples. The fluctuating SIRM values show a copasetic relationship to the SIRM/SIRM<sub>TD200</sub> ratios, which means SIRM is not a useful indication of magnetic concentration in this section since SIRM is also dependent on magnetic mineralogy.

#### Polis Basin (<5 Ma)

Although the stratigraphic samples end in the upper Pakhna unit, the present study also has a substantial amount of susceptibility data ( $\kappa$ ) from the Polis basin sub-area (local sub-area II, Fig. 3-5), which is comprised of limestones that were deposited subsequent to the deposition of the Pakhna (Fig. 3-4). The Polis basin samples exhibit a mean  $\kappa$  of 141 µSI (Fig. 2-2a), which is over three times greater than the mean  $\kappa$  of total samples of the study. This is thought to represent an even greater contribution of detrital material from the Troodos ophiolite than all previous formations.

## 4 – Conclusions

- Low-κ rocks such as limestone may show unstable AMS axes due to sub-equal competition from subfabrics of diamagnetic calcite and paramagnetic clays, with traces of magnetite. They may also show specimens of either positive or negative bulk susceptibility and this requires some care in plotting either orientations or shapes (Borradaile & Jackson, 2004). In the limestone cover to the Troodos ophiolite of Cyprus, such low-k subfabrics commonly arise from a weak tectonic overprint on depositional fabrics.
- 2. Standardizing AMS principal values of specimens to their κ equalizes the contributions of subfabrics/specimens with different κ in the overall sample mean-tensor. Thus, one subfabric may be emphasized or neutralized. This may have a similar effect to determining a PSD (pseudo-single domain, see magnetic mineralogy section) magnetite subfabric with AARM (Lagroix & Borradaile, 2000), although it is not a satisfactory substitute for AARM.
- 3. Applying the above techniques to the limestone cover of Cyprus isolates depositional fabrics from neotectonic fabrics associated with NNE subduction; neotectonic fabrics associated with rifting; and composite fabrics from feeble stylolitic foliation imprints on bedding.
- 4. Standardizing AMS data for petrofabrically homogenous subareas or domains reveals fabrics compatible with neotectonic stress trajectories in post-Paleogene strata. This is well shown in the Polis basin (<5Ma) and the Galataria sub-area (43Ma to 62Ma) (Figure 2-5b, sub-areas II and III respectively), which show

nearly identical fabrics in rocks with 40 million years age difference, but similar tectonic setting.

- 5. Examination of AMS tensors for sub-areas, and also for larger regions reveals tectonically significant axes, related to stress rather than finite strain. The orientation distribution of the mean tensor has an ellipsoid shape that may reveal the relative magnitudes of the principal stresses.
- 6. The examination of SIRM magnitudes at different demagnetization temperatures appears to be an innovative method of determining differences in magnetic mineralogy and concentration. This new method has proven particularly useful in cases of a bimodal magnetic mineralogy where the minerals in question have vastly different Curie temperatures (ie. Magnetite~ 585°C and TM<sup>60</sup>~ 180°C).
- 7. From the plotting of κARM/κ versus stratigraphic sequence, approximate stratigraphic control on magnetite grain sizes can be determined. In more complicated systems with more ferromagnetic minerals than just magnetite, relative grain size may also still be determined.
- 8. The combination and comparison of multiple magnetic techniques against stratigraphic sequence can illustrate changes in sedimentary and tectonic environments that may not be easily recognizable otherwise.
## 5-Discussion: Paleomagnetics and Tectonic Implications for Cyprus

### Plate Scale Tectonics

By studying paleomagnetism and the paleopoles of Cyprus ophiolites and other previously published paleomagnetic data, an APWP for Cyprus has been proposed by Borradaile and Lucas (2003). The APWP demonstrates that the Troodos microplate was located in equatorial latitudes between 88 and ~50 Ma and possessed a vertical intra-plate axis upon which its 60° anticlockwise rotation was based. Subsequently, during the time of limestone formation on Cyprus, the microplate drifted northwards to 34°N with minor anticlockwise rotation about a vertical axis located to the west of Cyprus (Table 2-1) (fig. 12, of Borradaile & Lucas, 2003).

### **Regional Scale Tectonics**

The magnetic fabrics determined by AMS from 1090 specimens from 419 sites over Southern Cyprus ( $\sim$ 2000 km<sup>2</sup>), demonstrate that much can be ascertained about the regional tectonics of Cyprus during the past 54 million years.

Non-standardized AMS for the five regional domains of this study (Fig. 2-6a) all show similar S>>L ODs (characteristic of bedding controlled depositional magnetic fabrics) with a  $k_{MAX}$  direction kinematically compatible with N-S extension, parallel to the alignment of the phyllosilicates caused by the stretching of the sedimentary cover over the Troodos ophiolite (Lagroix & Borradaile, 2000).

Examination of standardized AMS fabrics (Fig. 2-6b) reveal similar AMS axes, but show an east to west progression from L $\approx$ S to L>S ODs. This progression corresponds to the increasing tectonic strain from east to west, as inferred from earthquake data and structural trends (Borradaile & Hamilton, 2004; Arvidsson et al., 1998; Ben-Avraham, et al., 1988; Papazachos & Papaioannou, 1999; and Robertson, 2000).

AARM data for these samples (Fig. 2-6c) demonstrate similar magnetic fabric axes as standardized AMS but different (weaker) ODs possibly due to the near-uniaxial shape of magnetite. Other deviations from the standardized AMS ODs are probably due to composite fabrics of stylolitic cleavage incompletely overprinting the original bedding fabric (Lagroix & Borradaile, 2000).

#### Local Scale Tectonics

By examining the AMS data of different stratigraphic units and at a more local scale one can further define the tectonic regimes and justify the regional scale interpretations.

Local sub-areas adjacent to the Polis rift (I, II, III) demonstrate a wide variety of non-standardized AMS fabrics (Fig. 2-5a) including a neo-tectonic fabric (I), a depositional bedding fabric (II), and a possible composite fabric (III). Upon standardization of AMS (Fig. 2-5b), these three sub-areas appear to homogenize demonstrating a strong tectonic fabric corresponding to strain trajectories compatible to the formation of the Polis rift valley (Payne & Robertson, 2000) and the current tectonic stress regime deduced from earthquake data (Borradaile & Hamilton, 2004).

The three easternmost local sub-areas exhibit little difference between nonstandardized (Fig. 2-5c) and standardized samples (Fig. 2-5d). Elongate confidence cones  $k_{MAX}$  and  $k_{INT}$  and a tight  $k_{MIN}$  confidence cone characterize all of these fabrics with a shallow NNE dipping foliation. These OD fabrics represent a primary sedimentary fabric

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with some secondary tectonic control, similar to that seen in the corresponding regional sub-areas.

#### Magnetostratigraphy and Tectonic Implications

It was hoped that the present study would help resolve the timing of the uplift and subsequent erosion of the Troodos ophiolite. The use of the SIRM/SIRM<sub>TD200</sub> ratio as an indicator of  $TM_{60}$  contribution is expected to demonstrate presence of a sharp transition from low SIRM/SIRM<sub>TD200</sub> ratio values to higher values at the time of uplift. The data shows the presence of significant  $TM_{60}$  through out the entire Pakhna, Upper Marl Unit, and the older Chalk and Chert unit (Fig. 3-14). The presence of  $TM_{60}$  in the Chalk and Chert unit could be due to contributions from submarine volcanism similar to that found in the Lower Marl unit just below it. The Pakhna unit and Upper Marl Unit, in contrast, was deposited in a relatively shallow environment (<1 km depth) (Robertson, 2000), therefore submarine volcanism is not expected to contribute any significant part to these rocks. Therefore, it is believed that the gradual increase in the SIRM/SIRM<sub>TD200</sub> ratio in the Upper Marl Unit represents the first signs of uplift and erosion of the Troodos ophiolite, which may slightly predate 20 Ma. Unfortunately, due to the large hiatus in the sedimentary record, more precise chronometry is not possible.

Also of significant interest is the presence of a temporary sharp decrease in the SIRM/SIRM<sub>TD200</sub> ratio and KARM/K ratio at about 12 Ma (Fig. 3-14). This corresponds with the first record of coarse ultra-mafic material in the Cyprus limestone cover sequence documented by Orszag-Sperber et al.(1989) and probably represents a time of very rapid uplift and unroofing of the pillow and dike sequences (fig. 8, Robertson, 2000).

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### Appendix 1. Glossary of Magnetic and Tectonic Fabric Terminology from Borradaile and Jackson (2004)

We generally follow the usage of Collinson (1983) and Hunt et al (1995); symbols differ to varying degrees in standard references (Stacey & Banerjee 1974, O'Reilly 1984, Dunlop & Özdemir 1997, Tauxe 1998).

	Magnetishi & anisotropy terminology
p M	magnetic dipole moment $[Am^2]$ ; a measure of the strength of a magnet. volumetric magnetization intensity $[A/m]$ ; dipole moment per unit volume.
J H	mass-specific magnetization intensity [Am <sup>2</sup> /kg]; dipole moment per unit mass. magnetic field [A/m]. In the absence of free currents, the tangential component of <i>H</i> is continuous across a material boundary
В	magnetic induction $[T] = [Wb/m^2] = [J/(Am^2)]$ . $B = \mu_0(H + M)$ , where $\mu_0$ , the
K	permeability of free space, is a fundamental physical constant ( $\mu_0 = 4\pi \times 10^{-7}$ H/m). The normal component of <i>B</i> is continuous across a material boundary. magnetic susceptibility [dimensionless]; the ratio of induced magnetization to magnetizing field $\kappa = M / H$ , measured in a low direct field (e.g., SQUID
	magnetometer) or alternating field (e.g., induction coil). To preserve linear magnetization-field response ( $M = \kappa H$ ), the field must not affect the remanence of any permanently magnetizable content, i.e., usually $\leq 10$ mT. Induction coil methods use low frequencies ( $\leq 20$ KHz) to suppress conductivity responses. $\kappa$ is frequency dependent for conductive materials and for viscous superparamagnetic grains.
AMS	anisotropy of magnetic susceptibility with principal values $\kappa_{MAX} \ge \kappa_{INT} \ge \kappa_{MIN}$ ,
	described as a second-rank tensor. Where the principal values have the same sign,
AMS ellipsoid	The AMS tensor possesses a representation surface, a quadric of radii $r$ . Only where the principal susceptibilities have the same sign and where none are zero can we define a magnitude ellipsoid ( <i>the AMS ellipsoid</i> ) with radii $1/\sqrt{r}$ .
$\overline{\kappa}$	Bulk susceptibility; commonly given as arithmetic mean of the principal
	susceptibilities, $(\kappa_{MAX} + \kappa_{INT} + \kappa_{MIN})/3$ , if all principal values have same sign. The
	geometric mean is preferred, especially if the anisotropy is large, as in AARM or finite strain; requires non-zero, same-sign principal susceptibilities.
Standardized	Principal values ( $\kappa_{MAX}$ , etc.) may be standardized simply by dividing by $\kappa$ . For the
	finite strain tensor, principal axes must be standardized using their <i>geometric</i> mean since anisotropies may be large.
Р	Anisotropy degree, $P = \kappa_{MAX} / \kappa_{MIN}$
L	Magnetic lineation $L = \kappa_{MAX} / \kappa_{INT}$ cf. Flinn's <b>a</b>
F	Magnetic foliation $F = \kappa_{INT} / \kappa_{MIN} cf$ . Flinn's <b>b</b>
$P_j$ or $P'$	Jelínek's (1981) "corrected" anisotropy degree, reflecting eccentricity of the magnitude ellipsoid for a second rank tensor where all principal values have the same sign. Ranges from 1.0 (sphere, isotropy) upward, original definition involved normalization with arithmetic mean of susceptibility but for higher anisotropies, e.g. AARM or strain the geometric mean may be preferable.
Т	Jelínek's (1981) shape parameter for the magnitude ellipsoid, measuring the range from prolate (T=+1) through neutral (T=0) to oblate (T=+1) ellipsoids, independent of eccentricity; identical to Lode's parameter (1926), v of structural geology.

Magnetism & anisotropy terminology

χ DC	mass-specific susceptibility $[m^3 kg^{-1}]$ ; $\chi = J/H = \kappa$ /density. direct current used to apply a steady field, for IRM or as a bias field to generate an
AF	AKM. Alternating field; laboratory applied sine wave field damped so that its amplitude
	decays progressively and usually linearly with time.
Remanence	magnetization that persists in the absence of an applied magnetic field. In contrast induced magnetization, measured during the study of AMS, disappears when the applied field is removed.
ĸ	intrinsic magnetic susceptibility [dimensionless]; not directly measured for high- susceptibility materials, where it is "screened" by self-demagnetization.
μ	(relative) magnetic permeability. In linear materials and/or in weak applied fields, u = 1 + u, and absolute normaphility. $u = uu$ , relates magnetic induction <i>B</i> and
	$\mu = 1 + \kappa_i$ , and absolute permeability $\mu_{abs} = \mu \mu_0$ relates magnetic induction <i>b</i> and (interval) magnetic field <i>U</i>
	(internal) magnetic field $H$ P = w (H + M) = w (H + m H) = w H(1 + m) = w w H - w H
	$B = \mu_0(H + M) = \mu_0(H + \kappa_i H_i) = \mu_0 H(1 + \kappa_i) = \mu_0 \mu H = \mu_{abs} H$
ARM	anhysteretic remanent magnetization; laboratory remanence due to small DC field biasing the moments scattered during the decay of a simultaneously decaying large alternating field.
AARM	anisotropy of anhysteretic remanent magnetization
$\kappa_{_{ARM}}$ or $A$	anhysteretic susceptibility, $M_{ARM}/H_{dc}$ [dimensionless]. Mean value is
	$\overline{A} = \overline{\kappa_{ARM}} = \left(\kappa_{ARM,MAX}\kappa_{ARM,INT}\kappa_{ARM,MIN}\right)^{\frac{1}{3}}, \text{ where}$
	$\kappa_{ARM,MAX} \ge \kappa_{ARM,INT} \ge \kappa_{ARM,MIN}$ (Geometric mean is wiser, since anisotropies are
	large and ARM's are always positive values.)
pARM	Partial anhysteretic remanent magnetization (that due to grains in a selected range of coercivities).
pAARM	Anisotropy of pARM.
MD	multidomain (remanence-bearing) grain: for <i>magnetite</i> usually >5 domains and >2 $\mu$ m diameter but shape-dependent
SD	Remanence-bearing grain with a unique direction of spontaneous magnetization (in one domain): for <i>magnetite</i> 20-100 nm but shape-dependent
SP	Superparamagnetic grains are SD but thermally unstable; for <i>magnetite</i> <20nm but shape-dependent
PSD	Pseudo-single domain; remanence-bearing grain that has some remanence properties
	like SD and therefore desirable in routine paleomagnetism (for magnetite 2-
Dehidomain	5 domains, $\sim 0.1-2\mu m$ in diameter, depending on shape.
Polyaomain	umbrena term for MD & PSD characteristics.
TM	Titanomagnetite series $Fe_{3-x}Ti_xO_4$ e.g., $TM60 = Fe_{2.4}Ti_{0.6}O_4$
IRM	Isothermal remanent magnetization; remanence acquired in a large DC field
SIRM	Saturation isothermal magnetization; saturation remanence aquired in a large DC field
AIRM	Anisotropy of isothermal remanent magnetization
Inverse AMS	Due to (a) SD magnetite grain in which $\kappa_{MIN}$ must be parallel to the long-axis OR
fabric	

Blended AMS	Rock AMS fabric that combines magnetic subfabrics without a simple one-to-one
fabric	mapping or parallelism of their principal magnitudes, e.g., $\kappa_{MIN}$ for one sub- fabric is
	inclined to $\kappa_{MIN}$ for another subfabric. The subfabrics may be due to some
	combination of minerals with inverse and normal AMS, OR to some combination of
	competing petrofabrics.
Diamagnetism	Universal negative susceptibility response, usually Á -14µSI. Loosely refers to some
	minerals, which if pure, would only show a diamagnetic response, e.g., quartz,
	calcite. However, natural examples commonly have overwhelming positive
	responses from inclusions. Rocks such as quartzite and limestone are rarely
	diamagnetic. Diamagnetism is not temperature-dependent.
Paramagnetism	Positive response to an applied field with $0 \le \kappa \le 2000 \ \mu SI$ for most pure rock-forming
	minerals. (Unfortunately, matrix minerals are rarely pure and $\kappa$ may be much higher
	due to high- $\kappa$ microscopic-submicroscopic inclusions or exsolutions (e.g., iron-
	oxide; see "ferro" magnetic). Paramagnetic susceptibility decreases inversely with
	temperature.
"Ferro"-	Umbrella term for magnetically-ordered phase, more specifically and more
magnet	accurately described as, e.g., ferrimagnetic (magnetite) or antiferromagnetic
	(hematite). Sometimes stoichiometrically controlled, e.g., pyrrhotite (Fe <sub>1-x</sub> S) is
	ferrimagnetic for $x \ge 0.125$ , otherwise antiferromagnetic. Ferromagnetism mostly
	decreases non-linearly with increasing temperature and disappears above Curie
	temperature (ferrimagnets) or Néel temperature (antiferromagnets).

Structural & petrofabric terminology

Strain	Change of shape; homogenously, keeping parallel lines parallel and straight lines
	straight, of heterogeneously. Homogeneous finite strain, a second rank tensor, may
	always be represented by a magnitude empsoid since principal magnitudes are
	deduced from a single state of hom assesses fighte strains) may not be
··· · · · · · ·	deduced from a single state of nomogeneous finite strain.
$X \ge Y \ge Z$	Principal stretches or finite strains, axes of the finite strain ellipsoid (Ramsay, 1967).
	[Note that Flinn's original work (1961) used the convention, $Z \ge Y \ge X$ , which
	was never widely adopted]. Stretch = (new length)/(old length).
Flinn's a, b	a=X/Y, $b=Y/Z$ describes the magnitude ellipsoid of the finite strain tensor and the
	orientations-distribution tensor; $(x, y)$ coordinates of the Flinn and Woodcock plots.
	Comparable older terms in AMS are L and F.
Flinn's k	k = (a-1)/b-1; a measure strain ellipsoid shape from oblate ( $k = 0$ ) through plane
	strain $(k = 1)$ to prolate $k = \infty$ .
Ramsav's K	$K = \ln(a) / \ln(b)$ : $\log_{10}$ scaling of the Flinn plot disperses low anisotropy data points
2	for greater clarity; points separated by similar distances on the log-plot have similar strain-differences.
L-S scheme	Flinn's (1965) qualitative scheme; associates shape or mineral fabrics for a
	homogenous sample of specimens with the appropriate finite-strain or orientation-
	distribution ellipsoid. $L =$ prolate. $L=S$ neutral: S=oblate. general cases. e.g. $L>S$ or
	$L \le S$ Importantly recognizes the smooth spectrum of possibilities vis- $\partial$ -vis
	historically incorrect notion of discrete symmetry classes
$\Omega \Omega$	Orientation Distribution: frequency distribution of avec or directions in three
0D	dimensions illustrated on a standard or by on orientation tensor that is viewelized
	unitensions, musualed on a stereogram of by an orientation tensor that is visualized
	by its magnitude empsoid.

Orthorhombic	Mirror symmetry across three mutually orthogonal planes: no axial-symmetric rotation the planes' intersections; e.g. a magnitude ellipsoid representing for finite strain or AMS. End-member prolate and oblate ellipsoids possess higher, rotational symmetry about one axis. AMS ellipsoids never have less than orthorhombic symmetry whereas most rock-forming minerals have lower crystal symmetry.
Material	Physically characterized line, usually in a continuum, that may be tracked through a
line/plane	strain history, e.g., bedding.
Non-material	A finite strain axis $(X, Y, \text{ or } Z)$ or some other distinct linear property (e.g., line of no
line	finite strain) defined by the state of strain at any point in a strain history. While their orientation may be determined they are rarely tied to any material line (one exception would be <i>incremental</i> strain axes during simple shear strain history).
Deformation	Changes in location of parts of a material with respect to an external reference frame. May comprise any combination of: (i) translation (ii) rigid body rotation (iii) strain (iv) volume change.
Deform.	Material processes by which internal relative displacements are achieved; including
Mechanism	crystal-plasticity, diffusion, pressure solution, particulate flow, etc.
	A strain-history or fabric-evolution in which the orthogonal principal axes remain
Co-axial	parallel to the same material lines as events progress; including pure shear or compaction $(X=Y>1>Z)$ or general coaxial flattening $X>Y>1>Z$ ; cf. non-coaxial. Older terms irrotational/rotational may be confused with the internal rotation of material lines during coaxial strain history or even with external rigid-body rotation.
Vorticity	The rate and sense of finite strain axis rotation (in some complex three-dimensional manner), usually with respect to the rate of accumulation of strain increments. Usually very difficult to relate to the orientation of material lines.
PDO	Preferred dimensional orientation, for example of strained objects such as pebbles, grains or any other clasts, fossils, lapilli ( <i>L-S</i> scheme).
PCO	Preferred crystallographic orientation, for example an alignment of minerals by growth, rotation or solid-state plastic deformation into a linear-planar fabric ( $L$ - $S$ scheme).

Appendix 2- Sub-Areas Sample Location, Age, and Formation Data

Sample	Location	Easting	Northing	Bed dip dir.	Bed Dip	Age(Ma)	Biostrat	Formation
тно1	Lymbia	538565	3872933	257	30	54.0	Kahler	Lower Marl
TH02	Lymbia	538608	3872942	257	30	55.0	Kahler	Lower Marl
ТН03	Lymbia	538609	3872942	257	30	56.0	Kahler	Lower Marl
TH04	Lymbia	538657	3874592	330	5	48.0-62.0		Lower Marl
TH05	Lymbia	538595	3874584	330	5	48.0-62.0		Lower Marl
TH06	Lymbia	538702	3874601	330	5	48.0-62.0		Lower Marl
TH07	Omodhos/Pakhna	483117	3858097	190	20	47.4	Kahler	Chalk & Chert
TH08	Omodhos/Pakhna	483117	3858097	190	10	47.2	Kahler	Chalk & Chert
TH09	Omodhos/Pakhna	483117	3858097	190	10	47.0	Kahler	Chalk & Chert
TH10	Omodhos/Pakhna	483105	3858125	190	10	47.5	Kahler	Chalk & Chert
TH11	Omodhos/Pakhna	482954	3857920	165	16	46.8	Kahler	Chalk & Chert
TH12	Omodhos/Pakhna	482890	3857897	140	12	46.6	Kahler	Chalk & Chert
TH13	Omodhos/Pakhna	482768	3857827	90	25	46.4	Kahler	Chalk & Chert
TH14	Omodhos/Pakhna	482677	3857772	180	26	46.0	Kahler	Chalk
TH15	Omodhos/Pakhna	482630	3857730	135	18	44.0	Kahler	Chalk
TH16	Omodhos/Pakhna	482630	3857730	140	14	43.0	Kahler	Chalk
TH17	Omodhos/Pakhna	482608	3857728	170	5	42.0	Kahler	Chalk
TH18	Omodhos/Pakhna	482581	3857686	225	26	41.0	Kahler	Chalk
TH19	Omodhos/Pakhna	482541	3857655	280	17	39.0	Kahler	Chalk
TH20	Omodhos/Pakhna	482541	3857655	280	17	38.0	Kahler	Chalk
TH21	Omodhos/Pakhna	482485	3857615	72	22	37.0	Kahler	Chalk
TH22	Omodhos/Pakhna	482485	3857615	124	18	36.3	Kahler	Chalk
TH23	Omodhos/Pakhna	482260	3855916	0	0	16.7	Eaton	Pakhna
TH24	Omodhos/Pakhna	482702	3854857	232	18	16.4	Eaton	Pakhna
TH25	Omodhos/Pakhna	481968	3854090	250	10	16.0	Eaton	Pakhna
TH26	Omodhos/Pakhna	481799	3853866	195	15	15.9	Eaton	Pakhna
TH27	Omodhos/Pakhna	481800	3853871	220	10	15.9	Eaton	Pakhna
TH28	Omodhos/Pakhna	481795	3853870	210	14	15.8	Eaton	Pakhna
TH29	Omodhos/Pakhna	481721	3853872	250	12	15.8	Eaton	Pakhna
TH30	Omodhos/Pakhna	481644	3853878	238	8	15.7	Eaton	Pakhna
TH31	Omodhos/Pakhna	481365	3852838	180	14	15.6	Eaton	Pakhna
TH32	Omodhos/Pakhna	481369	3852839	204	12	15.5	Eaton	Pakhna
TH33	Omodhos/Pakhna	482152	3850455	130	6	15.4	Eaton	Pakhna
TH34	Omodhos/Pakhna	481815	3850150	150	8	15.0	Eaton	Pakhna
TH35	Omodhos/Pakhna	481641	3849934	190	6	14.5	Eaton	Pakhna
TH36	Omodhos/Pakhna	481618	3849757	0	0	14.0	Eaton	Pakhna
TH37	Omodhos/Pakhna	481411	3849429	200	14	13.5	Eaton	Pakhna
TH38	Omodhos/Pakhna	481306	3849116	180	6	13.0	Eaton	Pakhna
TH39	Omodhos/Pakhna	481306	3849116	190	8	12.0	Eaton	Pakhna
TH40	Omodhos/Pakhna	481520	3848443	150	14	11.5	Eaton	Pakhna
TH41	Omodhos/Pakhna	481469	3848371	200	10	10.0	Eaton	Pakhna
TH42	Omodhos/Pakhna	481416	3848302	192	4	7.0	Eaton	Pakhna
TH43	Omodhos/Pakhna	481549	3848911	190	5	9.0	Eaton	Pakhna
TH44	Omodhos/Pakhna	481469	3848075	185	5	5.5	Eaton	Pakhna
TH45	Galataria	465074	3858155	195	16	48.0-62.0		Chalk & Chert
TH46	Galataria	465261	3858254	200	6	48.0-62.0	1	Chalk & Chert
TH47	Galataria	464796	3859414	15	38	48.0-62.0	i	Chalk & Chert

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Appendix 2- Sub-Areas Location, Age, and Formation Data

Sample	Location	Easting	Northing	Bed dip dir.	Bed Dip	Age(Ma)	Biostrat	Formation
TH48	Galataria	464970	3860581	25	18	48.0-62.0		Chalk & Chert
TH49	Galataria	465306	3859634	0	6	48.0-62.0		Chalk & Chert
TH50	Lefkara	526308	3858718	300	18	51.5	Kahler	Chalk & Chert
TH51	Lefkara	526406	3858800	110	24	50.5	Kahler	Chalk & Chert
TH52	Lefkara	528093	3857690	140	4	52.0	Kahler	Chalk & Chert
TH53	Lefkara	528315	3857433	145	8	53.0	Kahler	Chalk & Chert
TH54	Lefkara	527279	3858301	100	4	51.0	Kahler	Chalk & Chert
TH55	Lefkara	527361	3858247	130	6	50.0	Kahler	Chalk & Chert
TH56	Lefkara	527430	3858164	0	0	49.0	Kahler	Chalk & Chert
TH57	Lefkara	527494	3858072	0	4	48.5	Kahler	Chalk & Chert
TH58	Lefkara	527592	3857999	50	8	48.0	Kahler	Chalk & Chert
TH59	Lefkara	527547	3858094	0	0	20.4	Kahler	Upper Mari
TH60	Lefkara	527547	3858094	0	Õ	19.0	Kahler	Upper Marl
TH61	Lefkara	527648	3857986	326	18	18.0	Kahler	Upper Marl
TH62	Lefkara	527676	3857932	0	0	17.1	Kahler	Upper Marl
GBPOI 01	Polis Rift	441868	3876978	Ŭ	U		T Carnot	oppor man
GBPOL02	Polis Rift	441868	3876978					
GBPOL03	Polis Rift	441532	3876016					
GBPOL 04	Polis Rift	441266	3876012					
GBPOL05	Polis Rift	439874	3876114					
GBPOL06	Polis Rift	440987	3876061					
GBPOL07	Polis Rift	440007	3875674					
GBPOL 08	Polis Rift	440681	3874880					
GBPOL 09	Polis Rift	441100	3875061					
GBPOI 10	Polis Rift	441822	3874616					
GBPOL 11	Polis Rift	442151	3874276					
GBPOI 12	Polis Rift	442258	3874179					
GBPOL13	Polis Rift	442493	3873918					
GBPOL 14	Polis Rift	442495	3874895					
GBPOI 15	Polis Valley	445073	3875632			<5.0		
GBPOI 16	Polis Valley	445062	3875477			<5.0		
GBPOI 17	Polis Rift	444856	3874862			0.0		
GBPOI 18	Polis Rift	444348	3873809					
GBPOI 19	Polis Rift	444348	3873809					
GBPOL20	Polis Valley	442801	3877925			<5.0		
GBPOI 21	Polis Rift	442694	3877173			0.0		
GBPOI 22	Polis Rift	442605	3877100					
GBPOI 23	Polis Riff	442402	3877051					
GBPOI 24	Polis Valley	446177	3875736			<5.0		
GBPOL25	Polis Rift	444143	3873158			-0.0		
GBPOL26	Polis Rift	443735	3872960					
GBPOI 27	Polis Rift	443925	3873366					
GBPOI 28	Polis Rift	445295	3869120					
GBPOI 29	Polis Rift	445225	3867153					
GBPOI 30	Polis Riff	445458	3866842					
GBPOI 31	Polis Rift	447340	3865758					
GBPOL32	Polis Rift	447627	3865733					

## Appendix 2- Sub-Areas Location, Age, and Formation Data

Sample	Location	Easting	Northing	Bed dip dir.	Bed Dip	Age(Ma)	<b>Biostrat Formation</b>
GBPOL33	Polis Rift	447407	3865516				
GBPOL34	Polis Rift	448175	3865606				
GBPOL35	Polis Valley	448595	3865773			<5.0	
GBPOL36	Polis Rift	446206	3867798				
GBPOL37	Polis Rift	446309	3868351				
GBPOL38	Polis Rift	446526	3868256				
GBPOL39	Polis Rift	445816	3868164				
GBPOL40	Polis Valley	447522	3868164			<5.0	
GBPOL41	Polis Valley	447826	3868116			<5.0	
GBPOL42	Polis Valley	449115	3869115			<5.0	
GBPOL43	Polis Valley	449968	3870034			<5.0	
GBPOL44	Polis Valley	449791	3870090			<5.0	
GBPOL45	Polis Valley	449805	3869818			<5.0	
GBPOL46	Polis Valley	450222	3869057			<5.0	
GBPOL47	Polis Valley	448426	3871457			<5.0	
GBPOL48	Polis Valley	448820	3871588			<5.0	
GBPOL49	Polis Valley	448937	3872088			<5.0	
GBPOL50	Polis Valley	452707	3871759			<5.0	
GBPOL51	Polis Rift	453290	3871780				
GBPOL52	Polis Rift	454124	3871811				
GBPOL53	Polis Rift	455012	3872117				
GBPOL54	Polis Rift	438716	3876167				
GBPOL55	Polis Rift	441934	3875067				
GBPOL56	Polis Rift	441827	3874627				
GBPOL57	Polis Rift	442318	3875105				
GBPOL58	Polis Rift	442993	3875005				
GBPOL59	Polis Rift	443120	3875233				
GBPOL60	Polis Rift	443348	3875695				
GBPOL61	Polis Rift	443677	3876077				
GBPOL62	Polis Valley	444337	3876452			<5.0	

Appendix 3 -	Sub-Areas	Magnetic	Fabric D	)ata

	μSI	μSI	μSI		μSI	_			0=para
Samples	Kmax	Kint	ł	Kmin	Kmean		Pj	т	1=diamag
1 GBPOL15A	1.031	0.988		0.980	166	1.	056	-0.668	0
2 GBPOL15B	1.009	1.002		0.988	154	1.	021	0.317	0
3 GBPOL16A	1.038	1.010	) (	0.953	49	1.	090	0.352	0
4 GBPOL16B	1.036	1.002		0.962	50	1.	077	0.099	0
5 GBPOL16C	1.017	1.004		0.978	50	1.	040	0.308	0
6 GBPOL16D	1.044	0.988	; (	0.968	55	1.	080	-0.462	0
7 GBPOL20A	1.024	1.009	) i	0.966	133	1.	062	0.498	0
8 GBPOL20B	1.028	1.012		0.959	143	1.	075	0.547	0
9 GBPOL20C	1.021	1.018	<b>;</b> 1	0.961	142	1.	070	0.908	0
10 GBPOL24A	1.007	1.001	I	0.990	52	1.	017	0.337	0
11 GBPOL24B	1.003	0.999	) (	0. <b>9</b> 97	51	1.	005	-0.332	0
12 GBPOL24B	1.014	0.999	) (	0.985	51	1.	029	-0.060	0
13 GBPOL24C	1.014	1.010	} 1	0.976	49	1.	042	0.793	0
14 GBPOL35A	1.117	1.014	. 1	0.882	10	1.	267	0.177	1
15 GBPOL35B	1.070	0.991		0.941	10	1.	137	-0.201	1
16 GBPOL35C	1.072	1.001	1	0.930	9	1.	152	0.035	1
17 GBPOL35D	1.063	0.986	j I	0.952	11	1.	118	-0.361	1
18 GBPOL40A	1.566	0.963	; (	0.662	1	2.	401	-0.129	0
19 GBPOL40B	1.216	1.013		0.810	2	1.	503	0.100	0
20 GBPOL40C	1.097	0.993	. 1	0.917	10	1.	196	-0.114	1
21 GBPOL40D	1.187	0.971	I	0.867	11	1.	376	-0.281	1
22 GBPOL41A	1.085	1.032		0.891	17	1.	226	0.492	0
23 GBPOL41B	1.085	1.032		0.891	17	1.	226	0.492	0
24 GBPOL41C	1.031	1.004	. 1	0.965	15	1.	068	0.215	0
25 GBPOL42A	1.007	1.000	)	0.991	257	1.	016	0.146	0
26 GBPOL42B	1.006	1.003		0.990	426	1.	017	0.602	0
27 GBPOL42C	1.011	1.002		0.985	191	1.	026	0.325	0
28 GBPOL42D	1.006	1.002		0.990	510	1.	017	0.497	0
29 GBPOL43A	1.003	0.999	) 1	0.997	95	1.	006	-0.332	0
30 GBPOL43B	1.013	0.999		0.987	79	1.	026	-0.042	0
31 GBPOL44A	2.790	1.001	-	0.358	1	1.	026	-0.042	0
32 GBPOL44B	1.823	1.002	_	0.547	1	1.	026	-0.042	0
33 GBPOL45A	1.127	1.014	. 4	0.873	3	1.	292	0.173	1
34 GBPOL45B	1.218	1.035		0.792	3	1.	547	0.245	1
35 GBPOL45C	1.111	0.995		0.903	4	1.	231	-0.060	1
36 GBPOL45D	3.262	1.565		0.195	2	24.	052	0.478	1
37 GBPOL46A	1.009	1.004	. (	0.986	319	1.	024	0.592	0
38 GBPOL46B	1.025	0.988	. (	0.986	157	1.	045	-0.902	0
39 GBPOL46B	1.005	0.997		0.996	155	1.	009	-0.714	0
40 GBPOL46C	1.004	1.003	. (	0.992	204	1.	013	0.983	0
41 GBPOL47A	1.072	1.014	. (	0.918	10	1.	170	0.285	1
42 GBPOL47B	1.055	1.027		0.922	10	1.	153	0.593	1
43 GBPOL47C	1.116	0.976		0.917	10	1.	222	-0.358	1
44 GBPOL48A	1.010	1.005		0.984	504	1.	027	0.601	0
45 GBPOL48B	1.013	1.007	· (	0.979	462	1.	036	0.679	0
46 GBPOL49A	1.009	1.000		0.990	136	1.	018	0.044	0
47 GBPOL49B	1.019	0.997		0.983	123	1.	037	-0.192	0
48 GBPOL49C	1.020	0.994	(	0.984	127	1.	037	-0.472	0
49 GBPOL50A	1.008	1.002	(	0.989	334	1.	019	0.347	0

Appendix	3 - Sub-Area	as Magnetic	Fabric Data

	μSI	μSI	μSI		μSI			0=para
Samples	Kmax	Kint		Kmin	Kmean	Pj	т	1=diamag
50 GBPOL50B	1.007	0.998		0.993	548	1.014	-0.340	0
51 GBPOL50C	1.008	0.998		0.993	431	1.015	-0.289	0
52 GBPOL62A	1.090	1.002		0.914	11	1.192	0.043	0
53 GBPOL62B	1.035	0.990		0.975	13	1.064	-0.489	0
1 GBPOL01A	1.020	0.998		0.980	95	1.040	-0.096	0
2 GBPOL01B	1.017	0.996		0.986	184	1.031	-0.387	0
3 GBPOL01C	1.009	0.998		0.992	94	1.017	-0.246	0
4 GBPOL02A	1.100	0.990		0.917	29	1.199	-0.164	0
5 GBPOL02B	1.021	1.000		0.978	42	1.043	0.010	0
6 GBPOL02C	1.050	1.034		0.920	38	1.155	0.773	0
7 GBPOL02D	1.034	1.000		0.966	38	1.070	0.016	0
8 GBPOL03A	1.084	1.023		0.901	24	1.208	0.373	1
9 GBPOL03B	1.028	0.989		0.982	25	1.051	-0.661	1
10 GBPOL03C	1.042	0.998		0.961	27	1.084	-0.071	1
11 GBPOL04A	1.725	1.137		0.509	2	3.568	0.316	1
12 GBPOL04B	1.371	0.968		0.753	3	1.834	-0.162	1
13 GBPOL04C	1.073	1.009		0.923	4	1.163	0.179	1
14 GBPOL04D	1.209	1.033		0.799	5	1.520	0.241	1
15 GBPOL04E	1.289	0.892		0.868	4	1.558	-0.858	1
16 GBPOL04F	1.300	1.111		0.692	4	1.938	0.502	1
17 GBPOL05A	1.257	0.933		0.852	2	1.505	-0.533	1
18 GBPOL05B	1.032	0.995		0.972	30	1.062	-0.208	1
19 GBPOL05C	1.056	0.997		0.949	28	1.113	-0.071	1
20 GBPOL05D	1.056	1.023		0.924	29	1,149	0.512	1
21 GBPOL06A	1.181	1.062		0.796	7	1.505	0,459	1
22 GBPOL06B	1,106	0.998		0.904	7	1.224	-0.017	1
23 GBPOL06C	1.082	0.990		0.932	8	1,161	-0.196	1
24 GBPOL07A	1.049	0.990		0.961	34	1.092	-0.314	0
25 GBPOL07B	1.017	1.001		0.981	38	1.037	0.151	0
26 GBPOL07C	1.067	0.990		0.945	24	1.130	-0.239	0
27 GBPOL07D	1.015	1.004		0.979	28	1.037	0.407	0
28 GBPOL07E	1.073	0.999		0.931	29	1.152	-0.013	0
29 GBPOL07F	1.073	1.013		0.919	28	1.169	0.263	0
30 GBPOL08A	1.075	1.019		0.911	23	1.184	0.352	1
31 GBPOL08B	1.054	0.979		0.967	25	1.097	-0.717	1
32 GBPOL08C	1.092	0.992		0.922	26	1.184	-0.141	1
33 GBPOL08D	1.068	1.021		0.916	27	1.171	0.413	1
34 GBPOL09A	1,190	0.978		0.858	10	1.391	-0.201	0
35 GBPOL09B	1.312	0.888		0.857	9	1.606	-0.834	0
36 GBPOL10A	1.109	1.037		0.868	4	1.288	0.449	1
37 GBPOL10B	1.468	1.129		0.602	2	2.533	0.411	1
38 GBPOL11A	1.015	1.002		0.982	30	1.034	0.207	1
39 GBPOL11B	1.013	1.000		0.986	30	1.026	0.006	1
40 GBPOL11C	1.023	1.001		0.975	27	1.048	0.088	1
41 GBPOL12A	1.029	0.994		0.977	28	1.054	-0.322	1
42 GBPOL12B	1.021	1.003		0.975	28	1.047	0.241	1
43 GBPOL12C	1.035	1.005		0.960	26	1.078	0.217	1
44 GBPOL13A	1.038	1.000		0.962	23	1.078	0.018	1
45 GBPOL13B	1.044	0.982		0.974	24	1.079	-0.758	1

Appendix 3 -	Sub-Areas	Magnetic	Fabric	Data

	μSI	μSI	μSI	μSI			0=para
Samples	Kmax	Kint	Kmin	Kmean	Pj	т	1=diamag
46 GBPOL13C	1.014	0.998	0.986	24	1.028	-0.136	1
47 GBPOL13D	1.013	0.997	0.989	25	1.024	-0.329	1
48 GBPOL14A	1.031	0.993	0.975	28	1.058	-0.363	1
49 GBPOL14B	1.014	1.003	0.982	28	1.033	0.340	1
50 GBPOL14C	1.060	1.023	0.920	27	1.158	0.500	1
51 GBPOL17A	1.025	0.990	0.983	43	1.045	-0.661	0
52 GBPOL17B	1.037	1.033	0.932	44	1.129	0.919	0
53 GBPOL17C	1.038	0.990	0.972	45	1.070	-0.454	0
54 GBPOL17D	1.028	1.003	0.968	47	1.063	0.187	0
55 GBPOL17E	1.029	0.997	0.973	46	1.057	-0.141	0
56 GBPOL18A	1.064	1.004	0.935	11	1.139	0.098	1
57 GBPOL18B	1.274	0.958	0.818	10	1.569	-0.289	1
58 GBPOL18C	1.054	1.007	0.941	16	1.121	0.185	1
59 GBPOL19A	1.017	0.995	0.987	27	1.031	-0.495	1
60 GBPOL19B	1.045	0.999	0.957	26	1.092	-0.022	1
61 GBPOL19C	1.093	0.986	0.926	27	1.182	-0.251	1
62 GBPOL19D	1.036	0.991	0.972	26	1.067	-0.399	1
63 GBPOL21A	1.014	1.003	0.981	45	1.034	0.340	0
64 GBPOI 21B	1.075	0.974	0.954	34	1.136	-0.650	0
65 GBPOI 21C	1 029	0.988	0.982	35	1.052	-0.760	0
66 GBPOI 22A	1.020	1 001	0.927	39	1 160	0.037	Ō
67 GBPOI 22B	1.301	1.001	0.604	31	2 420	0.939	0
68 GBPOI 22B	1.001	1 004	0.960	34	1 079	0.000	0
69 GBPOI 234	1.000	0.994	0.000	64	1 055	-0.342	Õ ·
70 GBPOI 238	1.020	0.00	0.070	62	1 025	-0 119	0
71 GBPOL23C	1 004	1 000	0.995	62	1 009	0.002	0
72 GBPOI 23D	1.004	0 997	0.000	63	1 021	-0.381	õ
73 GBPOI 23E	1.011	0.007	0.001	64	1 017	-0.087	õ
74 GBPOI 254	1.000	1 016	0.001	29	1 138	0.378	1
75 GRDOI 258	1.000	1.010	0.001	20	1.100	0.013	1
76 GBPOI 250	1.027	1.000	0.072	28	1.000	0.010	1
77 GBPOL250	1.010	1.000	0.903	20	1.021	0.000	1
	1.020	0 007	0.907	30	1.002	-0 143	1
	1.055	1 010	0.970	30	1 140	0.140	1
	1 000	1.013	0.323	29	1 222	0.440	1
81 GBPOL20C	1.034	1.010	0.097	23	1 032	0.274	1
82 GROUT	1.013	1.001	0.900	20	1.002	0.113	1
82 GBPOL27D	1.020	0.000		23	1.040	_0.241	1
84 GBPOL2/C	1.041	0.990	0.909	17	1.070	-0.558	1
85 GRDOL20A	1.040	1 016		24	1.007	0.530	1
	1.030	1.010	0.949	24	1.030	0.553	1
	1.010	1.007	0.970	22	1.042	0.002	1
07 GDPULSUA	1.020	1.000	0.9/0	20	1.007	0.200	1
	1.104	1.013	0.093	20	1 1 2 2 2	0.107	1
	1.079	1.013		21	1.100	0.239	1
SU GBPOLSUD	1.031	0.992	0.977	20	1.000	-0.444	1
91 GBPUL31A	1.076	1.032	0.899	20	1.200	0.002	1
92 GBPOL31B	1.140	0.956	0.91/	20	1.200		1
93 GBPOL31C	1.025	1.010	0.965	20	1.064	0.511	ا م
94 GBPOL31D	1.113	1.029	0.872	19	1.284	0.358	1

Appendix 3 -	<ul> <li>Sub-Areas I</li> </ul>	Magnetic	Fabric Data

Samples         Kmax         Kint         Kmein         Kmean         Pj         T<		μSI	μSI	μSI		μSI			0=para
96 GBPOL32A       1.178       1.021       0.831       15       1.421       0.179       1         96 GBPOL32D       1.087       0.984       0.933       15       1.261       0.198       1         97 GBPOL32D       1.092       1.008       0.907       16       1.204       0.142       1         99 GBPOL33A       1.051       0.983       0.967       25       1.098       0.023       1         100 GBPOL33B       1.099       1.003       0.906       23       1.213       0.048       1         102 GBPOL33C       1.131       1.022       0.864       22       1.313       0.250       1         103 GBPOL33E       1.030       0.998       0.971       25       1.060       -0.052       1         106 GBPOL34B       1.027       1.000       0.972       10       1.056       0.013       1         106 GBPOL34A       1.027       1.000       0.972       10       1.056       0.033       1         106 GBPOL34A       1.027       1.000       0.956       22       1.088       0.021       1         106 GBPOL34A       1.021       1.041       0.966       226       1.082       0.542	Samples	Kmax	Kint		Kmin	Kmean	Pj	Т	1=diamag
96       GBPOL32E       1.113       1.015       0.884       15       1.211       0.198       1         97       GBPOL32C       1.092       1.008       0.907       16       1.204       0.142       1         99       GBPOL33A       1.051       0.983       0.967       25       1.091       -0.607       1         100       GBPOL33C       1.047       1.000       0.953       25       1.098       0.023       1         101       GBPOL33E       1.030       0.996       0.971       25       1.060       -0.062       1         103       GBPOL34F       1.026       0.998       0.975       21       1.051       -0.079       1         105       GBPOL34F       1.027       1.000       0.975       21       1.056       0.013       1         106       GBPOL34B       1.031       0.042       0.884       10       1.252       0.322       1         106       GBPOL36A       1.031       0.976       22       1.082       0.542       1         109       GBPOL37A       1.051       0.986       0.945       12       1.163       0.647       1         109       <	95 GBPOL32A	1. <b>1</b> 78	1.021		0.831	15	1.421	0.179	1
97 GBPOL32C       1.087       0.984       0.933       15       1.168       -0.299       1         98 GBPOL32D       1.092       1.008       0.907       16       1.204       0.142       1         199 GBPOL33A       1.051       0.983       0.967       25       1.091       -0.607       1         100 GBPOL33C       1.047       1.000       0.953       25       1.098       0.023       1         103 GBPOL33E       1.030       0.998       0.971       25       1.060       -0.052       1         104 GBPOL33F       1.026       0.998       0.972       10       1.056       -0.079       1         105 GBPOL34A       1.027       1.000       0.972       10       1.056       -0.038       1         105 GBPOL34A       1.021       0.969       0.945       12       1.163       -0.647       1         106 GBPOL34A       1.021       1.000       0.956       22       1.082       0.542       1         106 GBPOL34A       1.051       1.031       0.922       20       1.152       0.327       1         106 GBPOL34A       1.051       1.031       0.922       1.152       0.542       1	96 GBPOL32B	1.113	1.015		0.884	15	1.261	0.198	1
98 GBPOL32D       1.092       1.008       0.907       16       1.204       0.407       1         99 GBPOL33B       1.099       1.003       0.906       23       1.213       0.048       1         101 GBPOL33E       1.047       1.000       0.953       25       1.098       0.023       1         102 GBPOL33D       1.131       1.022       0.864       22       1.313       0.250       1         103 GBPOL33E       1.026       0.998       0.971       25       1.060       -0.052       1         104 GBPOL34F       1.027       1.000       0.972       10       1.056       0.013       1         106 GBPOL34C       1.090       0.969       0.945       12       1.163       -0.647       1         108 GBPOL36A       1.031       1.072       0.884       10       1.252       0.322       1         110 GBPOL36A       1.031       0.956       22       1.082       0.542       1         110 GBPOL37B       1.066       1.031       0.922       1.152       0.719       1         112 GBPOL37A       1.051       1.031       0.922       1.152       0.714       1         113 GBPOL38A <td>97 GBPOL32C</td> <td>1.087</td> <td>0.984</td> <td></td> <td>0.933</td> <td>15</td> <td>1.168</td> <td>-0.299</td> <td>1</td>	97 GBPOL32C	1.087	0.984		0.933	15	1.168	-0.299	1
99         GBPOL33A         1.051         0.983         0.967         25         1.091         -0.647         1           100         GBPOL33C         1.047         1.000         0.953         25         1.098         0.023         1           102         GBPOL33C         1.047         1.000         0.953         25         1.060         -0.652         1           103         GBPOL33F         1.026         0.998         0.975         21         1.051         -0.079         1           106         GBPOL34F         1.027         1.000         0.975         21         1.056         0.013         1           106         GBPOL34F         1.027         1.000         0.975         21         1.056         0.013         1           106         GBPOL34C         1.090         0.969         0.945         12         1.163         -0.647         1           108         GBPOL34C         1.061         0.998         0.943         12         1.163         -0.647         1           110         GBPOL34C         1.061         0.958         23         1.088         0.021         1           110         GBPOL368         1.021	98 GBPOL32D	1.092	1.008		0.907	16	1.204	0.142	1
100 GBPOL33E       1.099       1.003       0.906       23       1.213       0.048       1         101 GBPOL33C       1.047       1.000       0.953       25       1.098       0.023       1         102 GBPOL33E       1.030       0.998       0.971       25       1.060       -0.052       1         103 GBPOL33E       1.026       0.998       0.972       10       1.056       0.013       1         106 GBPOL34B       1.027       1.000       0.972       10       1.056       0.013       1         106 GBPOL34B       1.021       0.898       0.943       12       1.163       -0.647       1         106 GBPOL34D       1.061       0.998       0.943       12       1.162       0.038       1         106 GBPOL34D       1.061       0.998       0.943       12       1.162       0.542       1         110 GBPOL34D       1.061       0.998       0.943       12       1.162       0.542       1         111 GBPOL37A       1.051       1.031       0.922       20       1.152       0.719       1         112 GBPOL38A       1.042       0.996       0.962       26       1.082       0.124	99 GBPOL33A	1.051	0.983		0.967	25	1.091	-0.607	1
101 GBPOL33C       1.047       1.000       0.953       25       1.098       0.023       1         102 GBPOL33D       1.131       1.022       0.864       22       1.313       0.250       1         103 GBPOL33F       1.026       0.998       0.975       21       1.051       -0.079       1         105 GBPOL34A       1.027       1.000       0.972       10       1.056       0.013       1         106 GBPOL34C       1.090       0.969       0.945       12       1.163       -0.647       1         108 GBPOL34C       1.061       0.998       0.943       12       1.126       -0.038       1         109 GBPOL36A       1.031       0.956       22       1.012       0.719       1         110 GBPOL37B       1.061       1.031       0.922       20       1.152       0.719       1         111 GBPOL38A       1.031       1.094       0.963       27       1.072       0.174       1         113 GBPOL38A       1.033       1.004       0.963       27       1.072       0.174       1         115 GBPOL38A       1.031       1.006       0.962       26       1.073       0.348       1     <	100 GBPOL33B	1.099	1.003		0.906	23	1.213	0.048	1
102 GBPOL33D       1.131       1.022       0.864       22       1.313       0.250       1         103 GBPOL33E       1.030       0.998       0.971       25       1.060       -0.052       1         104 GBPOL33F       1.026       0.998       0.975       21       1.056       0.013       1         105 GBPOL34A       1.027       1.000       0.972       10       1.056       0.013       1         106 GBPOL34D       1.061       0.998       0.945       12       1.163       -0.647       1         108 GBPOL36A       1.031       0.916       22       1.082       0.542       1         110 GBPOL37A       1.051       1.031       0.922       20       1.152       0.719       1         113 GBPOL37A       1.056       1.006       0.931       21       1.144       0.136       1         114 GBPOL38A       1.019       0.997       0.983       27       1.037       -0.192       1         114 GBPOL38A       1.031       1.042       0.996       266       1.062       -0.124       1         115 GBPOL38B       1.042       0.996       0.962       26       1.034       1       1 <td>101 GBPOL33C</td> <td>1.047</td> <td>1.000</td> <td></td> <td>0.953</td> <td>25</td> <td>1.098</td> <td>0.023</td> <td>1</td>	101 GBPOL33C	1.047	1.000		0.953	25	1.098	0.023	1
103 GBPOL33E       1.030       0.998       0.971       25       1.060       -0.052       1         104 GBPOL33F       1.026       0.998       0.975       21       1.051       -0.079       1         105 GBPOL34A       1.027       1.000       0.972       10       1.056       0.013       1         106 GBPOL34D       1.061       0.998       0.945       12       1.163       -0.647       1         108 GBPOL36A       1.031       0.916       0.956       22       1.082       0.542       1         110 GBPOL36A       1.031       1.013       0.956       22       1.088       0.021       1         111 GBPOL37B       1.066       1.000       0.958       23       1.088       0.021       1         113 GBPOL38A       1.019       0.997       0.983       27       1.037       -0.192       1         114 GBPOL38A       1.033       1.004       0.962       26       1.073       0.348       1         115 GBPOL38A       1.056       0.989       0.956       21       1.106       -0.312       1         116 GPPOL38A       1.066       0.989       0.970       26       1.076       -0.460 <td>102 GBPOL33D</td> <td>1.131</td> <td>1.022</td> <td></td> <td>0.864</td> <td>22</td> <td>1.313</td> <td>0.250</td> <td>1</td>	102 GBPOL33D	1.131	1.022		0.864	22	1.313	0.250	1
104 GBPOL33F       1.026       0.998       0.975       21       1.051       -0.079       1         105 GBPOL34A       1.027       1.000       0.972       10       1.056       0.013       1         106 GBPOL34C       1.090       0.969       0.945       12       1.163       -0.647       1         108 GBPOL34C       1.091       0.998       0.943       12       1.163       -0.038       1         109 GBPOL36A       1.031       1.013       0.956       22       1.082       0.719       1         110 GBPOL37A       1.051       1.031       0.922       20       1.152       0.719       1         113 GBPOL38A       1.019       0.997       0.983       27       1.037       -0.192       1         114 GBPOL38A       1.033       1.004       0.962       26       1.082       -0.124       1         115 GBPOL38B       1.042       0.996       0.962       21       1.034       1         116 GBPOL38A       1.033       1.004       0.962       26       1.073       0.348       1         116 GBPOL38A       1.055       0.952       21       1.122       -0.341       1	103 GBPOL33E	1.030	0.998		0.971	25	1.060	-0.052	1
105       GBPOL34A       1.027       1.000       0.972       10       1.056       0.013       1         106       GBPOL34C       1.090       0.969       0.945       12       1.163       -0.647       1         107       GBPOL34D       1.061       0.996       0.945       12       1.163       -0.647       1         108       GBPOL3AA       1.061       0.998       0.943       12       1.163       -0.647       1         109       GBPOL3AA       1.031       0.956       22       1.082       0.542       1         110       GBPOL37B       1.066       1.000       0.958       23       1.052       0.719       1         111       GBPOL37B       1.066       1.006       0.931       21       1.144       0.136       1         113       GBPOL38A       1.013       0.9463       27       1.037       0.174       1         115       GBPOL38A       1.033       1.004       0.962       26       1.073       0.348       1         115       GBPOL38A       1.056       0.989       0.952       21       1.122       -0.394       1         116       GBPOL38A	104 GBPOL33F	1.026	0.998		0.975	21	1.051	-0.079	1
106       GBPOL34B       1.103       1.024       0.884       10       1.252       0.322       1         107       GBPOL34C       1.090       0.969       0.945       12       1.163       -0.647       1         108       GBPOL36A       1.031       0.998       0.943       12       1.126       -0.038       1         109       GBPOL36A       1.031       1.013       0.956       22       1.082       0.542       1         110       GBPOL36B       1.042       1.000       0.958       23       1.088       0.021       1         111       GBPOL37B       1.066       1.006       0.931       21       1.144       0.136       1         113       GBPOL38A       1.033       1.004       0.963       27       1.072       0.174       1         116       GBPOL38A       1.031       1.008       0.962       26       1.073       0.348       1         117       GBPOL38A       1.056       0.985       0.952       21       1.122       -0.394       1         119       GBPOL51A       1.064       1.041       0.901       25       1.197       0.727       1	105 GBPOL34A	1.027	1.000		0.972	10	1.056	0.013	1
107       GBPOL34C       1.090       0.969       0.945       12       1.163       -0.647       1         109       GBPOL36A       1.031       1.013       0.956       22       1.082       0.542       1         110       GBPOL36B       1.042       1.000       0.958       23       1.088       0.021       1         111       GBPOL37A       1.051       1.031       0.922       20       1.152       0.719       1         113       GBPOL38A       1.019       0.997       0.983       27       1.037       -0.192       1         114       GBPOL38A       1.019       0.997       0.983       27       1.037       -0.192       1         114       GBPOL38A       1.042       0.996       0.962       26       1.073       0.348       1         116       GBPOL38A       1.056       0.985       0.952       21       1.106       -0.312       1         118       GBPOL51A       1.064       1.041       0.901       25       1.076       -0.460       1         120       GBPOL52A       1.089       0.976       0.939       5       1.166       -0.472       1      1	106 GBPOL34B	1.103	1.024		0.884	10	1.252	0.322	1
108       GBPOL34D       1.061       0.998       0.943       12       1.126       -0.038       1         109       GBPOL36A       1.031       1.013       0.956       22       1.082       0.542       1         110       GBPOL37A       1.051       1.031       0.922       20       1.152       0.719       1         112       GBPOL37B       1.066       1.006       0.931       21       1.144       0.136       1         113       GBPOL38A       1.019       0.997       0.983       27       1.072       0.174       1         115       GBPOL38A       1.033       1.004       0.963       27       1.072       0.174       1         115       GBPOL38A       1.031       1.008       0.962       26       1.073       0.348       1         116       GBPOL39A       1.065       0.985       0.952       21       1.122       -0.394       1         119       GBPOL51A       1.041       0.901       25       1.166       -0.472       1         120       GBPOL52A       1.098       0.976       0.939       5       1.666       -0.472       1         123	107 GBPOL34C	1.090	0.969		0.945	12	1.163	-0.647	1
109 GBPOL36A       1.031       1.013       0.956       22       1.082       0.542       1         110 GBPOL36B       1.042       1.000       0.958       23       1.086       0.021       1         111 GBPOL37A       1.051       1.031       0.922       20       1.152       0.719       1         113 GBPOL38A       1.0019       0.997       0.983       27       1.037       -0.192       1         114 GBPOL38A       1.033       1.004       0.963       27       1.072       0.174       1         115 GBPOL38B       1.042       0.996       0.962       26       1.073       0.348       1         117 GBPOL39A       1.056       0.985       0.952       21       1.122       -0.394       1         120 GBPOL51A       1.041       0.989       0.970       26       1.076       -0.460       1         121 GBPOL51A       1.041       0.991       25       1.197       0.727       1         123 GBPOL52A       1.089       0.976       0.339       5       1.166       -0.472       1         123 GBPOL52B       1.118       0.952       0.938       7       1.214       -0.834       1	108 GBPOL34D	1.061	0.998		0.943	12	1.126	-0.038	1
110       GBPOL36B       1.042       1.000       0.958       23       1.088       0.021       1         111       GBPOL37A       1.051       1.031       0.922       20       1.152       0.719       1         112       GBPOL37A       1.056       1.006       0.931       21       1.144       0.136       1         113       GBPOL38A       1.019       0.997       0.983       27       1.072       0.174       1         115       GBPOL38A       1.033       1.004       0.963       27       1.072       0.174       1         115       GBPOL38B       1.042       0.996       0.962       26       1.062       -0.124       1         116       GBPOL38B       1.042       0.996       0.956       21       1.106       -0.312       1         118       GBPOL39A       1.056       0.989       0.970       26       1.076       -0.460       1         120       GBPOL51A       1.041       0.901       25       1.197       0.727       1         121       GBPOL52A       1.089       0.976       0.575       4       3.219       -0.083       1         125	109 GBPOL36A	1.031	1.013		0.956	22	1.082	0.542	1
111       GBPOL37A       1.051       1.031       0.922       20       1.152       0.719       1         112       GBPOL37B       1.066       1.006       0.931       21       1.144       0.136       1         113       GBPOL38A       1.019       0.997       0.983       27       1.037       -0.192       1         114       GBPOL38A       1.033       1.004       0.963       27       1.072       0.174       1         115       GBPOL38B       1.031       1.008       0.962       26       1.082       -0.124       1         116       GBPOL38C       1.031       1.008       0.962       26       1.073       0.348       1         117       GBPOL38A       1.056       0.989       0.956       21       1.106       -0.312       1         118       GBPOL51A       1.041       0.907       26       1.076       -0.460       1         120       GBPOL51B       1.064       1.041       0.901       25       1.197       0.727       1         121       GBPOL52A       1.089       0.976       0.938       7       1.214       -0.834       1         124	110 GBPOL36B	1.042	1.000		0.958	23	1.088	0.021	1
112       GBPOL37B       1.066       1.006       0.931       21       1.144       0.136       1         113       GBPOL38A       1.019       0.997       0.983       27       1.037       -0.192       1         114       GBPOL38A       1.033       1.004       0.963       27       1.072       0.174       1         115       GBPOL38B       1.042       0.996       0.962       26       1.073       0.348       1         116       GBPOL39A       1.056       0.989       0.956       21       1.106       -0.312       1         118       GBPOL51A       1.041       0.989       0.970       26       1.076       -0.460       1         120       GBPOL51A       1.041       0.989       0.970       26       1.076       -0.460       1         121       GBPOL51B       1.064       1.041       0.901       25       1.166       -0.472       1         122       GBPOL52B       1.118       0.952       0.938       7       1.214       -0.834       1         125       GBPOL52D       1.097       1.019       0.893       6       1.231       0.278       1	111 GBPOL37A	1.051	1.031		0.922	20	1.152	0.719	1
113       GBPOL38A       1.019       0.997       0.983       27       1.037       -0.192       1         114       GBPOL38A       1.033       1.004       0.963       27       1.072       0.174       1         115       GBPOL38B       1.042       0.996       0.962       26       1.082       -0.124       1         116       GBPOL38C       1.031       1.008       0.962       26       1.073       0.348       1         117       GBPOL39A       1.065       0.985       0.952       21       1.122       -0.394       1         119       GBPOL51A       1.041       0.989       0.970       26       1.076       -0.460       1         120       GBPOL51B       1.064       1.041       0.901       25       1.197       0.727       1         121       GBPOL52C       1.074       1.008       0.923       25       1.166       -0.472       1         123       GBPOL52D       1.097       0.575       4       3.219       -0.089       1         125       GBPOL53A       1.029       1.016       0.955       72       1.082       0.670       0         127	112 GBPOL37B	1.066	1.006		0.931	21	1.144	0.136	1
114       GBPOL38A       1.033       1.004       0.963       27       1.072       0.174       1         115       GBPOL38B       1.042       0.996       0.962       26       1.082       -0.124       1         116       GBPOL38C       1.031       1.008       0.962       26       1.073       0.348       1         117       GBPOL39A       1.056       0.989       0.956       21       1.106       -0.312       1         118       GBPOL39B       1.065       0.985       0.952       21       1.122       -0.394       1         120       GBPOL51B       1.064       1.041       0.901       25       1.197       0.727       1         121       GBPOL52A       1.089       0.976       0.939       5       1.166       -0.472       1         123       GBPOL52B       1.118       0.952       0.938       7       1.214       -0.834       1         125       GBPOL52D       1.097       0.967       0.575       4       3.219       -0.089       1         125       GBPOL53A       1.029       1.016       0.955       72       1.082       0.670       0	113 GBPOL38A	1.019	0.997		0.983	27	1.037	-0.192	1
115       GBPOL38B       1.042       0.996       0.962       26       1.082       -0.124       1         116       GBPOL38C       1.031       1.008       0.962       26       1.073       0.348       1         117       GBPOL39A       1.056       0.989       0.956       21       1.106       -0.312       1         118       GBPOL39B       1.065       0.985       0.952       21       1.122       -0.394       1         120       GBPOL51A       1.041       0.989       0.970       26       1.076       -0.460       1         120       GBPOL51C       1.074       1.008       0.923       25       1.164       0.165       1         122       GBPOL52A       1.089       0.976       0.939       5       1.166       -0.472       1         123       GBPOL52D       1.097       1.019       0.893       6       1.231       0.278       1         125       GBPOL52D       1.097       1.019       0.893       6       1.231       0.278       1         126       GBPOL53B       1.027       1.020       0.953       133       1.066       0.468       0	114 GBPOL38A	1.033	1.004		0.963	27	1.072	0.174	1
116       GBPOL38C       1.031       1.008       0.962       26       1.073       0.348       1         117       GBPOL39A       1.056       0.989       0.956       21       1.106       -0.312       1         118       GBPOL39B       1.065       0.985       0.952       21       1.122       -0.394       1         119       GBPOL51A       1.041       0.989       0.970       26       1.076       -0.460       1         120       GBPOL51B       1.064       1.041       0.901       25       1.164       0.165       1         122       GBPOL52A       1.089       0.976       0.939       5       1.166       -0.472       1         123       GBPOL52C       1.796       0.967       0.575       4       3.219       -0.089       1         125       GBPOL53A       1.029       1.016       0.955       72       1.082       0.670       0         127       GBPOL53B       1.027       1.020       0.953       133       1.086       0.804       0         128       GBPOL53B       1.027       1.001       0.964       167       1.066       0.468       0      1	115 GBPOL38B	1.042	0.996		0.962	26	1.082	-0.124	1
117 GBPOL39A       1.056       0.989       0.956       21       1.106       -0.312       1         118 GBPOL39B       1.065       0.985       0.952       21       1.122       -0.394       1         119 GBPOL51A       1.041       0.989       0.970       26       1.076       -0.460       1         120 GBPOL51B       1.064       1.041       0.901       25       1.197       0.727       1         121 GBPOL52A       1.089       0.976       0.939       5       1.166       -0.472       1         123 GBPOL52B       1.118       0.952       0.938       7       1.214       -0.834       1         124 GBPOL52C       1.796       0.967       0.575       4       3.219       -0.089       1         126 GBPOL53B       1.027       1.020       0.953       133       1.086       0.804       0         128 GBPOL53C       1.026       1.009       0.964       167       1.066       0.468       0         129 GBPOL53E       1.015       1.012       0.972       170       1.049       0.841       0         131 GBPOL54A       1.024       1.003       0.972       23       1.053       0.179 <td>116 GBPOL38C</td> <td>1.031</td> <td>1.008</td> <td></td> <td>0.962</td> <td>26</td> <td>1.073</td> <td>0.348</td> <td>1</td>	116 GBPOL38C	1.031	1.008		0.962	26	1.073	0.348	1
118       GBPOL39B       1.065       0.985       0.952       21       1.122       -0.394       1         119       GBPOL51A       1.041       0.989       0.970       26       1.076       -0.460       1         120       GBPOL51B       1.064       1.041       0.901       25       1.197       0.727       1         121       GBPOL51C       1.074       1.008       0.923       25       1.164       0.165       1         122       GBPOL52A       1.089       0.976       0.939       5       1.166       -0.472       1         123       GBPOL52C       1.796       0.967       0.575       4       3.219       -0.089       1         125       GBPOL53A       1.029       1.016       0.955       72       1.082       0.670       0         127       GBPOL53B       1.027       1.020       0.953       133       1.086       0.804       0         128       GBPOL53C       1.026       1.009       0.964       167       1.066       0.468       0         129       GBPOL53E       1.015       1.012       0.972       170       1.049       0.841       0	117 GBPOI 39A	1 056	0.989		0.956	21	1,106	-0.312	1
119       GBPOL51A       1.041       0.989       0.970       26       1.076       -0.460       1         120       GBPOL51B       1.064       1.041       0.901       25       1.197       0.727       1         121       GBPOL51C       1.074       1.008       0.923       25       1.164       0.165       1         122       GBPOL52A       1.089       0.976       0.939       5       1.166       -0.472       1         123       GBPOL52B       1.118       0.952       0.938       7       1.214       -0.834       1         124       GBPOL52C       1.796       0.967       0.575       4       3.219       -0.089       1         125       GBPOL53A       1.029       1.016       0.955       72       1.082       0.670       0         126       GBPOL53B       1.027       1.020       0.953       133       1.086       0.804       0         128       GBPOL53D       1.035       1.001       0.964       167       1.066       0.468       0         130       GBPOL54A       1.024       1.003       0.972       23       1.053       0.179       1	118 GBPOI 39B	1 065	0 985		0.952	21	1.122	-0.394	1
120       GBPOL51B       1.041       0.901       25       1.197       0.727       1         121       GBPOL51C       1.074       1.008       0.923       25       1.164       0.165       1         122       GBPOL52A       1.089       0.976       0.939       5       1.166       -0.472       1         123       GBPOL52B       1.118       0.952       0.938       7       1.214       -0.834       1         124       GBPOL52C       1.796       0.967       0.575       4       3.219       -0.089       1         125       GBPOL53A       1.029       1.019       0.893       6       1.231       0.278       1         126       GBPOL53B       1.027       1.020       0.953       133       1.086       0.804       0         127       GBPOL53D       1.035       1.001       0.964       167       1.066       0.468       0         129       GBPOL53E       1.015       1.012       0.972       170       1.049       0.841       0         130       GBPOL54A       1.024       1.003       0.972       23       1.053       0.179       1         132	119 GBPOI 51A	1 041	0.989		0.970	26	1.076	-0.460	1
121GBPOL51C1.0741.0080.923251.1640.1651122GBPOL52A1.0890.9760.93951.166-0.4721123GBPOL52B1.1180.9520.93871.214-0.8341124GBPOL52C1.7960.9670.57543.219-0.0891125GBPOL52D1.0971.0190.89361.2310.2781126GBPOL53A1.0291.0160.955721.0820.6700127GBPOL53B1.0271.0200.9531331.0860.8040128GBPOL53C1.0261.0090.9641671.0660.4680129GBPOL53D1.0351.0010.9641381.0730.0780130GBPOL53E1.0151.0120.9721701.0490.8410131GBPOL54A1.0241.0030.972231.0530.1791132GBPOL55A1.1001.0140.895151.2300.2101133GBPOL55A1.1001.0140.895151.2300.2101135GBPOL55A1.0060.950171.1010.1991136GBPOL56A1.2010.9910.839101.433-0.0700138GBPOL56A1.2010.9910.839101.433-0.070 </td <td>120 GBPOI 51B</td> <td>1 064</td> <td>1.041</td> <td></td> <td>0.901</td> <td>25</td> <td>1,197</td> <td>0.727</td> <td>1</td>	120 GBPOI 51B	1 064	1.041		0.901	25	1,197	0.727	1
122       GBPOL52A       1.089       0.976       0.939       5       1.161       -0.472       1         123       GBPOL52B       1.118       0.952       0.938       7       1.214       -0.834       1         124       GBPOL52C       1.796       0.967       0.575       4       3.219       -0.089       1         125       GBPOL52D       1.097       1.019       0.893       6       1.231       0.278       1         126       GBPOL53A       1.029       1.016       0.955       72       1.082       0.670       0         127       GBPOL53B       1.027       1.020       0.953       133       1.086       0.804       0         128       GBPOL53C       1.026       1.009       0.964       167       1.066       0.468       0         129       GBPOL53D       1.035       1.001       0.964       138       1.073       0.078       0         130       GBPOL54A       1.024       1.003       0.972       23       1.053       0.179       1         132       GBPOL54A       1.024       1.003       0.972       23       1.052       0.278       1	121 GBPOL51C	1 074	1 008		0.923	25	1 164	0.165	1
123       GBPOL52B       1.118       0.952       0.938       7       1.214       -0.834       1         124       GBPOL52C       1.796       0.967       0.575       4       3.219       -0.089       1         125       GBPOL52D       1.097       1.019       0.893       6       1.231       0.278       1         126       GBPOL53A       1.029       1.016       0.955       72       1.082       0.670       0         127       GBPOL53B       1.027       1.020       0.953       133       1.086       0.804       0         128       GBPOL53D       1.026       1.009       0.964       167       1.066       0.468       0         129       GBPOL53D       1.035       1.001       0.964       138       1.073       0.078       0         130       GBPOL54A       1.024       1.003       0.972       23       1.053       0.179       1         132       GBPOL54A       1.024       1.003       0.972       23       1.053       0.179       1         133       GBPOL55A       1.010       1.048       0.762       18       1.654       0.287       1	122 GBPOI 52A	1 089	0.976		0.939	5	1.166	-0.472	1
124       GBPOL52C       1.796       0.967       0.575       4       3.219       -0.089       1         125       GBPOL52D       1.097       1.019       0.893       6       1.231       0.278       1         126       GBPOL53A       1.029       1.016       0.955       72       1.082       0.670       0         127       GBPOL53B       1.027       1.020       0.953       133       1.086       0.804       0         128       GBPOL53C       1.026       1.009       0.964       167       1.066       0.468       0         129       GBPOL53D       1.035       1.001       0.964       138       1.073       0.078       0         130       GBPOL53E       1.015       1.012       0.972       170       1.049       0.841       0         131       GBPOL54A       1.024       1.003       0.972       23       1.053       0.179       1         132       GBPOL54A       1.024       1.003       0.972       23       1.053       0.287       1         133       GBPOL55A       1.100       1.048       0.762       18       1.654       0.287       1	123 GBPOL 52B	1 118	0.952		0.938	7	1 2 1 4	-0.834	1
125       GBPOL52D       1.097       1.019       0.893       6       1.231       0.278       1         126       GBPOL53A       1.029       1.016       0.955       72       1.082       0.670       0         127       GBPOL53A       1.029       1.016       0.955       72       1.082       0.670       0         127       GBPOL53B       1.027       1.020       0.953       133       1.086       0.804       0         128       GBPOL53C       1.026       1.009       0.964       167       1.066       0.468       0         129       GBPOL53D       1.035       1.001       0.964       138       1.073       0.078       0         130       GBPOL53E       1.015       1.012       0.972       170       1.049       0.841       0         131       GBPOL54A       1.024       1.003       0.972       23       1.053       0.179       1         132       GBPOL54C       1.055       0.990       0.956       20       1.105       -0.278       1         133       GBPOL55A       1.100       1.014       0.895       15       1.230       0.210       1	124 GBPOI 52C	1 796	0.967		0.575	4	3.219	-0.089	1
126       GBPOL53A       1.029       1.016       0.955       72       1.082       0.670       0         127       GBPOL53B       1.027       1.020       0.953       133       1.086       0.804       0         128       GBPOL53C       1.026       1.009       0.964       167       1.066       0.468       0         129       GBPOL53C       1.026       1.009       0.964       138       1.073       0.078       0         130       GBPOL53E       1.015       1.012       0.972       170       1.049       0.841       0         131       GBPOL54A       1.024       1.003       0.972       23       1.053       0.179       1         132       GBPOL54A       1.024       1.003       0.972       23       1.053       0.179       1         132       GBPOL54C       1.055       0.990       0.956       20       1.105       -0.278       1         133       GBPOL55A       1.100       1.014       0.895       15       1.230       0.210       1         135       GBPOL55E       1.045       1.006       0.950       17       1.101       0.199       1	125 GBPOL 52D	1 097	1 019		0.893	6	1.231	0.278	1
127       GBPOL53B       1.027       1.020       0.953       133       1.066       0.804       0         128       GBPOL53C       1.026       1.009       0.964       167       1.066       0.468       0         129       GBPOL53D       1.035       1.001       0.964       138       1.073       0.078       0         130       GBPOL53E       1.015       1.012       0.972       170       1.049       0.841       0         131       GBPOL54A       1.024       1.003       0.972       23       1.053       0.179       1         132       GBPOL54B       1.250       1.048       0.762       18       1.654       0.287       1         133       GBPOL54C       1.055       0.990       0.956       20       1.105       -0.278       1         134       GBPOL55A       1.100       1.014       0.895       15       1.230       0.210       1         135       GBPOL55E       1.045       1.006       0.950       17       1.101       0.199       1         136       GBPOL56A       1.201       0.991       0.839       10       1.433       -0.070       0	126 GBPOL53A	1 029	1 016		0.955	72	1.082	0.670	0
128       GBPOL53C       1.026       1.009       0.964       167       1.066       0.468       0         129       GBPOL53D       1.035       1.001       0.964       138       1.073       0.078       0         130       GBPOL53E       1.015       1.012       0.972       170       1.049       0.841       0         131       GBPOL54A       1.024       1.003       0.972       23       1.053       0.179       1         132       GBPOL54B       1.250       1.048       0.762       18       1.654       0.287       1         133       GBPOL54C       1.055       0.990       0.956       20       1.105       -0.278       1         134       GBPOL55A       1.100       1.014       0.895       15       1.230       0.210       1         135       GBPOL55B       1.170       1.078       0.791       17       1.512       0.582       1         136       GBPOL56A       1.201       0.991       0.839       10       1.433       -0.070       0         137       GBPOL56A       1.201       0.997       0.823       8       1.428       -0.132       0	127 GBPOI 53B	1 027	1 020		0.953	133	1.086	0.804	0
129 GBPOL53D       1.035       1.001       0.964       138       1.073       0.078       0         130 GBPOL53E       1.015       1.012       0.972       170       1.049       0.841       0         131 GBPOL54A       1.024       1.003       0.972       23       1.053       0.179       1         132 GBPOL54B       1.250       1.048       0.762       18       1.654       0.287       1         133 GBPOL54C       1.055       0.990       0.956       20       1.105       -0.278       1         134 GBPOL55A       1.100       1.014       0.895       15       1.230       0.210       1         135 GBPOL55B       1.170       1.078       0.791       17       1.512       0.582       1         136 GBPOL56A       1.201       0.991       0.839       10       1.433       -0.070       0         137 GBPOL56A       1.201       0.991       0.839       10       1.433       -0.021       0         139 GBPOL56C       1.217       0.997       0.823       8       1.480       -0.021       0         140 GBPOL57A       1.038       0.988       0.974       28       1.069       -0.545 <td>128 GBPOL 53C</td> <td>1 026</td> <td>1 009</td> <td></td> <td>0 964</td> <td>167</td> <td>1.066</td> <td>0.468</td> <td>0</td>	128 GBPOL 53C	1 026	1 009		0 964	167	1.066	0.468	0
130 GBPOL53E       1.015       1.012       0.972       170       1.049       0.841       0         131 GBPOL54A       1.024       1.003       0.972       23       1.053       0.179       1         132 GBPOL54B       1.250       1.048       0.762       18       1.654       0.287       1         133 GBPOL54C       1.055       0.990       0.956       20       1.105       -0.278       1         134 GBPOL55A       1.100       1.014       0.895       15       1.230       0.210       1         135 GBPOL55B       1.170       1.078       0.791       17       1.512       0.582       1         136 GBPOL55C       1.045       1.006       0.950       17       1.101       0.199       1         137 GBPOL56A       1.201       0.991       0.839       10       1.433       -0.070       0         138 GBPOL56E       1.203       0.984       0.843       6       1.428       -0.132       0         139 GBPOL56C       1.217       0.997       0.823       8       1.480       -0.021       0         140 GBPOL57A       1.038       0.988       0.974       28       1.069       -0.545	129 GBPOL 53D	1 035	1 001		0.964	138	1.073	0.078	0
131 GBPOL54A       1.024       1.003       0.972       23       1.053       0.179       1         132 GBPOL54B       1.250       1.048       0.762       18       1.654       0.287       1         133 GBPOL54C       1.055       0.990       0.956       20       1.105       -0.278       1         134 GBPOL55A       1.100       1.014       0.895       15       1.230       0.210       1         135 GBPOL55B       1.170       1.078       0.791       17       1.512       0.582       1         136 GBPOL55C       1.045       1.006       0.950       17       1.101       0.199       1         137 GBPOL56A       1.201       0.991       0.839       10       1.433       -0.070       0         138 GBPOL56B       1.203       0.984       0.843       6       1.428       -0.132       0         139 GBPOL56C       1.217       0.997       0.823       8       1.480       -0.021       0         140 GBPOL57A       1.038       0.988       0.974       28       1.069       -0.545       1         141 GBPOL57B       1.047       0.999       0.955       27       1.096       -0.017	130 GBPOL 53E	1 015	1 012		0.972	170	1.049	0.841	0
132 GBPOL54B       1.250       1.048       0.762       18       1.654       0.287       1         133 GBPOL54C       1.055       0.990       0.956       20       1.105       -0.278       1         134 GBPOL55A       1.100       1.014       0.895       15       1.230       0.210       1         135 GBPOL55B       1.170       1.078       0.791       17       1.512       0.582       1         136 GBPOL55C       1.045       1.006       0.950       17       1.101       0.199       1         137 GBPOL56A       1.201       0.991       0.839       10       1.433       -0.070       0         138 GBPOL56B       1.203       0.984       0.843       6       1.428       -0.132       0         139 GBPOL56C       1.217       0.997       0.823       8       1.480       -0.021       0         140 GBPOL57A       1.038       0.988       0.974       28       1.069       -0.545       1         141 GBPOL57B       1.047       0.999       0.955       27       1.096       -0.017       1         142 GBPOL58A       1.042       1.010       0.949       28       1.098       0.328	131 GBPOL 54A	1.074	1 003		0.972	23	1.053	0.179	1
133 GBPOL54C       1.055       0.990       0.956       20       1.105       -0.278       1         134 GBPOL55A       1.100       1.014       0.895       15       1.230       0.210       1         135 GBPOL55B       1.170       1.078       0.791       17       1.512       0.582       1         136 GBPOL55C       1.045       1.006       0.950       17       1.101       0.199       1         137 GBPOL56A       1.201       0.991       0.839       10       1.433       -0.070       0         138 GBPOL56B       1.203       0.984       0.843       6       1.428       -0.132       0         139 GBPOL56C       1.217       0.997       0.823       8       1.480       -0.021       0         140 GBPOL57A       1.038       0.988       0.974       28       1.069       -0.545       1         141 GBPOL57B       1.047       0.999       0.955       27       1.096       -0.017       1         142 GBPOL58A       1.042       1.010       0.949       28       1.098       0.328       1         143 GBPOL58B       1.073       1.020       0.912       9       1.180       0.368	132 GBPOI 54B	1 250	1 048		0 762	18	1.654	0.287	1
134 GBPOL55A       1.100       1.014       0.895       15       1.230       0.210       1         135 GBPOL55B       1.170       1.078       0.791       17       1.512       0.582       1         136 GBPOL55C       1.045       1.006       0.950       17       1.101       0.199       1         137 GBPOL56A       1.201       0.991       0.839       10       1.433       -0.070       0         138 GBPOL56B       1.203       0.984       0.843       6       1.428       -0.132       0         139 GBPOL56C       1.217       0.997       0.823       8       1.480       -0.021       0         140 GBPOL57A       1.038       0.988       0.974       28       1.069       -0.545       1         141 GBPOL57B       1.047       0.999       0.955       27       1.096       -0.017       1         142 GBPOL58A       1.042       1.010       0.949       28       1.098       0.328       1         143 GBPOL58B       1.073       1.020       0.912       9       1.180       0.368       1	133 GBPOI 54C	1.055	0 990		0.956	20	1.105	-0.278	1
135 GBPOL55B       1.170       1.078       0.791       17       1.512       0.582       1         136 GBPOL55C       1.045       1.006       0.950       17       1.101       0.199       1         137 GBPOL56A       1.201       0.991       0.839       10       1.433       -0.070       0         138 GBPOL56B       1.203       0.984       0.843       6       1.428       -0.132       0         139 GBPOL56C       1.217       0.997       0.823       8       1.480       -0.021       0         140 GBPOL57A       1.038       0.988       0.974       28       1.069       -0.545       1         141 GBPOL57B       1.047       0.999       0.955       27       1.096       -0.017       1         142 GBPOL58A       1.042       1.010       0.949       28       1.098       0.328       1         143 GBPOL58B       1.073       1.020       0.912       9       1.180       0.368       1	134 GBPOI 55A	1 100	1 014		0.895	15	1 2 3 0	0.210	1
136       GBPOL55C       1.045       1.006       0.950       17       1.101       0.199       1         136       GBPOL55C       1.045       1.006       0.950       17       1.101       0.199       1         137       GBPOL56A       1.201       0.991       0.839       10       1.433       -0.070       0         138       GBPOL56B       1.203       0.984       0.843       6       1.428       -0.132       0         139       GBPOL56C       1.217       0.997       0.823       8       1.480       -0.021       0         140       GBPOL57A       1.038       0.988       0.974       28       1.069       -0.545       1         141       GBPOL57B       1.047       0.999       0.955       27       1.096       -0.017       1         142       GBPOL58A       1.042       1.010       0.949       28       1.098       0.328       1         143       GBPOL58B       1.073       1.020       0.912       9       1.180       0.368       1	135 GBPOI 55B	1 170	1 078		0 791	17	1.512	0.582	1
137 GBPOL56A       1.201       0.991       0.839       10       1.433       -0.070       0         138 GBPOL56B       1.203       0.984       0.843       6       1.428       -0.132       0         139 GBPOL56C       1.217       0.997       0.823       8       1.480       -0.021       0         140 GBPOL57A       1.038       0.988       0.974       28       1.069       -0.545       1         141 GBPOL57B       1.047       0.999       0.955       27       1.096       -0.017       1         142 GBPOL58A       1.042       1.010       0.949       28       1.098       0.328       1         143 GBPOL58B       1.073       1.020       0.912       9       1.180       0.368       1	136 GBPOL55C	1.045	1 006		0.950	17	1 101	0.199	1
138 GBPOL56B       1.203       0.984       0.843       6       1.428       -0.132       0         139 GBPOL56C       1.217       0.997       0.823       8       1.480       -0.021       0         140 GBPOL57A       1.038       0.988       0.974       28       1.069       -0.545       1         141 GBPOL57B       1.047       0.999       0.955       27       1.096       -0.017       1         142 GBPOL58A       1.042       1.010       0.949       28       1.098       0.328       1         143 GBPOL58B       1.073       1.020       0.912       9       1.180       0.368       1	137 GBPOI 564	1 201	0 991		0.839	10	1.433	-0.070	0
139 GBPOL56C       1.217       0.997       0.823       8       1.480       -0.021       0         140 GBPOL57A       1.038       0.988       0.974       28       1.069       -0.545       1         141 GBPOL57B       1.047       0.999       0.955       27       1.096       -0.017       1         142 GBPOL58A       1.042       1.010       0.949       28       1.098       0.328       1         143 GBPOL58B       1.073       1.020       0.912       9       1.180       0.368       1	138 GBPOL 56B	1 203	0 984		0.843	.5	1.428	-0.132	Ō
140 GBPOL57A       1.038       0.988       0.974       28       1.069       -0.545       1         141 GBPOL57B       1.047       0.999       0.955       27       1.096       -0.017       1         142 GBPOL58A       1.042       1.010       0.949       28       1.098       0.328       1         143 GBPOL58B       1.073       1.020       0.912       9       1.180       0.368       1	139 GBPOI 560	1 217	0 997		0.823	8	1,480	-0.021	Ō
141 GBPOL57B       1.047       0.999       0.955       27       1.096       -0.017       1         142 GBPOL58A       1.042       1.010       0.949       28       1.098       0.328       1         143 GBPOL58B       1.073       1.020       0.912       9       1.180       0.368       1	140 GBPOI 574	1 038	0.007		0.974	28	1,069	-0.545	1
142 GBPOL58A       1.042       1.010       0.949       28       1.098       0.328       1         143 GBPOL58B       1.073       1.020       0.912       9       1.180       0.368       1	141 GRPOI 578	1 047	0.000		0.955	 27	1.096	-0.017	1
143 GBPOL58B 1.073 1.020 0.912 9 1.180 0.368 1	142 GBPOI 584	1 042	1 010		0.949	28	1.098	0.328	1
	143 GBPOI 58B	1.073	1.020		0.912		1.180	0.368	1

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Appendi	x 3 -	Sub-Areas	Magnetic	Fabric Data

	μSI	μSI	μSI		μSI			0=para
Samples	Kmax	Kint		Kmin	Kmean	Pj	Т	1=diamag
147 GBPOL60A	1.120	1.034		0.862	2	1.309	0.389	1
148 GBPOL60B	1.144	0.968		0.902	4	1.276	-0.406	1
149 GBPOL60C	1.213	0. <b>9</b> 70		0.849	3	1.435	-0.252	1
150 GBPOL61A	1.122	0.988		0.901	10	1.246	-0.165	1
151 GBPOL61B	1.048	1.010		0.943	10	1.112	0.296	1
152 GBPOL61C	1.077	1.001		0.926	10	1.163	0.037	1
1 TH45A	1.023	1.012		0.964	25	1.065	0.609	0
2 TH45B	1.087	0.967		0.950	11	1.157	-0.735	0
3 TH45C	1.053	0.996		0.953	14	1.104	-0.119	0
4 TH45D	1.030	1.017		0.953	15	1.087	0.677	0
5 TH45E	1.016	1.007		0.976	22	1.042	0.562	0
6 TH46A	1.179	1.015		0.835	6	1.414	0.132	0
7 TH46B	1.193	0.957		0.874	7	1.378	-0.416	0
8 TH46C	1.080	1.028		0.900	7	1.207	0.464	0
9 TH46D	1.253	1.130		0.705	8	1.854	0.640	0
10 TH46E	1.150	1.012		0.858	6	1.340	0.124	0
11 TH47A	1.125	1.028		0.863	27	1.310	0.320	0
12 TH47B	1.121	1.003		0.888	27	1.261	0.042	0
13 TH47C	1.398	1.221		0.585	25	2.589	0.689	0
14 TH47D	1.044	1.003		0.954	26	1.094	0.105	0
15 TH47E	1.020	1.011		0.968	34	1.057	0.673	0
16 TH48A	1.067	0.987		0.947	14	1.128	-0.307	0
17 TH48B	1.087	0.992		0.926	13	1.175	-0.143	0
18 TH48C	1.118	1.028		0.869	13	1.293	0.329	0
19 TH48D	1.071	0.969		0.962	13	1.126	-0.860	0
20 TH48E	1.019	1.005		0.975	27	1.046	0.343	0
21 TH49A	1.043	1.026		0.933	22	1.127	0.694	0
22 TH49B	1.029	1.005		0.966	20	1.065	0.245	0
23 TH49C	1.044	0.980		0.976	22	1.078	-0.863	0
24 TH49D	1.024	1.008		0.968	24	1.059	0.440	0
25 TH49E	1.025	1.014		0.961	18	1.071	0.675	0
26 TH50A	1.033	1.019		0.950	22	1.093	0.678	0
27 TH50B	1.022	1.005		0.974	23	1.050	0.284	0
28 TH50C	1.023	1.007		0.970	24	1.056	0.396	0
29 TH51A	1.021	1.000		0.980	34	1.042	0.010	0
30 TH51B	1.020	0.997		0.983	43	1.038	-0.241	0
31 TH51C	1.015	1.006		0.980	43	1.037	0.473	0
32 TH52A	1.016	0.999		0.985	57	1.032	-0.103	0
33 TH52B	1.016	1.000		0.985	58	1.032	0.008	0
34 TH52C	1.013	1.000		0.987	54	1.026	0.007	0
35 TH53A	1.023	1.014		0.964	24	1.067	0.722	0
36 TH53B	1.036	1.006		0.959	23	1.081	0.240	0
37 TH53C	1.010	1.001		0.989	24	1.021	0.205	0
38 TH54A	1.019	1.008		0.974	62	1.048	0.508	0
39 TH54B	1.013	1.006		0.981	70	1.034	0.551	0
40 TH54C	1.019	1.008		0.974	56	1.048	0.528	0
41 TH55A	1.027	1.004		0.970	26	1.059	0.214	0
42 TH55B	1.042	0.998		0.962	36	1.084	-0.083	0
43 TH55C	1.011	1.009		0.980	35	1.035	0.821	0

Appendix 3 -	Sub-Areas	Magnetic	Fabric Data
			and the second

Samples         Kmax         Kint         Kmin         Kmean         Pj         T         T         Telaimag           47         TH57A         1.024         1.011         0.966         63         1.062         0.565         0           48         TH57B         1.012         1.011         0.967         56         1.061         0.577         0           50         TH58A         1.010         0.973         24         1.050         0.643         0           53         TH59A         1.026         1.016         0.957         1.050         0.643         0           53         TH59A         1.026         1.016         0.959         19         1.076         0.701         0           54         TH59B         1.094         0.976         0.936         20         1.175         -0.470         0           56         TH60A         1.047         0.887         0.968         27         1.085         0.509         0           57         TH60B         1.024         1.001         0.976         31         1.049         0.079         0           60         TH612         1.027         1.010         0.964         300			μSI	μSI	μSI		μSI			0=para
47       TH57A       1.024       1.011       0.966       63       1.062       0.565       0         48       TH57B       1.018       1.016       0.967       57       1.060       0.933       0         50       TH58A       1.016       0.997       0.988       21       1.029       -0.327       0         51       TH58B       1.020       1.016       0.964       25       1.056       0.861       0         52       TH58C       1.018       1.016       0.973       24       1.050       0.643       0         53       TH59A       1.026       1.016       0.959       19       1.076       0.701       0         54       TH59B       1.094       0.976       0.933       20       1.127       0.331       0         55       TH59C       1.054       1.013       0.937       20       1.127       0.331       0         57       TH60B       1.022       1.001       0.976       31       1.049       0.079       0         60       TH61A       1.027       1.010       0.964       30       1.068       0.216       0       3       1.027       1.023		Samples	Kmax	Kint		Kmin	Kmean	Pj	Т	1=diamag
48         TH57E         1.018         1.016         0.967         57         1.060         0.933         0           49         TH57C         1.023         1.011         0.967         66         1.061         0.577         0           50         TH58A         1.020         1.016         0.964         25         1.065         0.861         0           51         TH58A         1.026         1.016         0.959         19         1.076         0.701         0           54         TH59A         1.026         1.016         0.959         19         1.076         0.470         0           55         TH59C         1.054         1.013         0.937         20         1.127         0.331         0           56         TH60C         1.027         1.005         0.971         29         1.057         0.263         0           57         TH60E         1.024         1.001         0.976         31         1.049         0.079         0           60         H61C         1.027         1.010         0.964         32         1.017         0.531         0           61         TH61A         1.024         0.996	47	TH57A	1.024	1.011		0.966	63	1.062	0.565	0
49         TH57C         1.023         1.011         0.967         66         1.061         0.577         0           50         TH58A         1.016         0.997         0.988         21         1.029         -0.327         0           51         TH58B         1.020         1.016         0.964         25         1.065         0.861         0           52         TH59A         1.026         1.016         0.953         20         1.175         -0.470         0           54         TH59B         1.094         0.976         0.935         20         1.175         -0.470         0           56         TH60A         1.047         0.987         0.968         27         1.055         -0.509         0           57         TH60B         1.025         1.005         0.971         29         1.065         0.263         0           57         TH60B         1.025         1.006         0.971         29         1.085         0.263         0           61         TH61A         1.024         1.001         0.976         31         1.049         0.079         0           62         TH62A         1.031         1.005 <td>48</td> <td>TH57B</td> <td>1.018</td> <td>1.016</td> <td></td> <td>0.967</td> <td>57</td> <td>1.060</td> <td>0.933</td> <td>0</td>	48	TH57B	1.018	1.016		0.967	57	1.060	0.933	0
50 TH58A         1.016         0.997         0.988         21         1.029         -0.37         0           51 TH58B         1.020         1.016         0.964         25         1.065         0.861         0           53 TH59A         1.026         1.016         0.973         24         1.050         0.643         0           54 TH59A         1.026         1.016         0.937         20         1.175         -0.470         0           55 TH59C         1.054         1.013         0.937         20         1.127         0.331         0           56 TH60A         1.047         0.987         0.968         27         1.085         -0.509         0           57 TH60B         1.027         1.001         0.976         31         1.049         0.079         0           60 TH61B         1.024         1.001         0.976         31         1.049         0.079         0           61 TH61C         1.027         1.010         0.964         30         1.068         0.216         0           62 TH62A         1.031         1.005         0.965         23         1.068         0.216         0           63 TH62B         1.033	49	TH57C	1.023	1.011		0.967	66	1.061	0.577	0
51 TH58B       1.020       1.016       0.964       25       1.065       0.8643       0         52 TH58C       1.018       1.010       0.973       24       1.050       0.6433       0         53 TH59A       1.026       1.016       0.959       19       1.076       0.701       0         54 TH59B       1.054       1.013       0.937       20       1.127       0.331       0         55 TH59C       1.054       1.017       0.987       0.968       27       1.085       0.609       0         57 TH60B       1.025       1.005       0.971       29       1.057       0.263       0         58 TH60C       1.037       1.005       0.968       27       1.082       0.201       0         59 TH61A       1.024       1.001       0.976       31       1.048       0.866       0 </td <td>50</td> <td>TH58A</td> <td>1.016</td> <td>0.997</td> <td></td> <td>0.988</td> <td>21</td> <td>1.029</td> <td>-0.327</td> <td>0</td>	50	TH58A	1.016	0.997		0.988	21	1.029	-0.327	0
52 TH58C       1.018       1.010       0.973       24       1.050       0.6701       0         53 TH59A       1.026       0.976       0.936       20       1.175       0.470       0         55 TH59C       1.054       1.013       0.937       20       1.127       0.331       0         55 TH59C       1.054       1.013       0.937       20       1.127       0.263       0         57 TH60B       1.025       1.005       0.971       29       1.057       0.263       0         58 TH60C       1.037       1.005       0.959       28       1.082       0.201       0         59 TH61A       1.024       1.001       0.976       31       1.049       0.079       0         60 TH61B       1.059       0.983       0.961       32       1.072       -0.234       0         61 TH61C       1.027       1.010       0.965       19       1.099       -0.088       0         62 TH62A       1.031       1.005       0.969       23       1.072       -0.234       0         64 TH62C       1.050       0.997       0.955       19       1.099       0.088       0       0	51	TH58B	1.020	1.016		0.964	25	1.065	0.861	0
53 TH59A       1.026       1.016       0.959       19       1.076       0.701       0         54 TH59B       1.054       0.976       0.937       20       1.175       -0.470       0         55 TH59C       1.054       1.013       0.937       20       1.127       0.331       0         56 TH60A       1.047       0.987       0.968       27       1.085       -0.509       0         57 TH50B       1.024       1.001       0.976       31       1.049       0.079       0         60 TH61B       1.024       1.001       0.976       31       1.068       0.486       0         61 TH61C       1.027       1.010       0.965       23       1.068       0.486       0         62 TH62A       1.031       1.005       0.965       23       1.072       -0.234       0         63 TH62B       1.033       0.995       0.969       23       1.072       0.234       0         64 TH62C       1.050       0.997       0.955       19       1.099       -0.088       0         65 TH01G       1.033       1.008       0.960       42       1.077       0.307       0 <t< td=""><td>52</td><td>TH58C</td><td>1.018</td><td>1.010</td><td></td><td>0.973</td><td>24</td><td>1.050</td><td>0.643</td><td>0</td></t<>	52	TH58C	1.018	1.010		0.973	24	1.050	0.643	0
54 TH59B       1.094       0.976       0.936       20       1.175       -0.470       0         55 TH60C       1.047       0.987       0.968       27       1.085       -0.509       0         57 TH60B       1.025       1.005       0.971       29       1.057       0.263       0         58 TH60C       1.037       1.005       0.959       28       1.082       0.201       0         59 TH61A       1.024       1.001       0.976       31       1.049       0.079       0         60 TH61B       1.059       0.983       0.961       32       1.107       -0.531       0         61 TH61C       1.027       1.010       0.964       30       1.068       0.216       0         63 TH62B       1.038       0.995       0.969       23       1.077       0.307       0         65 TH01F       1.025       1.016       0.960       42       1.077       0.307       0         67 TH02F       1.018       1.014       0.969       177       1.056       0.841       0         68 TH02G       1.020       1.012       0.969       151       1.057       0.779       0         <	53	TH59A	1.026	1.016		0.959	19	1.076	0.701	0
55       TH59C       1.054       1.013       0.937       20       1.127       0.331       0         56       TH60A       1.047       0.987       0.968       27       1.085       -0.509       0         57       TH60B       1.025       1.005       0.971       29       1.057       0.263       0         58       TH60C       1.037       1.005       0.959       28       1.082       0.201       0         59       TH61A       1.024       1.001       0.976       31       1.049       0.079       0         60       TH61B       1.059       0.983       0.961       32       1.107       -0.531       0         61       TH61C       1.027       1.010       0.964       30       1.068       0.486       0         62       TH62A       1.031       1.005       0.965       23       1.072       -0.234       0         63       TH62C       1.025       1.016       0.960       42       1.077       0.307       0         65       TH01F       1.025       1.014       0.969       117       1.056       0.841       0         65       TH02F	54	TH59B	1.094	0.976		0.936	20	1.175	-0.470	0
56       TH60A       1.047       0.987       0.968       27       1.085       -0.509       0         57       TH60B       1.025       1.005       0.971       29       1.057       0.263       0         58       TH60C       1.037       1.005       0.976       31       1.049       0.079       0         60       TH61A       1.024       1.001       0.976       31       1.049       0.079       0         60       TH61B       1.027       1.010       0.964       30       1.068       0.486       0         61       TH62A       1.031       1.005       0.965       23       1.068       0.216       0         63       TH62B       1.033       0.995       0.969       23       1.072       -0.234       0         64       TH82C       1.050       0.997       0.955       19       1.099       -0.088       0         65       TH01F       1.025       1.016       0.960       42       1.077       0.307       0         67       TH02F       1.018       1.012       0.969       185       1.056       0.745       0       0       0       0 <td< td=""><td>55</td><td>TH59C</td><td>1.054</td><td>1.013</td><td></td><td>0.937</td><td>20</td><td>1.127</td><td>0.331</td><td>0</td></td<>	55	TH59C	1.054	1.013		0.937	20	1.127	0.331	0
57       TH60B       1.025       1.005       0.971       29       1.057       0.263       0         58       TH60C       1.037       1.005       0.959       28       1.082       0.201       0         59       TH61A       1.024       1.001       0.976       31       1.049       0.079       0         60       TH61B       1.027       1.010       0.964       30       1.068       0.216       0         61       TH61C       1.027       1.010       0.965       23       1.072       -0.234       0         63       TH62B       1.038       0.997       0.955       19       1.099       -0.088       0         64       TH62C       1.050       0.997       0.955       19       1.099       -0.088       0         65       TH01F       1.025       1.016       0.960       42       1.077       0.307       0         67       TH02F       1.018       1.012       0.969       119       1.057       0.679       0         68       TH02G       1.020       1.012       0.969       185       1.032       0.257       0         70       TH04H	56	TH60A	1.047	0.987		0.968	27	1.085	-0.509	0
58 TH60C       1.037       1.005       0.959       28       1.082       0.201       0         59 TH61A       1.024       1.001       0.976       31       1.049       0.079       0         60 TH61B       1.059       0.983       0.961       32       1.107       -0.531       0         61 TH61C       1.027       1.010       0.965       23       1.068       0.486       0         62 TH62A       1.031       1.005       0.965       23       1.068       0.216       0         63 TH62B       1.038       0.995       0.969       23       1.072       -0.234       0         64 TH62C       1.050       0.997       0.955       19       1.099       -0.088       0         65 TH01G       1.033       1.008       0.960       42       1.077       0.307       0         68 TH02G       1.020       1.012       0.969       1185       1.056       0.745       0         70 TH04A       1.017       1.005       0.979       51       1.039       0.376       0         71 TH04B       1.013       1.002       0.983       52       1.029       0.207       0         <	57	TH60B	1.025	1.005		0.971	29	1.057	0.263	0
59       TH61A       1.024       1.001       0.976       31       1.049       0.079       0         60       TH61B       1.059       0.983       0.961       32       1.107       -0.531       0         61       TH61C       1.027       1.010       0.964       30       1.068       0.216       0         63       TH62A       1.031       1.005       0.965       23       1.068       0.216       0         64       TH62C       1.050       0.997       0.955       19       1.099       -0.234       0         65       TH01F       1.025       1.016       0.960       42       1.077       0.307       0         66       TH01G       1.033       1.008       0.969       117       1.056       0.841       0         68       TH02F       1.019       1.012       0.969       185       1.056       0.745       0         70       TH04A       1.017       1.005       0.979       51       1.039       0.376       0         71       TH04A       1.013       1.002       0.983       52       1.022       0.267       0         73       TH04D	58	TH60C	1.037	1.005		0.959	28	1.082	0.201	0
60         TH61B         1.059         0.983         0.961         32         1.107         -0.531         0           61         TH61C         1.027         1.010         0.964         30         1.068         0.216         0           62         TH62A         1.031         1.005         0.965         23         1.068         0.216         0           64         TH62B         1.038         0.997         0.955         19         1.099         -0.088         0           65         TH01F         1.025         1.016         0.960         42         1.077         0.307         0           67         TH02F         1.018         1.014         0.969         119         1.056         0.841         0           68         TH02G         1.020         1.012         0.969         185         1.056         0.745         0           70         TH04H         1.017         1.005         0.979         51         1.032         0.376         0           71         TH04B         1.013         1.002         0.983         52         1.032         0.257         0           73         TH04D         1.013         1.002 <td>59</td> <td>TH61A</td> <td>1.024</td> <td>1.001</td> <td></td> <td>0.976</td> <td>31</td> <td>1.049</td> <td>0.079</td> <td>0</td>	59	TH61A	1.024	1.001		0.976	31	1.049	0.079	0
61       TH61C       1.027       1.010       0.964       30       1.068       0.486       0         62       TH62A       1.031       1.005       0.965       23       1.068       0.216       0         63       TH62C       1.050       0.997       0.955       19       1.099       -0.088       0         64       TH62C       1.050       0.997       0.955       19       1.099       -0.088       0         65       TH01F       1.025       1.016       0.960       42       1.077       0.307       0         66       TH02F       1.018       1.014       0.969       177       1.056       0.745       0         69       TH02H       1.019       1.012       0.969       185       1.039       0.376       0         70       TH04A       1.017       1.005       0.979       51       1.039       0.376       0         71       TH04B       1.013       1.001       0.986       53       1.027       0.149       0         73       TH04D       1.013       1.002       0.982       50       1.034       0.185       0         75       TH04F	60	TH61B	1.059	0.983		0.961	32	1.107	-0.531	0
62       TH62A       1.031       1.005       0.965       23       1.072       -0.234       0         63       TH62B       1.038       0.995       0.969       23       1.072       -0.234       0         64       TH62C       1.050       0.997       0.955       19       1.099       -0.088       0         65       TH01F       1.025       1.016       0.960       64       1.077       0.307       0         67       TH02F       1.018       1.014       0.969       177       1.056       0.841       0         68       TH02G       1.020       1.012       0.969       185       1.056       0.745       0         70       TH04A       1.017       1.005       0.979       51       1.039       0.376       0         71       TH04B       1.013       1.001       0.985       52       1.029       0.207       0         73       TH04D       1.013       1.002       0.982       50       1.034       0.185       0         75       TH04F       1.013       1.004       0.983       53       1.031       0.381       0         76       TH05A	61	TH61C	1.027	1.010		0.964	30	1.068	0.486	0
63 TH62B       1.038       0.995       0.969       23       1.072       -0.234       0         64 TH62C       1.050       0.997       0.955       19       1.099       -0.088       0         65 TH01F       1.025       1.016       0.960       68       1.077       0.307       0         67 TH02F       1.018       1.014       0.969       119       1.057       0.679       0         69 TH02H       1.019       1.012       0.969       185       1.056       0.841       0         69 TH02H       1.019       1.012       0.969       185       1.056       0.745       0         70 TH04A       1.017       1.003       0.983       52       1.032       0.257       0         73 TH04D       1.013       1.002       0.985       52       1.029       0.207       0         74 TH04E       1.013       1.004       0.983       53       1.034       0.185       0         75 TH04F       1.013       1.007       0.977       51       1.042       0.507       0         74 TH04E       1.017       1.007       0.977       51       1.038       0.689       0         <	62	TH62A	1.031	1.005		0.965	23	1.068	0.216	0
64       TH62C       1.050       0.997       0.955       19       1.099       -0.088       0         65       TH01F       1.025       1.016       0.960       68       1.074       0.735       0         66       TH02F       1.018       1.014       0.969       177       1.056       0.841       0         67       TH02F       1.018       1.014       0.969       119       1.057       0.679       0         68       TH02G       1.020       1.012       0.969       185       1.056       0.745       0         69       TH02H       1.019       1.012       0.969       185       1.056       0.745       0         70       TH04A       1.017       1.005       0.979       51       1.039       0.376       0         71       TH04B       1.013       1.001       0.986       52       1.032       0.257       0         73       TH04D       1.013       1.002       0.983       53       1.034       0.185       0         74       TH04E       1.016       1.002       0.982       50       1.034       0.185       0         75       TH04F	63	TH62B	1.038	0.995		0.969	23	1.072	-0.234	0
65         THOIF         1.025         1.016         0.960         68         1.074         0.735         0           66         THO1G         1.033         1.008         0.960         42         1.077         0.307         0           67         TH02F         1.018         1.014         0.969         177         1.056         0.841         0           68         THO2G         1.020         1.012         0.969         185         1.056         0.745         0           69         THO2H         1.019         1.012         0.969         185         1.056         0.745         0           70         THO4A         1.017         1.005         0.979         51         1.039         0.376         0           71         THO4B         1.013         1.001         0.986         53         1.027         0.149         0           72         THO4C         1.014         1.002         0.985         50         1.034         0.185         0           75         THO4F         1.013         1.002         0.982         50         1.034         0.185         0           75         THO4F         1.013         1.004	64	TH62C	1.050	0.997		0.955	19	1.099	-0.088	0
66         THO1G         1.033         1.008         0.960         42         1.077         0.307         0           67         TH02F         1.018         1.014         0.969         177         1.056         0.841         0           68         TH02G         1.020         1.012         0.969         119         1.057         0.679         0           69         TH02H         1.019         1.012         0.969         185         1.056         0.745         0           70         TH04A         1.017         1.005         0.979         51         1.039         0.376         0           71         TH04B         1.013         1.002         0.985         52         1.029         0.207         0           74         TH04E         1.016         1.002         0.982         50         1.034         0.185         0           75         TH04F         1.013         1.004         0.983         53         1.031         0.381         0           76         TH05A         1.019         1.007         0.977         51         1.042         0.507         0           78         TH05C         1.014         1.008	65	TH01F	1.025	1.016		0.960	68	1.074	0.735	Ō
67       TH02F       1.018       1.014       0.969       177       1.056       0.841       0         68       TH02G       1.020       1.012       0.969       119       1.057       0.679       0         69       TH02H       1.019       1.012       0.969       185       1.056       0.745       0         70       TH04A       1.017       1.005       0.979       51       1.039       0.376       0         71       TH04B       1.013       1.001       0.986       53       1.022       0.257       0         73       TH04D       1.013       1.002       0.982       50       1.034       0.185       0         75       TH04F       1.013       1.004       0.983       53       1.031       0.381       0         75       TH04F       1.013       1.004       0.983       53       1.031       0.381       0         75       TH04F       1.013       1.007       0.977       51       1.042       0.507       0         78       TH05C       1.014       1.008       0.979       55       1.038       0.689       0         79       TH05D	66	TH01G	1 033	1 008		0.960	42	1.077	0.307	0
68       THO2G       1.020       1.011       0.069       119       1.057       0.679       0         69       THO2H       1.019       1.012       0.969       185       1.056       0.745       0         70       THO4A       1.017       1.005       0.979       51       1.039       0.376       0         71       THO4B       1.013       1.001       0.986       53       1.027       0.149       0         72       THO4C       1.014       1.003       0.983       52       1.032       0.257       0         73       THO4D       1.013       1.002       0.985       52       1.024       0.185       0         75       THO4E       1.016       1.002       0.983       53       1.031       0.381       0         76       THO5A       1.019       1.004       0.983       53       1.031       0.381       0         76       THO5A       1.019       1.007       0.977       51       1.042       0.507       0         78       THO5C       1.014       1.008       0.979       55       1.038       0.689       0         70       THO5D	67	TH02E	1 018	1 014		0.969	177	1 056	0.841	0
05       11020       1.012       0.969       185       1.056       0.745       0         70       TH04A       1.017       1.005       0.979       51       1.039       0.376       0         71       TH04B       1.013       1.001       0.986       53       1.027       0.149       0         72       TH04C       1.014       1.003       0.983       52       1.032       0.257       0         73       TH04D       1.016       1.002       0.985       52       1.029       0.207       0         74       TH04E       1.016       1.002       0.982       50       1.034       0.185       0         75       TH04F       1.013       1.004       0.983       53       1.031       0.381       0         76       TH05A       1.019       1.009       0.973       60       1.049       0.563       0         77       TH05B       1.017       1.007       0.977       51       1.042       0.507       0         78       TH05C       1.014       1.008       0.979       55       1.038       0.689       0         79       TH05D       1.019	68	TH02G	1.010	1 012		0.969	119	1 057	0.679	õ
000       11021       11022       01079       51       11039       0.376       0         71       TH04A       1.013       1.001       0.986       53       1.027       0.149       0         72       TH04C       1.014       1.003       0.983       52       1.032       0.257       0         73       TH04D       1.013       1.002       0.985       52       1.029       0.207       0         74       TH04E       1.016       1.002       0.982       50       1.034       0.185       0         75       TH04F       1.013       1.004       0.983       53       1.031       0.381       0         76       TH05A       1.019       1.009       0.973       60       1.049       0.563       0         77       TH05B       1.017       1.007       0.977       51       1.042       0.507       0         78       TH05C       1.014       1.008       0.979       55       1.038       0.689       0         70       TH05D       1.019       1.011       0.970       51       1.054       0.686       0         80       TH06E       1.020	69	TH02H	1.019	1 012		0.969	185	1.056	0 745	Ő
11001       1.001       0.986       53       1.027       0.149       0         72       THO4C       1.014       1.003       0.983       52       1.027       0.149       0         73       THO4C       1.013       1.002       0.985       52       1.029       0.207       0         74       THO4E       1.016       1.002       0.982       50       1.034       0.185       0         75       THO4F       1.013       1.004       0.983       53       1.031       0.381       0         76       TH05A       1.019       1.009       0.973       60       1.049       0.563       0         77       THO5B       1.017       1.007       0.977       51       1.042       0.507       0         78       THO5C       1.014       1.008       0.979       55       1.038       0.689       0         79       TH05D       1.019       1.011       0.970       51       1.054       0.686       0         80       TH05E       1.022       0.997       0.981       48       1.043       -0.190       0         81       TH06A       1.028       1.007	70	TH04A	1.010	1.012		0.979	51	1 039	0.376	Ő
1111042       1.010       1.001       0.000       1.011       0.110       0.110         72       THOAC       1.013       1.002       0.983       52       1.032       0.257       0         74       THO4E       1.016       1.002       0.982       50       1.034       0.185       0         75       THO4F       1.013       1.004       0.983       53       1.031       0.381       0         76       THO5A       1.019       1.007       0.973       60       1.049       0.563       0         77       TH05B       1.017       1.007       0.977       51       1.042       0.507       0         78       THO5C       1.014       1.008       0.979       55       1.038       0.689       0         79       THO5D       1.019       1.011       0.970       51       1.054       0.686       0         80       TH06A       1.028       1.007       0.966       24       1.066       0.347       0         81       TH06A       1.026       1.012       0.963       22       1.069       0.582       0         83       TH06E       1.021       1.004	71	TH04R	1.013	1.000		0.986	53	1.000	0 149	Õ
73 THO4D       1.011       1.002       0.985       52       1.029       0.207       0         74 THO4E       1.016       1.002       0.982       50       1.034       0.185       0         75 THO4F       1.013       1.004       0.983       53       1.031       0.381       0         76 THO5A       1.019       1.007       0.973       60       1.049       0.563       0         77 THO5B       1.017       1.007       0.977       51       1.042       0.507       0         78 THO5C       1.014       1.008       0.979       55       1.038       0.689       0         79 THO5D       1.019       1.011       0.970       51       1.054       0.686       0         80 TH05E       1.022       0.997       0.981       48       1.043       -0.190       0         81 TH06A       1.028       1.007       0.966       24       1.066       0.347       0         82 TH06B       1.020       1.000       0.983       22       1.069       0.582       0         84 TH06D       1.013       1.004       0.983       24       1.031       0.435       0         8	72	THOAC	1.010	1 003		0.983	52	1 032	0.257	Õ
74 THO4E       1.016       1.002       0.982       50       1.025       0.185       0         75 TH04F       1.013       1.004       0.983       53       1.034       0.185       0         76 TH05A       1.019       1.009       0.973       60       1.049       0.563       0         77 TH05B       1.017       1.007       0.977       51       1.042       0.507       0         78 TH05C       1.014       1.008       0.979       55       1.038       0.689       0         79 TH05D       1.019       1.011       0.970       51       1.054       0.686       0         80 TH05E       1.022       0.997       0.981       48       1.043       -0.190       0         81 TH06A       1.028       1.007       0.966       24       1.066       0.347       0         82 TH06B       1.020       1.000       0.983       22       1.041       0.010       0         83 TH06C       1.026       1.012       0.963       22       1.069       0.582       0         84 TH06D       1.013       1.004       0.983       24       1.031       0.435       0         8	73	TH04D	1.013	1 002		0.985	52	1 029	0 207	Õ
75       THO4F       1.013       1.004       0.983       53       1.031       0.381       0         75       TH04F       1.013       1.004       0.983       53       1.031       0.381       0         76       TH05A       1.019       1.009       0.973       60       1.049       0.563       0         77       TH05B       1.017       1.007       0.977       51       1.042       0.507       0         78       TH05C       1.014       1.008       0.979       55       1.038       0.689       0         79       TH05D       1.019       1.011       0.970       51       1.054       0.686       0         80       TH05E       1.022       0.997       0.981       48       1.043       -0.190       0         81       TH06A       1.028       1.007       0.966       24       1.066       0.347       0         82       TH06B       1.020       1.000       0.983       22       1.041       0.010       0         83       TH06C       1.026       1.012       0.963       22       1.048       0.211       0         85       TH06E	74	THOAE	1.016	1.002		0.982	50	1 034	0 185	Ő
76       THORT       1.009       0.973       60       1.049       0.563       0         76       THO5A       1.019       1.009       0.973       60       1.049       0.563       0         77       TH05B       1.017       1.007       0.977       51       1.042       0.507       0         78       TH05C       1.014       1.008       0.979       55       1.038       0.689       0         79       TH05D       1.019       1.011       0.970       51       1.054       0.686       0         80       TH05E       1.022       0.997       0.981       48       1.043       -0.190       0         81       TH06A       1.028       1.007       0.966       24       1.066       0.347       0         82       TH06B       1.020       1.000       0.980       25       1.041       0.010       0         83       TH06C       1.026       1.012       0.963       22       1.069       0.582       0         84       TH06D       1.013       1.004       0.983       24       1.031       0.435       0         85       TH06E       1.022	75	THOAE	1.013	1.002		0.983	53	1.031	0.381	Õ
77 TH05B       1.017       1.007       0.977       51       1.042       0.507       0         78 TH05C       1.014       1.008       0.979       55       1.038       0.689       0         79 TH05D       1.019       1.011       0.970       51       1.054       0.686       0         80 TH05E       1.022       0.997       0.981       48       1.043       -0.190       0         81 TH06A       1.028       1.007       0.966       24       1.066       0.347       0         82 TH06B       1.020       1.000       0.980       25       1.041       0.010       0         83 TH06C       1.026       1.012       0.963       22       1.069       0.582       0         84 TH06D       1.013       1.004       0.983       24       1.031       0.435       0         85 TH06E       1.037       0.993       0.971       23       1.068       -0.319       0         86 TH06F       1.022       1.003       0.976       22       1.048       0.211       0         87 TH06G       1.040       0.999       0.962       22       1.081       -0.039       0 <td< td=""><td>76</td><td>TH05A</td><td>1.010</td><td>1 009</td><td></td><td>0.000</td><td>60</td><td>1 049</td><td>0.563</td><td>Ő</td></td<>	76	TH05A	1.010	1 009		0.000	60	1 049	0.563	Ő
78       THOSE       1.011       1.001       0.011       0.	77	TH05B	1.017	1.000		0.977	51	1.042	0.507	Ő
79 TH05D       1.019       1.011       0.970       51       1.053       0.080       0         80 TH05E       1.022       0.997       0.981       48       1.043       -0.190       0         81 TH06A       1.028       1.007       0.966       24       1.066       0.347       0         82 TH06B       1.020       1.000       0.980       25       1.041       0.010       0         83 TH06C       1.026       1.012       0.963       22       1.069       0.582       0         84 TH06D       1.013       1.004       0.983       24       1.031       0.435       0         85 TH06E       1.037       0.993       0.971       23       1.068       -0.319       0         86 TH06F       1.022       1.003       0.976       22       1.048       0.211       0         87 TH06G       1.040       0.999       0.962       22       1.081       -0.039       0         88 TH08F       1.029       1.022       0.951       15       1.091       0.839       0         90 TH09G       1.059       0.991       0.953       13       1.112       -0.261       0 <t< td=""><td>78</td><td>TH05C</td><td>1 014</td><td>1.007</td><td></td><td>0.979</td><td>55</td><td>1.038</td><td>0.689</td><td>õ</td></t<>	78	TH05C	1 014	1.007		0.979	55	1.038	0.689	õ
10000       1.000       1.000       0.0000 <t< td=""><td>79</td><td>TH05D</td><td>1.019</td><td>1.000</td><td></td><td>0.970</td><td>51</td><td>1.054</td><td>0.686</td><td>Õ</td></t<>	79	TH05D	1.019	1.000		0.970	51	1.054	0.686	Õ
81 TH06A       1.028       1.007       0.966       24       1.066       0.347       0         82 TH06B       1.020       1.000       0.980       25       1.041       0.010       0         83 TH06C       1.026       1.012       0.963       22       1.069       0.582       0         84 TH06D       1.013       1.004       0.983       24       1.031       0.435       0         85 TH06E       1.037       0.993       0.971       23       1.068       -0.319       0         86 TH06F       1.022       1.003       0.976       22       1.081       -0.039       0         87 TH06G       1.040       0.999       0.962       22       1.081       -0.039       0         87 TH06G       1.029       1.022       0.951       15       1.091       0.839       0         88 TH08F       1.029       1.022       0.951       15       1.091       0.839       0         89 TH09F       1.053       1.006       0.944       13       1.112       -0.261       0         90 TH09G       1.059       0.991       0.953       13       1.027       0.780       0 <t< td=""><td>80</td><td>THOSE</td><td>1.010</td><td>0.997</td><td></td><td>0.981</td><td>48</td><td>1 043</td><td>-0 190</td><td>Ő</td></t<>	80	THOSE	1.010	0.997		0.981	48	1 043	-0 190	Ő
82 TH06B       1.020       1.000       0.980       25       1.041       0.010       0         83 TH06C       1.026       1.012       0.963       22       1.069       0.582       0         84 TH06D       1.013       1.004       0.983       24       1.031       0.435       0         85 TH06E       1.037       0.993       0.971       23       1.068       -0.319       0         86 TH06F       1.022       1.003       0.976       22       1.041       0.039       0         87 TH06G       1.040       0.999       0.962       22       1.081       -0.039       0         88 TH08F       1.029       1.022       0.951       15       1.091       0.839       0         89 TH09F       1.053       1.006       0.944       13       1.112       -0.261       0         90 TH09G       1.059       0.991       0.953       13       1.112       -0.261       0         91 TH10F       1.021       1.010       0.971       36       1.054       0.564       0         92 TH10G       1.009       1.006       0.985       37       1.027       0.780       0 <t< td=""><td>81</td><td>THOSE</td><td>1.022</td><td>1 007</td><td></td><td>0.966</td><td>24</td><td>1.066</td><td>0.347</td><td>0 0</td></t<>	81	THOSE	1.022	1 007		0.966	24	1.066	0.347	0 0
83 TH06C       1.026       1.012       0.963       22       1.069       0.582       0         84 TH06D       1.013       1.004       0.983       24       1.031       0.435       0         85 TH06E       1.037       0.993       0.971       23       1.068       -0.319       0         86 TH06F       1.022       1.003       0.976       22       1.048       0.211       0         87 TH06G       1.040       0.999       0.962       22       1.081       -0.039       0         88 TH08F       1.029       1.022       0.951       15       1.091       0.839       0         88 TH08F       1.029       1.022       0.951       15       1.091       0.839       0         89 TH09F       1.053       1.006       0.944       13       1.112       -0.261       0         90 TH09G       1.059       0.991       0.953       13       1.112       -0.261       0         91 TH10F       1.021       1.010       0.971       36       1.054       0.564       0         92 TH10G       1.009       1.006       0.985       37       1.027       0.780       0 <t< td=""><td>82</td><td>THOOR</td><td>1.020</td><td>1.007</td><td></td><td>0.980</td><td>25</td><td>1 041</td><td>0.010</td><td>0</td></t<>	82	THOOR	1.020	1.007		0.980	25	1 041	0.010	0
86 TH06C       1.012       1.012       0.000       1.012       0.000       0.000         84 TH06D       1.013       1.004       0.983       24       1.031       0.435       0         85 TH06E       1.037       0.993       0.971       23       1.068       -0.319       0         86 TH06F       1.022       1.003       0.976       22       1.048       0.211       0         87 TH06G       1.040       0.999       0.962       22       1.081       -0.039       0         87 TH06G       1.029       1.022       0.951       15       1.091       0.839       0         88 TH08F       1.029       1.022       0.951       15       1.091       0.839       0         89 TH09F       1.053       1.006       0.944       13       1.115       0.169       0         90 TH09G       1.059       0.991       0.953       13       1.112       -0.261       0         91 TH10F       1.021       1.010       0.971       36       1.054       0.564       0         92 TH10G       1.009       1.006       0.985       37       1.027       0.780       0         93 TH11F	83	THOSE	1.026	1.000		0.963	22	1 069	0.582	0
85 TH06E       1.037       0.993       0.971       23       1.068       -0.319       0         86 TH06F       1.022       1.003       0.976       22       1.048       0.211       0         87 TH06G       1.040       0.999       0.962       22       1.081       -0.039       0         88 TH08F       1.029       1.022       0.951       15       1.091       0.839       0         89 TH09F       1.053       1.006       0.944       13       1.115       0.169       0         90 TH09G       1.059       0.991       0.953       13       1.112       -0.261       0         91 TH10F       1.021       1.010       0.971       36       1.054       0.564       0         92 TH10G       1.009       1.006       0.985       37       1.027       0.780       0         93 TH11F       1.043       0.983       0.976       13       1.075       -0.771       0         94 TH12F       1.019       1.007       0.975       31       1.047       0.438       0         95 TH12G       1.032       1.000       0.968       31       1.066       0.016       0 <td>84</td> <td>THOOD</td> <td>1.020</td> <td>1 004</td> <td></td> <td>0.983</td> <td>24</td> <td>1 031</td> <td>0.435</td> <td>0 0</td>	84	THOOD	1.020	1 004		0.983	24	1 031	0.435	0 0
86 TH06E       1.007       0.000       0.017       1.005       0.017       1.005       0.016       0         86 TH06F       1.022       1.003       0.976       22       1.048       0.211       0         87 TH06G       1.040       0.999       0.962       22       1.081       -0.039       0         88 TH08F       1.029       1.022       0.951       15       1.091       0.839       0         89 TH09F       1.053       1.006       0.944       13       1.115       0.169       0         90 TH09G       1.059       0.991       0.953       13       1.112       -0.261       0         91 TH10F       1.021       1.010       0.971       36       1.054       0.564       0         92 TH10G       1.009       1.006       0.985       37       1.027       0.780       0         93 TH11F       1.043       0.983       0.976       13       1.075       -0.771       0         94 TH12F       1.019       1.007       0.975       31       1.047       0.438       0         95 TH12G       1.032       1.000       0.968       31       1.066       0.016       0	85	THOSE	1.017	0 993		0.971	23	1 068	-0.319	0 0
87 TH06G       1.040       0.999       0.962       22       1.081       -0.039       0         88 TH08F       1.029       1.022       0.951       15       1.091       0.839       0         89 TH09F       1.053       1.006       0.944       13       1.115       0.169       0         90 TH09G       1.059       0.991       0.953       13       1.112       -0.261       0         91 TH10F       1.021       1.010       0.971       36       1.054       0.564       0         92 TH10G       1.009       1.006       0.985       37       1.027       0.780       0         93 TH11F       1.043       0.983       0.976       13       1.075       -0.771       0         94 TH12F       1.019       1.007       0.975       31       1.047       0.438       0         95 TH12G       1.032       1.000       0.968       31       1.066       0.016       0	86	THOOF	1.007	1 003		0.976	22	1 048	0.211	0
88 TH08F       1.029       1.022       0.951       15       1.091       0.839       0         89 TH09F       1.053       1.006       0.944       13       1.115       0.169       0         90 TH09G       1.059       0.991       0.953       13       1.112       -0.261       0         91 TH10F       1.021       1.010       0.971       36       1.054       0.564       0         92 TH10G       1.009       1.006       0.985       37       1.027       0.780       0         93 TH11F       1.043       0.983       0.976       13       1.075       -0.771       0         94 TH12F       1.019       1.007       0.975       31       1.047       0.438       0         95 TH12G       1.032       1.000       0.968       31       1.066       0.016       0	87	THORG	1.022	0 999		0.962	22	1.081	-0.039	Ő
89 TH09F       1.053       1.006       0.944       13       1.115       0.169       0         90 TH09G       1.059       0.991       0.953       13       1.112       -0.261       0         91 TH10F       1.021       1.010       0.971       36       1.054       0.564       0         92 TH10G       1.009       1.006       0.985       37       1.027       0.780       0         93 TH11F       1.043       0.983       0.976       13       1.075       -0.771       0         94 TH12F       1.019       1.007       0.975       31       1.047       0.438       0         95 TH12G       1.032       1.000       0.968       31       1.066       0.016       0	88	THOSE	1.070	1 022		0.002	15	1.001	0.000	Ő
90 TH09G       1.059       0.991       0.953       13       1.110       0.105       0         91 TH10F       1.021       1.010       0.971       36       1.054       0.564       0         92 TH10G       1.009       1.006       0.985       37       1.027       0.780       0         93 TH11F       1.043       0.983       0.976       13       1.075       -0.771       0         94 TH12F       1.019       1.007       0.975       31       1.047       0.438       0         95 TH12G       1.032       1.000       0.968       31       1.066       0.016       0	80		1.020	1.022		0.001	13	1 115	0.000	0
91 TH10F       1.021       1.010       0.971       36       1.054       0.564       0         92 TH10G       1.009       1.006       0.985       37       1.027       0.780       0         93 TH11F       1.043       0.983       0.976       13       1.075       -0.771       0         94 TH12F       1.019       1.007       0.975       31       1.047       0.438       0         95 TH12G       1.032       1.000       0.968       31       1.066       0.016       0	03	THOOG	1.000	0.991		0.044	13	1.110	-0.261	0
92 TH10G       1.009       1.006       0.985       37       1.027       0.780       0         93 TH11F       1.043       0.983       0.976       13       1.075       -0.771       0         94 TH12F       1.019       1.007       0.975       31       1.047       0.438       0         95 TH12G       1.032       1.000       0.968       31       1.066       0.016       0	Q1	THINE	1 021	1 010		0.000	26	1 054	0.564	n n
93 TH11F       1.043       0.983       0.976       13       1.027       0.760       0         94 TH12F       1.019       1.007       0.975       31       1.047       0.438       0         95 TH12G       1.032       1.000       0.968       31       1.066       0.016       0	91	THIOG	1 000	1 006		0.071	37	1 027	0.780	ñ
94 TH12F       1.019       1.007       0.975       31       1.043       0.438       0         95 TH12G       1.032       1.000       0.968       31       1.066       0.016       0	02	TH11E	1 0/2	U 083		0.000	12	1 075	_0 771	n
95 TH12G 1.032 1.000 0.968 31 1.066 0.016 0	0J	TH12E	1 010	1 007		0.075	-0 -21	1 0/7	0/38	0
	95	TH12G	1 032	1 000		0.968	31	1 066	0.016	õ

Appendix 3	- Sub-Areas	Magnetic	Fabric	Data
			the second s	

	μSI	μSI	μSI	_	μSI			0=para
Samples	Kmax	Kint		Kmin	Kmean	Pj	Т	1=diamag
99 TH14G	1.020	1.000		0.981	25	1.040	0.010	0
100 TH16F	1.015	1.007		0.979	36	1.039	0.545	0
101 TH17F	1.019	1.006		0.975	23	1.046	0.409	0
102 TH17G	1.023	0.999		0.979	25	1.045	-0.080	0
103 TH18F	1.025	1.013		0.964	16	1.068	0.610	0
104 TH19A	1.020	1.013		0.968	15	1.058	0.756	0
105 TH19B	1.037	0.985		0.979	16	1.065	-0.772	0
106 TH20A	1.030	1.019		0.953	18	1.089	0.724	0
107 TH20B	1.026	1.006		0.969	19	1.060	0.286	0
108 TH21A	1.053	1.004		0.946	21	1.113	0.117	0
109 TH21B	1.070	0.985		0.949	31	1.131	-0.380	0
110 TH22B	1.021	1.007		0.972	35	1.052	0.422	0
111 TH22C	1.028	0.988		0.985	34	1.050	-0.864	0
112 TH23A	1.070	0.982		0.952	17	1.128	-0.478	0
113 TH23B	1.037	1.000		0.964	16	1.076	0.018	0
114 TH24A	1.136	0.978		0.900	9	1.267	-0.280	0
115 TH24B	1.077	0.998		0.930	9	1.159	-0.040	0
116 TH25A	1.025	0.999		0.976	35	1.050	-0.047	0
117 TH25B	1.012	1.001		0.987	36	1.025	0.117	0
118 TH26A	1.035	0.999		0.967	22	1.071	-0.050	0
119 TH26B	1.020	1.009		0.972	29	1.052	0.579	0
120 TH27A	1.084	0.973		0.948	23	1.153	-0.604	0
121 TH27B	1.046	0.999		0.957	19	1.093	-0.037	0
122 TH28A	1.023	1.014		0.964	20	1.066	0.675	0
123 TH28B	1.041	1.015		0.946	19	1.104	0.463	0
124 TH29A	1.022	0.999		0.979	39	1.044	-0.048	0
125 TH29B	1.014	1.004		0.983	42	1.032	0.391	0
126 TH30A	1.029	1.005		0.967	21	1.064	0.245	0
127 TH30B	1.034	1.009		0.959	20	1.079	0.350	0
128 TH31A	1.015	0. <b>9</b> 98		0.987	82	1.029	-0.211	0
129 TH31B	1.022	0.993		0.985	75	1.039	-0.549	0
130 TH32A	1.013	1.005		0.982	85	1.033	0.488	0
131 TH32C	1.017	1.001		0.982	86	1.035	0.075	0
132 TH33A	1.019	1.004		0.978	19	1.043	0.260	0
133 TH33B	1.030	0.995		0.976	20	1.056	-0.260	0
134 TH34A	1.020	0.997		0.984	30	1.037	-0.264	0
135 TH34B	1.026	0.994		0.981	31	1.047	-0.419	0
136 TH35A	1.036	0.998		0.967	13	1.071	-0.094	0
137 TH35B	1.040	1.007		0.955	15	1.091	0.251	0
138 TH36A	1.022	0.989		0.989	19	1.038	-1.000	0
139 TH36B	1.037	1.000		0.964	19	1.077	0.018	0
140 TH37A	1.038	1.006		0.958	12	1.085	0.219	0
141 TH37B	1.042	1.003		0.956	13	1.090	0.112	0
142 TH38A	1.056	1.001		0.946	15	1.116	0.027	0
143 TH38B	1.024	1.006		0.970	17	1.057	0.345	0
144 TH39A	1.026	0.996		0.978	17	1.049	-0.239	0
145 TH39B	1.030	1.014		0.957	19	1.080	0.584	0
146 TH40A	1.013	1.000		0.987	62	1.026	0.006	0
147 TH40B	1.007	1.002		0.992	61	1.015	0.337	0

Appendix	3 - Si	ub-Areas	Magnetic	Fabric	Data

		μSI	μSI	μSI	μSI			0=para
	Samples	Kmax	Kint	Kmin	Kmean	Pj	т	1=diamag
151	TH42B	1.014	1.008	0.978	31	1.039	0.642	0
152	TH43A	1.033	1.002	0.966	19	1.069	0.094	0
153	TH43B	1.030	1.009	0.962	19	1.072	0.399	0
154	TH44A	1.023	1.003	0.974	31	1.051	0.212	0
155	TH44B	1.026	0.998	0.977	32	1.051	-0.113	0

Appendix 4	-Regional	Area	Sample	Location	and	Formatio	วท

Sample	Northing	Easting	Formation	Sample	Northing	Easting	Formation
CY9701	3844700	500540	?	FL98212	3851037	481200	Pakhna
CY9702	3844950	499550	?	FL98213A	3851618	480922	Pakhna
CY9703	3847180	495020	?	FL98214	3852065	481041	Pakhna
CY9704	3846875	492570	?	FL98215A	3850217	481762	Pakhna
CY9705	3850500	492425	?	FL98216	3849676	481533	Pakhna
CY9706	3851450	492500	?	FL98217A	3849172	481383	Pakhna
CY9707	3855025	492150	?	FL98218	3848433	481477	Pakhna
CY9708	3856300	492320	?	FL98219A	3847673	481254	Pakhna
CY9709	3856590	487900	?	FL98220	3846092	480339	Pakhna
CY9710	3856590	487900	?	FL98222	3842511	479742	Pakhna
CY9711	3854020	488020	?	FL98223A	3841925	479638	Pakhna
CY9712	3854550	486580	?	FL98225A	3839085	478406	Pakhna
CY9713	3854550	486580	?	FL98226	3840536	494153	Pakhna
CY9714	3853200	484775	?	FL98228	3842115	493364	Pakhna
CY9715	3851075	484150	?	FL98229A	3842271	492773	Pakhna
CY9721	3837700	491800	?	FL98230	3842922	492235	Pakhna
CY9722	3840000	485850	?	FL98231A	3843861	492351	Pakhna
CY9723	3836525	466600	?	FL98232	3844565	492617	Pakhna
CY9724	3836800	466100	?	FL98233A	3844565	492617	Pakhna
CY9725	3840525	460850	?	FL98234	3846550	491806	Pakhna
CY9726	3840525	460850	?	FL98237A	3847019	492281	Pakhna
CY9727A	3840525	460850	?	FL98238	3847275	491572	Pakhna
CY9727B	3853520	450600	?	FL98239A	3848215	491436	Pakhna
CY9728	3855825	451600	?	FL98240	3848712	490936	Pakhna
CY9729	3857450	452620	?	FL98241A	3849639	490008	Pakhna
CY9730	3859400	452810	?	FL98242	3850396	489979	Pakhna
CY9731	3859400	452810	?	FL98243A	3852950	487920	Pakhna
CY9732	3864700	447175	?	FL98244	3852838	487811	Pakhna
CY9748	3879650	508975	?	FL98245A	3852613	486880	Pakhna
CY9749	3878700	510000	?	FL98246	3851892	486643	Pakhna
CY9750	3878700	510000	?	FL98248	3851204	486149	Pakhna
CY9751	3878200	517900	?	FL98249A	3850751	485832	Pakhna
CY9752	3843100	499050	?	FL98250	3850271	485229	Pakhna
CY9766	3845650	507600	?	FL98253A	3 <b>8491</b> 81	484552	Pakhna
FL98004	3846302	507713	Lefkara	FL98254	3841947	459400	Pakhna
FL98005	3846302	507713	Lefkara	FL98255	3842926	460941	Pakhna
FL98006	3846241	507764	Lefkara	FL98256	3843319	461842	Pakhna
FL98015	3845847	508559	Lefkara	FL98257A	3843535	463075	Pakhna
FL98016	3845741	508435	Lefkara	FL98259A	3852590	474566	Lefkara
FL98024	3844559	508056	Lefkara	FL98260	3853136	474579	Lefkara
FL98027	3843069	511336	Pakhna	FL98261A	3853136	474579	Lefkara
FL98031A	3843239	511721	Lefkara	FL98272	3853891	478898	Lefkara
FL98036	3849151	502799	Lefkara	FL98273	3854789	479207	Lefkara
FL98054	3850910	499887	Lefkara	FL98275	3855879	478561	Lefkara
FL98060	3852513	528236	Lefkara	FL98279A	3857177	475178	Lefkara
FL98061A	3852442	527241	Lefkara	FL98280	3857404	475118	Lefkara
FL98067A	3853393	532861	Lefkara	FL98281	3857670	473832	Pakhna
FL98070	3854132	532583	Lefkara	FL98282	3854594	471199	Lefkara
FL98074	3854931	531541	Lefkara	FL98283A	3854027	471365	Lefkara

Ap	pendix	4	-Regiona	l Area	Sample	Location	and	Formati	on

Sample	Northing	Easting	Formation	Sample	Northing	Easting	Formation
FL98083A	3856493	528292	Lefkara	FL98287	3850032	466538	Lefkara
FL98084	3856525	528556	Lefkara	FL98288	3849534	465813	Lefkara
FL98085A	3856420	528 <b>8</b> 55	Lefkara	FL98289A	3846154	463102	Lefkara
FL98086	3856880	528627	Lefkara	FL98290	3842359	459795	Pakhna
FL98087A	3851003	496704	Pakhna	FL98291A	3842534	458685	Pakhna
FL98088	3850846	496397	Pakhna	FL98296	3848945	460364	Lefkara
FL98089A	3850611	496535	Pakhna	FL98297	3849302	460542	Lefkara
FL98090	3850163	496865	Pakhna	FL98298	3849879	460670	Lefkara
FL98091A	3849509	496962	Pakhna	FL98299	3850384	460417	Lefkara
FL98093A	3847540	496983	Pakhna	FL98300	3851422	459916	Lefkara
FL98094	3846575	497269	Pakhna	FL98301A	3850822	<b>45888</b> 8	Kalavasos
FL98095	3844816	497936	Pakhna	FL98302	3850071	458666	Lefkara
FL98096	3844673	498575	Pakhna	FL98304	3849544	458688	Lefkara
FL98097A	3844006	498581	Pakhna	FL98305A	3854529	462776	Pakhna
FL98098	3843645	498885	Pakhna	FL98306	3855032	463100	Lefkara
FL98099A	3842967	498901	Pakhna	FL98307A	3855442	463667	Lefkara
FL98100	3842513	498861	Pakhna	FL98308	3859432	465364	Lefkara
FL98101A	3851978	490941	Pakhna	FL98309A	3860760	464810	Pakhna
FL98102	3854813	489940	Lefkara	FL98310	3861184	464853	Pakhna
FL98103	3855783	489580	Lefkara	FL98311A	3861789	465004	Pakhna
FL98104B	3855927	489549	Lefkara	FL98312	3863086	465187	Lefkara
FL98105A	3856094	489345	Lefkara	FL98313A	3864318	466279	Lefkara
FL98106	3855848	489824	Lefkara	FL98315A	3860682	464565	Pakhna
FL98107A	3856106	490038	Lefkara	FL98316	3859396	464787	Pakhna
FL98108	3856215	489753	Lefkara	FL98317A	3859555	461353	Pakhna
FL98109A	3856769	489552	Lefkara	FL98318	3859642	460704	Pakhna
FL98110	3857419	486310	Lefkara	FL98319A	3859323	460223	Pakhna
FL98113A	3846318	507645	Lefkara	FL98320	3856679	457034	Pakhna
FL98114	3846047	507758	Pakhna	FL98321A	3853559	450343	Lefkara
FL98115A	3845872	507670	Pakhna	FL98322	3854003	451239	Pakhna
FL98116	3845840	507665	Pakhna	FL98323A	3854807	451438	Pakhna
FL98117A	3845734	507812	Pakhna	FL98324	3855423	451497	Pakhna
FL98118	3845598	507825	Pakhna	FL98325A	3853893	453613	Pakhna
FL98119A	3845037	507577	Pakhna	FL98326	3853421	453726	Pakhna
FL98121A	3844716	507692	Pakhna	FL98327A	3853005	454292	Pakhna
FL98122	3844767	507586	Pakhna	FL98328	3856273	451685	Pakhna
FL98126	3842814	507713	Pakhna	FL98329A	3856634	452423	Pakhna
FL98128	3845484	497096	Pakhna	FL98330	3857463	452473	Pakhna
FL98136	3846179	495940	Pakhna	FL98331A	3858266	452740	Pakhna
FL98137A	3846347	495675	Pakhna	FL98332	3859494	452649	Pakhna
FL98138	3846734	495446	Pakhna	FL98333A	3861226	451767	Kalavasos
FL98139A	3846734	495446	Pakhna	FL98334	3861940	449963	Nicosia
FL98140	3846879	495347	Pakhna	FL98335A	3862528	449102	Pakhna
FL98141A	3846879	495347	Pakhna	FL98336	3863331	448247	Pakhna
FL98142	3847364	494989	Pakhna	FL98337A	3863250	447145	Pakhna
FL98146	3847158	494021	Pakhna	FL98338	3862728	446160	Pakhna
FL98147A	3846643	493428	Pakhna	FL98339A	3862437	445396	Pakhna
FL98148	3846641	492921	Pakhna	FL98340	3861900	444029	Pakhna
FL98149A	3838655	494008	Pakhna	FL98341A	3861814	442806	Pakhna

Ap	pendix	4	-Regional	Area	Sampl	е	Location	and	For	natior	۱

Sample	Northing	Easting	Formation	Sample	Northing	Easting	Formation
FL98153A	3839813	485703	Pakhna	FL98346	3848853	492265	Pakhna
FL98154	3839336	484642	Pakhna	FL98347A	3854248	492445	Lekfara
FL98156	3839336	484642	Pakhna	FL98348	3854538	491855	Lefkara
FL98157A	3837415	481937	Pakhna	FL98349A	3855115	491610	Lefkara
FL98158	3837939	479151	Pakhna	FL98350	3840800	505200	Kalavasos
FL98159A	3837939	479151	Pakhna	FL98352	3841591	508681	Pakhna
FL98160A	3837860	475223	Nicosia	FL98353A	3841297	511693	Pakhna
FL98161A	3837860	475223	Nicosia	FL98354	3842260	512394	Pakhna
FL98162A	3837771	473189	Nicosia	FL98355	3840913	512703	Pakhna
FL98166	3836443	469359	Lefkara	FL98356	3865568	448443	Pakhna
FL98167A	3835262	467671	Lefkara	FL98357A	3864907	448676	Pakhna
FL98168	3835262	467671	Lefkara	FL98358	3865239	448957	Pakhna
FL98169A	3835479	467088	Lefkara	FL98359A	3866560	449166	Pakhna
FL98170	3836222	466468	Lefkara	FL98360B	3867889	449674	Nicosia
FL98171	3836044	489657	Reef	FL98361A	3869361	450218	Nicosia
FL98172	3836363	489372	Pakhna	FL98363A	3875068	446218	Nicosia
FL98173A	3837089	486410	Pakhna	FL98364C	3872516	445626	Nicosia
FL98174	3836740	484068	Pakhna	FL98365	3871152	445731	Pakhna
FL98175A	3837126	483453	Pakhna	FL98366	3866855	445433	Pakhna
FL98176	3837957	484309	Pakhna	FL98367A	3865355	446835	Pakhna
FL98177A	3836978	483111	Nicosia	FL98368	3837963	471439	Pakhna
FL98179	3835796	468256	Pakhna	FL98369A	3841124	471423	Nicosia
FL98180	3835796	468256	Pakhna	FL98370	3841679	474531	Pakhna
FL98181A	3837178	463819	Pakhna	FL98371A	3841679	474531	Pakhna
FL98182	3837178	463819	Pakhna	FL98372	3842015	517144	Pakhna
FL98183A	3842253	463594	Pakhna	FL98373A	3842015	517144	Lefkara
FL98184	3842440	463883	Pakhna	FL98374	3842015	517144	Lefkara
FL98185A	3842698	464633	Pakhna	FL98379A	3840672	524593	Lefkara
FL98186	3843092	465260	Pakhna	FL98383	3846981	527531	Pakhna
FL98187A	3843248	466811	Pakhna	FL98388	3847894	525957	Lefkara
FL98188A	3844612	468071	Reef	FL98389A	3847663	525144	Lefkara
FL98190	3845359	470448	Lefkara	FL98390	3847867	524444	Lefkara
FL98191A	3845622	471439	Pakhna	GBFL001A	3861640	546700	Lefkara
FL98192	3847322	4/3074	Pakhna	GBFL002	3861750	545850	Lefkara
FL98193A	3847853	474235	Pakhna	GBFL003A	3863000	544100	Lefkara
FL98194	3848564	4/51/0	Pakhna	GBFL004	3862300	543640	Lefkara
FL98195	3849525	476037	Pakhna	GBFL005	3863050	542420	Lefkara
FL98196	3850851	476326	Paknna	GBFL006	3866340	545600	Letkara
FL98198	3851837	4/8564	Paknna	GBFL007A	3865500	548380	Letkara
FL98199A	3852445	479452	Pakhna	GBFL008	3864980	549900	Letkara
FL98200	3839371	491026	Paknna	GBFLUTU	3864259	550621	Ракпла
FL98201	3840419	490113	Paknna				
FL98202	3847340	490098	Pakhna				
FL98203A	3842847	489860	Paknna				
FL98204	38444/6	488807	Pakhna				
FL98205A	30403/4	406221	Paknna				
	3040/14	485654	Paknna				
FL9020/	304/302	404050	Ракппа				

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90

Pakhna

484592

FL98208 3848709

		Minimum		Interm	ediate	Maximum			
Sample FL1 (I)	Declination	Inclination	Intensity	Dec.	Inc.	Intensity	Dec.	Inc.	Intensity
FL98342A	350.8	43.4	-26.6	248.8	12.5	-26.3	146.5	43.9	-25.6
FL98342B	226.2	19.9	-25.4	14.6	67.0	-24.7	132.1	11.1	-24.4
FL98342C	53.8	25.9	-26.4	265.8	60.2	-25.9	150.6	13.7	-25.6
FL98341B	233.7	60.6	-12.9	360.0	18.4	-12.3	97.7	22.0	-12.3
FL98343B	189.0	85.2	72.6	295.7	1.4	75.2	25.8	4.6	76.4
FL98340A	94.0	61.9	5.8	282.0	29.5	6.5	190.2	3.3	6.9
FL98340B	84.8	54.7	6.6	180.4	4.0	7.6	273.2	35.1	7.7
FL98340C	256.2	82.3	3.8	43.8	7.3	4.3	134.3	5.7	4.6
FL98340D	180.0	45.0	5.5	38.9	37.9	5.6	292.0	20.5	5.9
FL98339B	259.4	72.1	9.8	134.8	10.4	10.5	42.1	14.4	10.9
FL98339C	239.3	52.8	14.6	89.5	33.3	15.1	349.5	14.7	15.5
FL98339D	277.8	48.9	10.5	18.0	8.8	11.1	115.4	39.8	11.2
FL98367B	310.7	27.8	-24.8	56.7	27.6	-23.9	183.5	48.9	-22.5
FL98365B	130.9	1.3	-33.4	222.8	55.3	-29.0	40.0	34.6	-25.0
FL98366A	278.6	42.6	2.8	166.6	22.1	5.1	57.3	39.2	7.5
FL98366B	46.2	46.3	7.9	297.0	17.4	11.2	192.6	38.5	12.4
FL98366C	101.5	72.5	11.0	260.6	16.4	11.1	352.4	5.9	11.4
FL98338B	124.8	57.2	-3.4	269.0	27.6	-2.8	7.8	16.3	-2.3
FL98338C	33.6	65.9	-4.0	278.6	10.7	-3.7	184.3	21.4	-3.3
FL98363B	126.2	77.5	38.1	286.0	11.8	39.1	16.9	4.2	39.5
FL98364A	225.3	53.5	32.9	91.8	27.0	33.8	349.6	22.6	34.2
FL98364B	66.2	82.2	27.4	283.5	6.2	28.2	193.0	4.7	29.1
FL98364C	11.2	76.1	38.0	246.5	8.0	39.3	154.9	11.3	40.1
FL98368A	331.6	26.3	-22.6	218.0	39.0	-21.9	85.8	39.7	-20.9
FL98368B	176.9	23.9	-23.6	287.9	39.0	-19.9	63.7	41.5	-19.8
FL98368C	152.9	81.2	-40.8	5.8	7.4	-17.0	275.1	4.7	-8.2
FL98337B	15.8	11.6	-20.3	262.0	63.0	-19.9	111.1	24.0	-19.6
CY9732A	276.7	63.4	-10.7	77.0	25.3	-10.5	170.7	7.9	-10.0
CY9732B	300.5	46.2	-11.0	80.9	36.4	-10.8	187.2	20.8	-10.5
CY9732C	246.0	74.4	-10.1	83.6	14.9	-9.7	352.4	4.5	-9.2
CY9732D	90.0	90.0	-10.9	90.0	90.0	-10.7	270.0	90.0	-9.9
CY9732D	97.8	7.8	-10.8	195.4	44.0	-10.5	360.0	45.0	-10.4
CY9732E	55.0	65.3	-7.9	301.8	10.3	-7.6	207.5	22.2	-7.5
FL98336A	79.8	8.1	6.0	175.6	35.2	6.5	338.7	53.6	6.8
FL98336B	163.9	60.4	2.6	350.1	29.4	3.2	258.6	2.7	3.4
FL98356B	289.2	61.9	2.2	43.2	12.2	3.1	138.9	24.9	3.5
FL98356C	262.5	62.3	3.0	43.4	22.2	3.7	140.0	15.8	4.1
FL98357B	104.2	68.2	21.5	257.2	19.7	22.2	350.5	9.2	23.5
FL98357C	227.7	77.0	16.8	67.5	12.2	17.8	336.5	4.3	17.9
FL98358A	90.9	40.7	28.9	249.8	47.3	30.2	351.5	10.7	31.6
FL98358B	295.4	86.3	32.3	96.9	3.5	33.0	187.0	1.2	33.9
FL98358C	267.2	54.1	28.8	75.0	35.3	30.0	169.2	5.8	30.3
FL98335B	233.9	54.3	3.2	82.3	32.3	3.4	343.5	13.5	4.0
FL98335C	225.8	70.0	10.4	110.8	8.8	10.9	17.9	17.9	11.7
FL98359B	276.9	47.9	3.7	100.0	42.0	4.5	8.6	1.6	5.0
FL98359D	299.6	78.3	4.0	102.9	11.2	4.7	193.5	3.3	5.5
FL98360A	209.5	72.7	10.3	76.4	12.0	10.8	343.7	12.2	11.5

Appendix	5 -	Regional	Magnetic	Fabric	Data

		Minimum			Interm	ediate	Maximum		
Sample	Declination	Inclination	Intensity	Dec.	Inc.	Intensity	Dec.	Inc.	Intensity
FL98360B	248.3	61.9	3.4	139.9	9.5	4.1	45.2	26.2	4.7
FL98334A	242.6	47.6	31.1	66.7	42.3	31.9	334.9	2.1	32.2
FL98334B	211.8	81.4	28.0	104.5	2.6	28.8	14.2	8.2	29.2
FL98334C	258.3	46.1	30.8	137.6	26.2	32.1	29.4	32.3	33.6
FL98361B	338.7	88.4	187.5	139.1	1.5	191.8	229.1	0.5	192.4
FL98361C	203.8	80.6	266.2	305.6	1.9	270.3	35. <del>9</del>	9.2	271.5
FL98321B	335.9	79.0	-14.1	113.9	8.2	-13.4	205.0	7.2	-12.4
FL98321C	263.1	25.8	-10.2	111.4	61.2	-9.9	358.9	11.9	-9.4
CY9727B	210.5	74.2	13.2	54.8	14.5	13.6	323.2	6.2	14.4
CY9727B1	238.2	74.4	7.3	78.2	14.7	7.9	346.8	5.1	8.3
CY9727B3	165.7	58.4	15.4	331.7	30.9	15.7	65.5	6.3	16.0
CY9727B4	194.8	69.2	18.6	89.5	5.7	19.1	357.4	19.9	19.7
CY9727B5	197.0	64.8	19.3	56.9	19.9	19.9	321.4	14.9	20.3
FL98322A	212.2	0.6	-11.4	122.0	12.1	-11.2	305.2	77.8	-9.6
FL98322B	103.8	58.7	-18.8	266.7	30.1	-18.4	1.2	7.6	-17.8
FL98322C	244.3	75.3	-19.2	74.6	14.5	-18.8	343.9	2.5	-18.0
FL98322D	232.9	2.9	-12.1	336.5	78.0	-12.0	142.3	11.7	-11.7
FL98323B	72.8	36.6	-29.5	228.0	50.7	-29.4	333.5	12.3	-28.5
FL98324A	267.0	47.1	11.6	97.9	42.4	11.7	2.9	5.4	13.3
FL98324B	3.5	37.6	12.2	249.1	28.2	12.6	132.9	39.5	14.2
FL98324C	226.1	11.4	11.7	14.0	76.6	12.0	134.7	6.9	12.8
CY9728A	300.9	77.0	26.0	100.1	12.2	26.6	191.0	4.5	27.2
CY9728B	360.0	84.3	35.7	180.0	0.0	37.2	180.0	5.7	37.2
CY9728B	39.6	71.9	35.9	130.4	0.3	36.6	220.5	18.1	38.1
CY9728C	279.8	66.1	47.1	74.7	21.9	47.5	168.5	9.2	48.6
CY9728C	180.0	5.7	46.1	0.0	84.3	47.6	360.0	85.7	48.1
CY9728D	292.4	65.3	33.4	53.8	13.5	34.2	148.8	20.3	34.5
CY9728E	64.5	77.2	27.6	246.0	12.8	28.3	155.9	0.3	28.9
FL98328A	214.7	80.0	15.7	109.3	2.7	16.2	18.9	9.6	16.7
FL98328B	268.7	81.0	16.7	62.6	8.1	17.3	153.2	3.9	17.9
FL98328C	245.0	66.5	12.6	92.6	21.0	13.8	358.8	9.9	14.1
FL98328D	290.1	59.4	16.5	107.3	30.6	17.2	198.0	1.2	17.9
FL98333B	263.2	24.4	-34.1	105.4	63.9	-33.8	357.2	8.7	-33.6
FL98329B	275.7	2.7	15.1	160.3	83.7	15.8	5.9	5.7	16.2
FL98329C	282.9	58.4	19.2	116.0	31.0	19.7	22.5	5.8	20.0
FL98329D	260.9	82.0	21.3	88.3	7.9	22.1	358.2	1.0	23.2
FL98330A	222.1	64.9	9.8	99.7	14.1	10.4	4.3	20.3	11.1
FL98330B	239.3	52.0	8.2	123.0	19.1	8.8	20.8	31.4	9.0
FL98330C	153.4	65.9	10.6	280.7	15.2	11.0	15.8	18.3	11.9
CY9729A	57.6	<b>8</b> 1. <b>1</b>	13.4	260.9	8.2	14.0	170.4	3.5	14.4
CY9729A	270.0	90.0	13.5	90.0	90.0	14.2	90.0	90.0	14.5
CY9729B	40.6	75.7	13.2	261.2	10.9	13.7	169.5	9.1	14.1
CY9729C	326.9	56.5	12.9	123.3	31.3	13.2	220.0	10.9	13.3
CY9729D	315.0	70.7	11.0	135.0	0.0	11.9	135.0	19.3	12.0
FL98332A	180.0	75.3	-17.0	0.0	0.0	-16.1	0.0	14.7	-16.0
FL98332A	132.8	30.5	-16.7	330.5	58.2	-16.2	227.5	8.0	-15.9
FL98332B	57.1	42.1	-17.8	169.2	22.7	-17.5	279.3	39.4	-17.0
FL98332C	270.2	57.0	-17.6	62.7	29.9	-16.8	160.1	12.6	-16.0

Appendix 5	5 - č	Regional	Magnetic	Fabric	Data

Sample         Declination         Intensity         Dec.         Intensity         Dec.         Intensity           FL98331E         91.2         80.9         -10.2         220.8         5.9         -9.8         311.5         7.0         -8.9           FL98331C         97.0         68.5         -8.8         205.7         7.2         -8.4         298.4         20.1         -8.2           CY9730A         83.7         64.9         -15.4         266.3         25.1         -15.1         175.7         10.0         -14.6           CY9730B         95.6         20.1         -14.6         331.6         58.8         12.8         -14.0         152.3         33.1         -13.8           CY9731D         95.6         20.1         -14.6         331.6         56.8         13.6         195.5         25.2         -13.0           CY9731D         322.1         18.1         -14.3         147.8         71.8         -14.1         52.7         1.7         -13.8           FL98326B         90.0         90.0         -4.1         200.9         90.0         90.0         90.0         90.0         90.0         90.0         90.0         90.0         90.0         90.0			Minimum			Interm	ediate	Maximum		
FL98331F       91.2       80.9       -10.2       220.8       5.9       -9.8       311.5       7.0       -8.9         FL98331C       97.0       68.5       -8.8       205.7       7.2       -8.4       298.4       20.1       -8.2         CY9730B       287.5       39.2       -15.2       127.3       49.0       -14.9       25.7       10.0       -13.7         CY9730B       287.5       39.2       -16.5       276.5       45.9       -15.5       33.3       23.7       -15.0         CY9731C       282.5       73.5       -15.4       114.1       16.2       -14.7       23.2       3.2       -14.6         CY9731D       222.1       18.1       -14.3       147.8       71.8       -14.1       52.7       1.7       -13.8         FL9332B       97.6       66.8       15.7       294.3       21.6       16.5       201.8       5.8       16.9         FL9332B       97.6       66.8       15.7       294.3       21.6       16.5       201.8       5.8       15.4       147.7       20.4       201.8       5.8       15.4       15.4       12.5       0.8       -3.1       1.9       1.0       -3.0	Sample	Declination	Inclination	Intensity	Dec.	Inc.	Intensity	Dec.	Inc.	Intensity
FL98331C       97.0       68.5       -8.8       205.7       7.2       -8.4       286.4       20.1       -8.2         CY9730A       83.7       64.9       -15.4       266.3       25.1       -15.1       175.8       1.0       -13.7         CY9730B       287.5       33.2       -15.2       127.3       49.0       -14.9       25.7       10.0       -14.6         CY9730C       305.6       53.9       -16.5       276.5       45.9       -15.5       33.3       23.7       -15.0         CY9731D       282.5       73.5       -15.4       114.1       16.2       -14.7       23.2       3.2       -14.6         CY9731D       322.1       18.1       -14.3       147.8       71.8       -14.1       52.7       1.7       -13.8         FL98326B       90.0       90.0       -4.1       90.0       90.0       90.0       90.0       -3.1       F1.983206       31.5       -3.1       F1.983206       33.3       68.8       19.5       128.4       17.7       20.4       21.4       9.4       1.0       -3.0         FL98320E       36.5       85.8       15.4       169.1       2.9       16.0       25.9.3       3	FL98331B	91.2	80.9	-10.2	220.8	5.9	-9.8	311.5	7.0	-8.9
CY9730A       83.7       64.9       -15.4       266.3       25.1       -15.1       17.8       1.0       -13.7         CY9730B       287.5       39.2       -15.2       127.3       49.0       -14.9       25.7       1.00       -14.6         CY9730C       305.6       53.9       -14.3       53.8       12.8       -14.0       152.3       33.1       -13.8         CY9731C       282.5       73.5       -15.4       114.1       162.2       -14.7       23.2       3.2       -14.6         CY9731C       282.5       73.5       -15.4       114.1       162.2       -14.7       23.2       3.2       -14.6         CY9731D       282.1       181       -14.4       3147.8       71.8       71.4       114.1       162.2       71.7       -17.7       -13.8         FL983285       97.6       66.8       15.7       294.3       21.6       16.5       201.8       5.8       16.9         FL983285       97.6       66.8       15.7       294.3       21.6       15.3       3.1       1.0       -3.0         FL983285       97.6       66.8       15.7       29.1       -11.7       2.4       3.1       1.0<	FL98331C	97.0	68.5	-8.8	205.7	7.2	-8.4	298.4	20.1	-8.2
CY9730B       287.5       39.2       -15.2       127.3       49.0       -14.9       25.7       10.0       -14.6         CY9730C       305.6       53.9       -14.3       53.8       12.8       -14.0       152.3       33.1       -13.8         CY9731A       140.9       34.7       -16.5       276.5       45.9       -15.5       33.3       23.7       -15.0         CY9731D       282.5       73.5       -15.4       114.1       162.2       -14.7       23.2       3.2       -14.6         CY9731D       322.1       18.1       -14.3       147.8       71.8       -14.7       23.2       3.2       -14.6         CY9731D       322.1       18.1       -14.3       147.8       71.8       -14.7       23.2       3.2       -14.6         CY9731D       322.1       18.1       -14.3       147.8       71.8       -14.7       3.2       3.2       -14.6         CY9731D       322.1       18.1       -14.3       147.7       20.4       -21.8       5.6       8.8       15.1       18.9       -16.0       2.9       16.0       2.9       16.0       2.9       16.0       2.9       16.0       2.9       14.3	CY9730A	83.7	64.9	-15.4	266.3	25.1	-15.1	175.8	1.0	-13.7
CY9730C         305.6         53.9         -14.3         53.8         12.8         -14.0         152.3         33.1         -13.8           CY9731A         140.9         34.7         -16.5         276.5         45.9         -15.5         33.3         2.37         -15.0           CY9731B         95.6         20.1         -14.6         316.6         56.8         -13.6         195.5         25.2         3.2         -14.6           CY9731C         282.5         73.5         -15.4         114.1         162         -14.7         23.2         3.2         -14.6           CY9731D         322.1         18.1         -14.3         147.8         71.8         71.4         14.7         23.2         1.7         -13.8           FL98326B         90.0         90.0         -4.1         90.0         90.0         -4.0         90.0         90.0         -3.6           FL98320A         38.3         69.8         19.5         128.4         17.7         20.4         221.4         9.4         21.0           FL98320A         38.6         34.5         -14.1         210.5         23.3         1.16.2         1.10.8         112.1         13.5         32.1         1.16.2 <td>CY9730B</td> <td>287.5</td> <td>39.2</td> <td>-15.2</td> <td>127.3</td> <td>49.0</td> <td>-14.9</td> <td>25.7</td> <td>10.0</td> <td>-14.6</td>	CY9730B	287.5	39.2	-15.2	127.3	49.0	-14.9	25.7	10.0	-14.6
CY9731A       140.9       34.7       -16.5       276.5       45.9       -15.5       33.3       23.7       -15.0         CY9731C       282.5       73.5       -15.4       114.1       16.2       -14.7       23.2       3.2       -14.6         CY9731C       282.5       73.5       -15.4       114.1       16.2       -14.7       23.2       3.2       -14.6         CY9731D       322.1       18.1       -14.3       147.8       71.8       -14.7       23.2       3.2       -14.6         CY9731D       322.1       18.1       -14.3       147.8       71.8       -14.7       23.2       3.2       -14.6         CY9731D       322.1       18.1       -14.3       147.8       71.8       -14.7       23.2       3.2       -14.6         CY9320B       97.6       66.8       15.7       29.3       16.1       2.9       16.0       25.0       8.3       1.1       -13.3         FL98322B       36.5       85.8       15.4       16.91       2.9       16.0       259.3       3.1       16.2         FL98302C       306.0       78.5       -14.3       48.1       2.4       -14.0       138.6       11.2 <td>CY9730C</td> <td>305.6</td> <td>53.9</td> <td>-14.3</td> <td>53.8</td> <td>12.8</td> <td>-14.0</td> <td>152.3</td> <td>33.1</td> <td>-13.8</td>	CY9730C	305.6	53.9	-14.3	53.8	12.8	-14.0	152.3	33.1	-13.8
CY9731B         95.6         20.1         -14.6         331.6         56.8         -13.6         195.5         25.2         -13.0           CY9731C         282.5         73.5         -15.4         114.1         16.2         -14.7         23.2         3.2         -14.6           CY9731D         322.1         18.1         -14.3         147.8         71.8         -14.1         52.7         1.7         -13.8           FL98326B         90.0         -4.1         90.0         90.0         -4.0         90.0         90.0         -3.6           FL98326B         115.1         38.3         -4.7         293.1         51.7         -3.7         24.3         1.0         -3.0           FL98320B         38.3         69.8         19.5         12.84         17.7         20.4         22.1         9.4         21.0         9.4         21.0         -3.0           FL98320B         36.5         85.8         15.4         169.1         2.9         16.0         25.9.3         3.1         16.2           FL98320D         79.4         29.2         -16.7         22.0         54.2         -16.5         33.8         16.9         5.5         33.3         16.9 <t< td=""><td>CY9731A</td><td>140.9</td><td>34.7</td><td>-16.5</td><td>276.5</td><td>45.9</td><td>-15.5</td><td>33.3</td><td>23.7</td><td>-15.0</td></t<>	CY9731A	140.9	34.7	-16.5	276.5	45.9	-15.5	33.3	23.7	-15.0
CY9731C       282.5       73.5       -15.4       114.1       16.2       -14.7       23.2       3.2       -14.6         CY9731D       282.1       18.1       -14.3       147.8       71.8       -14.7       23.2       3.2       -14.6         CY9731D       322.1       18.1       -14.3       147.8       71.8       -14.7       23.2       3.2       -14.6         CY9731D       322.1       18.1       -74.3       147.8       71.8       -14.7       23.2       3.2       -14.6         FL98326B       90.0       90.0       -4.1       90.0       90.0       -4.0       90.0       90.0       -3.6         FL98326B       15.1       38.3       -4.7       293.1       51.7       -3.7       24.3       1.0       -3.0         FL98320B       36.5       85.8       15.4       169.1       2.9       16.0       25.9.3       3.1       16.2         FL98320C       306.0       78.5       -14.3       48.1       2.4       -14.0       138.6       11.2       -13.2         FL98320C       189.7       66.2       -13.9       30.90.0       12.2       -13.1       43.6       20.1       -14.3       32.	CY9731B	95.6	20.1	-14.6	331.6	56.8	-13.6	195.5	25.2	-13.0
CY9731C       282.5       73.5       -15.4       114.1       16.2       -14.7       23.2       3.2       -14.6         CY9731D       322.1       18.1       -14.3       147.8       71.8       -14.1       52.7       1.7       -13.8         FL98325B       97.6       66.8       15.7       294.3       21.6       16.5       201.8       5.8       16.9         FL98326B       115.1       38.3       -4.7       293.1       51.7       -3.7       24.3       1.0       -3.0         FL98320B       36.5       85.8       15.4       169.1       2.9       16.0       259.3       3.1       16.2         FL98320D       38.6       34.5       -14.7       270.4       54.0       -14.7       27.9       25.1       -14.3         FL98302C       306.0       78.5       -14.3       48.1       2.4       -14.0       138.6       11.2       -13.2         FL98302D       189.7       66.2       -33.9       30.9       12.2       -13.1       43.6       20.1       -12.8         FL98201B       302.6       75.2       31.6       95.3       13.2       33.1       186.9       6.5       33.3 <t< td=""><td>CY9731C</td><td>282.5</td><td>73.5</td><td>-15.4</td><td>114.1</td><td>16.2</td><td>-14.7</td><td>23.2</td><td>3.2</td><td>-14.6</td></t<>	CY9731C	282.5	73.5	-15.4	114.1	16.2	-14.7	23.2	3.2	-14.6
CY9731D       322.1       18.1       -14.3       147.8       71.8       -14.1       52.7       1.7       -13.8         FL98326B       97.6       66.8       15.7       294.3       21.6       16.5       201.8       5.8       16.9         FL98326B       115.1       38.3       -4.7       293.1       51.7       -3.7       24.3       1.0       -3.0         FL98326A       38.3       69.8       19.5       128.4       17.7       20.4       221.4       9.4       21.0         FL98320A       38.6       34.5       -14.7       270.0       45.0       -14.7       27.9       25.1       -14.3         FL98302A       136.6       34.5       -14.7       270.0       45.0       -14.0       138.4       18.9       -15.3         FL98302D       189.7       66.2       -13.9       309.0       12.2       -13.1       43.6       20.1       -12.8         FL98202D       189.7       66.2       -13.9       309.0       12.2       -13.1       43.6       20.1       -12.8         FL98201C       102.7       78.4       30.7       261.3       10.8       31.5       352.1       4.1       32.1	CY9731C	282.5	73.5	-15.4	114.1	16.2	-14.7	23.2	3.2	-14.6
FL98325B97.666.815.7294.321.616.5201.85.816.9FL98326B90.090.0-4.190.090.0-4.090.090.0-3.6FL98326B115.138.3-4.7293.151.7-3.724.31.0-3.0FL98327C103.451.9-4.1281.938.0-3.912.50.8-3.1FL98320A38.369.819.5128.417.720.4221.49.421.0FL98302B36.585.815.4169.12.916.0250.33.116.2FL98302B136.634.5-14.727.045.0-14.727.925.1-14.3FL98302D136.766.2-13.9309.012.2-13.143.620.1-12.8FL98202D189.766.2-13.9309.012.2-13.143.620.1-12.8FL98201D102.778.430.7261.310.831.5352.14.132.1FL98301B350.468.0-31.3174.421.9-30.883.81.4-30.5FL98301D225.056.2-27.4225.035.3-27.045.033.8-26.4FL98301D255.653.4-31.795.035.1-31.6358.49.4-30.5FL98301D255.653.4-31.9171.243.6-13.458.422.2-13.0 </td <td>CY9731D</td> <td>322.1</td> <td>18.1</td> <td>-14.3</td> <td>147.8</td> <td>71.8</td> <td>-14.1</td> <td>52.7</td> <td>1.7</td> <td>-13.8</td>	CY9731D	322.1	18.1	-14.3	147.8	71.8	-14.1	52.7	1.7	-13.8
FL98326B90.090.0-4.190.090.0-4.090.090.0-3.6FL98326B115.138.3-4.7293.151.7-3.724.31.0-3.0FL98327C103.451.9-4.1281.938.0-3.912.50.8-3.1FL98320A338.369.819.5128.417.720.4221.49.421.0FL98302A136.634.5-14.7270.045.0-14.727.925.1-14.3FL98302B79.429.2-16.720.254.2-16.5338.418.9-15.3FL98302C306.078.5-14.348.12.4-14.0138.611.2-13.2FL98302D189.766.2-13.9309.012.2-13.143.620.1-12.8FL98201B302.675.231.695.313.233.1186.96.533.3FL98201B302.675.231.665.313.233.1186.96.533.3FL98301B350.468.0-31.3174.421.9-30.883.81.4-30.5FL98301C25.056.2-27.425.035.3-27.045.033.8-26.4FL98301C25.653.4-31.795.035.1-31.6358.49.4-30.5FL98301D25.653.4-37.8237.114.839.0145.94.439.4 <td>FL98325B</td> <td>97.6</td> <td>66.8</td> <td>15.7</td> <td>294.3</td> <td>21.6</td> <td>16.5</td> <td>201.8</td> <td>5.8</td> <td>16.9</td>	FL98325B	97.6	66.8	15.7	294.3	21.6	16.5	201.8	5.8	16.9
FL98326B115.138.3-4.7293.151.7-3.724.31.0-3.0FL98327C103.451.9-4.1281.938.0-3.912.50.8-3.1FL98320A336.369.819.5128.417.720.4221.49.421.0FL98320B36.585.8154169.12.916.0259.33.116.2FL98302A136.634.5-14.7270.045.0-14.727.925.1-14.3FL98302D306.078.5-14.348.12.4-14.0138.611.2-13.2FL98302D189.766.2-13.9309.012.2-13.143.620.1-12.8FL98291D102.778.430.7261.310.831.5352.14.132.1FL98304B325.163.0-10.8218.28.4-10.6124.225.5-10.3FL98301D255.653.4-31.3174.421.9-30.883.81.4-30.5FL98301D255.653.4-31.795.035.1-31.6358.49.4-30.5FL98301D255.653.4-31.9171.243.6-13.458.422.2-13.0FL9820A39.638.2-13.9171.243.6-13.458.422.2-13.0FL98301D255.653.4-31.795.035.1-31.6358.49.4-30.5<	FL98326B	90.0	90.0	-4.1	90.0	90.0	-4.0	90.0	90.0	-3.6
FL98327C103.451.9-4.1281.938.0-3.912.50.8-3.1FL98320A33.369.819.5128.417.720.4221.49.421.0FL98320B36.585.815.4169.12.916.0259.33.116.2FL98302B136.634.5-14.7270.045.0-14.727.925.1-14.3FL98302D306.078.5-14.348.12.4-14.0138.611.2-13.2FL98302D189.766.2-13.9309.012.2-13.143.620.1-12.8FL98291B302.675.231.695.313.233.1186.96.533.3FL98291D102.778.430.7261.310.831.5352.14.132.1FL98304A281.326.2-11.8160.446.3-11.729.332.1-11.4FL98304B352.163.0-10.8218.28.4-10.6124.225.5-10.3FL98301D350.468.0-31.3174.421.9-30.883.81.4-30.5FL98301D255.653.4-31.795.035.1-31.6358.49.4-40.5FL98200D24.576.919.3269.312.620.2178.63.221.3FL98200D24.576.919.3269.312.620.2178.63.221.3<	FL98326B	115.1	38.3	-4.7	293.1	51.7	-3.7	24.3	1.0	-3.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	FL98327C	103.4	51.9	-4.1	281.9	38.0	-3.9	12.5	0.8	-3.1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	FL98320A	338.3	69.8	19.5	128.4	17.7	20.4	221.4	9.4	21.0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	FL98320B	36.5	85.8	15.4	169.1	2.9	16.0	259.3	3.1	16.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	FL98302A	136.6	34.5	-14.7	270.0	45.0	-14.7	27.9	25.1	-14.3
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	FL98302B	79.4	29.2	-16.7	220.2	54.2	-16.5	338.4	18.9	-15.3
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	FL98302C	306.0	78.5	-14.3	48.1	2.4	-14.0	138.6	11.2	-13.2
FL98291B $302.6$ $75.2$ $31.6$ $95.3$ $13.2$ $33.1$ $186.9$ $6.5$ $33.3$ FL98291C $102.7$ $78.4$ $30.7$ $261.3$ $10.8$ $31.5$ $352.1$ $4.1$ $32.1$ FL98304A $281.3$ $26.2$ $-11.8$ $160.4$ $46.3$ $-11.7$ $29.3$ $32.1$ $-11.4$ FL98304B $325.1$ $63.0$ $-10.8$ $218.2$ $8.4$ $-10.6$ $124.2$ $25.5$ $-10.3$ FL98301C $225.0$ $56.2$ $-27.4$ $225.0$ $35.3$ $-27.0$ $45.0$ $33.8$ $-26.4$ FL98301C $134.5$ $8.3$ $-27.3$ $26.2$ $65.0$ $-26.6$ $228.1$ $23.4$ $-26.5$ FL98301D $255.6$ $53.4$ $-31.7$ $95.0$ $35.1$ $-31.6$ $358.4$ $9.4$ $-30.5$ FL9829A $74.5$ $76.9$ $19.3$ $269.3$ $12.6$ $20.2$ $178.6$ $3.2$ $21.3$ FL9829DC $221.2$ $3.3$ $20.2$ $131.0$ $2.7$ $21.1$ $2.2$ $85.8$ $23.1$ FL9829DC $221.2$ $3.3$ $20.2$ $131.0$ $2.7$ $21.1$ $2.2$ $85.8$ $23.1$ FL9829DC $222.2$ $73.5$ $5.7$ $249.1$ $13.9$ $6.6$ $341.3$ $8.6$ $7.1$ FL9829DA $263.7$ $71.6$ $-3.5$ $166.6$ $2.4$ $-2.9$ $75.8$ $18.3$ $-2.6$ FL9829BC $294.7$ $74.5$ $6.4$ $122.0$ <td>FL98302D</td> <td>189.7</td> <td>66.2</td> <td>-13.9</td> <td>309.0</td> <td>12.2</td> <td>-13.1</td> <td>43.6</td> <td>20.1</td> <td>-12.8</td>	FL98302D	189.7	66.2	-13.9	309.0	12.2	-13.1	43.6	20.1	-12.8
FL98291C102.778.430.7261.310.831.5352.14.132.1FL98304A281.326.2-11.8160.446.3-11.729.332.1-11.4FL98304B325.163.0-10.8218.28.4-10.6124.225.5-10.3FL98301C225.056.2-27.4225.035.3-27.045.033.8-26.4FL98301C134.58.3-27.326.265.0-26.6228.123.4-26.5FL98301D255.653.4-31.795.035.1-31.6358.49.4-30.5FL98290A74.576.919.3269.312.620.2178.63.221.3FL98290B341.681.619.3161.68.420.2151.446.120.3FL98290C221.23.320.2131.02.721.12.285.823.1FL98300B37.774.537.8237.114.839.0145.94.439.4FL98300B270.573.437.774.716.038.7166.04.339.1FL2 (II)TTT5.7249.113.96.6341.38.67.1FL98296C185.980.72.573.63.63.234.18.63.5FL98297B171.074.1-9.870.090.0-9.2270.090.0-8.8 <t< td=""><td>FL98291B</td><td>302.6</td><td>75.2</td><td>31.6</td><td>95.3</td><td>13.2</td><td>33.1</td><td>186.9</td><td>6.5</td><td>33.3</td></t<>	FL98291B	302.6	75.2	31.6	95.3	13.2	33.1	186.9	6.5	33.3
FL98304A       281.3       26.2       -11.8       160.4       46.3       -11.7       29.3       32.1       -11.4         FL98304B       325.1       63.0       -10.8       218.2       8.4       -10.6       124.2       25.5       -10.3         FL98301C       225.0       56.2       -27.4       225.0       35.3       -27.0       45.0       33.8       -26.4         FL98301C       134.5       8.3       -27.3       26.2       65.0       -26.6       228.1       23.4       -26.5         FL98301D       255.6       53.4       -31.7       95.0       35.1       -31.6       358.4       9.4       -30.5         FL98290A       74.5       76.9       19.3       269.3       12.6       20.2       178.6       3.2       21.3         FL98290B       341.6       81.6       19.3       161.6       8.4       20.2       151.4       46.1       20.3         FL98290C       221.2       3.3       20.2       131.0       2.7       21.1       2.2       85.8       23.1         FL98290D       39.7       74.5       37.8       237.1       14.8       39.0       145.9       4.4       39.4	FL98291C	102.7	78.4	30.7	261.3	10.8	31.5	352.1	4.1	32.1
FL98304B $325.1$ $63.0$ $-10.8$ $218.2$ $8.4$ $-10.6$ $124.2$ $25.5$ $-10.3$ FL98301B $350.4$ $68.0$ $-31.3$ $174.4$ $21.9$ $-30.8$ $83.8$ $1.4$ $-30.5$ FL98301C $225.0$ $56.2$ $-27.4$ $225.0$ $35.3$ $-27.0$ $45.0$ $33.8$ $-26.4$ FL98301D $255.6$ $53.4$ $-31.7$ $95.0$ $35.1$ $-31.6$ $358.4$ $9.4$ $-30.5$ FL98254C $309.6$ $38.2$ $-13.9$ $171.2$ $43.6$ $-13.4$ $58.4$ $22.2$ $-13.0$ FL98290A $74.5$ $76.9$ $19.3$ $269.3$ $12.6$ $20.2$ $178.6$ $3.2$ $21.3$ FL98290B $341.6$ $81.6$ $19.3$ $161.6$ $8.4$ $20.2$ $151.4$ $46.1$ $20.3$ FL98290C $221.2$ $3.3$ $20.2$ $131.0$ $2.7$ $21.1$ $2.2$ $85.8$ $23.1$ FL98300B $270.5$ $73.4$ $37.7$ $74.7$ $16.0$ $38.7$ $166.0$ $4.3$ $39.1$ FL2 (II)FL2 (II)FL2 (II)FL2 (II)FL98296C $185.9$ $80.7$ $2.5$ $73.6$ $3.6$ $3.2$ $343.1$ $8.6$ $7.1$ FL98296C $185.9$ $80.7$ $2.5$ $73.6$ $3.6$ $3.2$ $343.1$ $8.6$ $7.1$ FL98296C $102.2$ $73.5$ $5$	FL98304A	281.3	26.2	-11.8	160.4	46.3	-11.7	29.3	32.1	-11.4
FL98301B $350.4$ $68.0$ $-31.3$ $174.4$ $21.9$ $-30.8$ $83.8$ $1.4$ $-30.5$ FL98301C $225.0$ $56.2$ $-27.4$ $225.0$ $35.3$ $-27.0$ $45.0$ $33.8$ $-26.4$ FL98301C $134.5$ $8.3$ $-27.3$ $26.2$ $65.0$ $-26.6$ $228.1$ $23.4$ $-26.5$ FL98254C $309.6$ $38.2$ $-13.9$ $171.2$ $43.6$ $-13.4$ $58.4$ $9.4$ $-30.5$ FL98290A $74.5$ $76.9$ $19.3$ $269.3$ $12.6$ $20.2$ $178.6$ $3.2$ $21.3$ FL98290B $341.6$ $81.6$ $19.3$ $161.6$ $8.4$ $20.2$ $151.4$ $46.1$ $20.3$ FL98290C $221.2$ $3.3$ $20.2$ $131.0$ $2.7$ $21.1$ $2.2$ $85.8$ $23.1$ FL98300A $39.7$ $74.5$ $37.8$ $237.1$ $14.8$ $39.0$ $145.9$ $4.4$ $39.4$ FL9830B $270.5$ $73.4$ $37.7$ $74.7$ $16.0$ $38.7$ $166.0$ $4.3$ $39.1$ FL2 (II) $FL2$ (II) $FL2$ (II) $FL2$ (II) $FL320.2$ $75.8$ $18.3$ $-2.6$ FL98296C $282.1$ $58.5$ $5.1$ $83.1$ $27.7$ $5.7$ $345.7$ $13.8$ $6.4$ FL98297B $270.0$ $90.0$ $-9.6$ $270.0$ $90.0$ $-9.2$ $270.0$ $90.0$ $-8.8$ FL98297B $271.0$ $90.0$ $-9.6$ $270.0$ $90.0$	FL98304B	325.1	63.0	-10.8	218.2	8.4	-10.6	124.2	25.5	-10.3
FL98301C $225.0$ $56.2$ $-27.4$ $225.0$ $35.3$ $-27.0$ $45.0$ $33.8$ $-26.4$ FL98301C $134.5$ $8.3$ $-27.3$ $26.2$ $65.0$ $-26.6$ $228.1$ $23.4$ $-26.5$ FL98301D $255.6$ $53.4$ $-31.7$ $95.0$ $35.1$ $-31.6$ $358.4$ $9.4$ $-30.5$ FL98254C $309.6$ $38.2$ $-13.9$ $171.2$ $43.6$ $-13.4$ $58.4$ $22.2$ $-13.0$ FL98290A $74.5$ $76.9$ $19.3$ $269.3$ $12.6$ $20.2$ $178.6$ $3.2$ $21.3$ FL98290B $341.6$ $81.6$ $19.3$ $161.6$ $8.4$ $20.2$ $151.4$ $46.1$ $20.3$ FL98290C $221.2$ $3.3$ $20.2$ $131.0$ $2.7$ $21.1$ $2.2$ $85.8$ $23.1$ FL98300A $39.7$ $74.5$ $37.8$ $237.1$ $14.8$ $39.0$ $145.9$ $4.4$ $39.4$ FL98300B $270.5$ $73.4$ $37.7$ $74.7$ $16.0$ $38.7$ $166.0$ $4.3$ $39.1$ FL2 (II) $FL2$ (II	FL98301B	350.4	68.0	-31.3	174.4	21.9	-30.8	83.8	1.4	-30.5
FL98301C134.58.3 $-27.3$ 26.265.0 $-26.6$ 228.123.4 $-26.5$ FL98301D255.653.4 $-31.7$ 95.035.1 $-31.6$ 358.49.4 $-30.5$ FL98254C309.638.2 $-13.9$ 171.243.6 $-13.4$ 58.422.2 $-13.0$ FL98290A74.576.919.3269.312.620.2178.63.221.3FL98290B341.681.619.3161.68.420.2151.446.120.3FL98290C221.23.320.2131.02.721.12.285.823.1FL98300A39.774.537.8237.114.839.0145.94.439.4FL98300B270.573.437.774.716.038.7166.04.339.1FL2 (II) $-25$ 73.63.63.234.18.67.1FL98296C185.980.72.573.63.63.234.38.67.1FL98299B232.158.55.183.127.75.7345.713.86.4FL98299C294.774.56.4122.015.46.931.51.97.3FL98297B171.074.1-9.870.13.1-9.6339.215.5-8.8FL98297C160.526.0-5.8335.864.0-5.669.61.8-4.8FL98298A78.6	FL98301C	225.0	56.2	-27.4	225.0	35.3	-27.0	45.0	33.8	-26.4
FL98301D255.653.4 $-31.7$ 95.035.1 $-31.6$ 358.49.4 $-30.5$ FL98254C309.638.2 $-13.9$ 171.243.6 $-13.4$ 58.422.2 $-13.0$ FL98290A74.576.919.3269.312.620.2178.63.221.3FL98290B341.681.619.3161.68.420.2151.446.120.3FL98290C221.23.320.2131.02.721.12.285.823.1FL98300A39.774.537.8237.114.839.0145.94.439.4FL98300B270.573.437.774.716.038.7166.04.339.1FL2 (II) $-36.6$ 341.38.67.1FL98296A263.771.6 $-3.5$ 166.62.4 $-2.9$ 75.818.3 $-2.6$ FL98296C185.980.72.573.63.63.2343.18.63.5FL98299B232.158.55.183.127.75.7345.713.86.4FL98299C294.774.56.4122.015.46.931.51.97.3FL98297B171.074.1 $-9.8$ 70.13.1 $-9.6$ 339.215.5 $-8.8$ FL98297C160.526.0 $-5.8$ 335.864.0 $-5.6$ 69.61.8 $-4.8$ <trr< td=""><td>FL98301C</td><td>134.5</td><td>8.3</td><td>-27.3</td><td>26.2</td><td>65.0</td><td>-26.6</td><td>228.1</td><td>23.4</td><td>-26.5</td></trr<>	FL98301C	134.5	8.3	-27.3	26.2	65.0	-26.6	228.1	23.4	-26.5
FL98254C $309.6$ $38.2$ $-13.9$ $171.2$ $43.6$ $-13.4$ $58.4$ $22.2$ $-13.0$ FL98290A $74.5$ $76.9$ $19.3$ $269.3$ $12.6$ $20.2$ $178.6$ $3.2$ $21.3$ FL98290B $341.6$ $81.6$ $19.3$ $161.6$ $8.4$ $20.2$ $151.4$ $46.1$ $20.3$ FL98290C $221.2$ $3.3$ $20.2$ $131.0$ $2.7$ $21.1$ $2.2$ $85.8$ $23.1$ FL98290C $221.2$ $3.3$ $20.2$ $131.0$ $2.7$ $21.1$ $2.2$ $85.8$ $23.1$ FL98300B $39.7$ $74.5$ $37.8$ $237.1$ $14.8$ $39.0$ $145.9$ $4.4$ $39.4$ FL98300B $270.5$ $73.4$ $37.7$ $74.7$ $16.0$ $38.7$ $166.0$ $4.3$ $39.1$ FL98319B $102.2$ $73.5$ $5.7$ $249.1$ $13.9$ $6.6$ $341.3$ $8.6$ $7.1$ FL98296A $263.7$ $71.6$ $-3.5$ $166.6$ $2.4$ $-2.9$ $75.8$ $18.3$ $-2.6$ FL98296C $185.9$ $80.7$ $2.5$ $73.6$ $3.6$ $3.2$ $343.1$ $8.6$ $3.5$ FL98299B $232.1$ $58.5$ $5.1$ $83.1$ $27.7$ $5.7$ $345.7$ $13.8$ $6.4$ FL98297B $270.0$ $90.0$ $-9.6$ $270.0$ $90.0$ $-9.2$ $270.0$ $90.0$ $-8.8$ FL98297B $271.0$ $74.1$ $-9.8$ $70.1$ $3.1$ <t< td=""><td>FL98301D</td><td>255.6</td><td>53.4</td><td>-31.7</td><td>95.0</td><td>35.1</td><td>-31.6</td><td>358.4</td><td>9.4</td><td>-30.5</td></t<>	FL98301D	255.6	53.4	-31.7	95.0	35.1	-31.6	358.4	9.4	-30.5
FL98290A       74.5       76.9       19.3       269.3       12.6       20.2       178.6       3.2       21.3         FL98290B       341.6       81.6       19.3       161.6       8.4       20.2       151.4       46.1       20.3         FL98290C       221.2       3.3       20.2       131.0       2.7       21.1       2.2       85.8       23.1         FL98300A       39.7       74.5       37.8       237.1       14.8       39.0       145.9       4.4       39.4         FL98300B       270.5       73.4       37.7       74.7       16.0       38.7       166.0       4.3       39.1         FL2 (II)	FL98254C	309.6	38.2	-13.9	171.2	43.6	-13.4	58.4	22.2	-13.0
FL98290B       341.6       81.6       19.3       161.6       8.4       20.2       151.4       46.1       20.3         FL98290C       221.2       3.3       20.2       131.0       2.7       21.1       2.2       85.8       23.1         FL98300A       39.7       74.5       37.8       237.1       14.8       39.0       145.9       4.4       39.4         FL98300B       270.5       73.4       37.7       74.7       16.0       38.7       166.0       4.3       39.1         FL2 (II)       FL2 (II)       FL       FL       FL       FL98319B       102.2       73.5       5.7       249.1       13.9       6.6       341.3       8.6       7.1         FL98296A       263.7       71.6       -3.5       166.6       2.4       -2.9       75.8       18.3       -2.6         FL98299B       232.1       58.5       5.1       83.1       27.7       5.7       345.7       13.8       6.4         FL98299C       294.7       74.5       6.4       122.0       15.4       6.9       31.5       1.9       7.3         FL98297B       270.0       90.0       -9.6       270.0       90.0       -9.	FL98290A	74.5	76.9	19.3	269.3	12.6	20.2	178.6	3.2	21.3
FL98290C       221.2       3.3       20.2       131.0       2.7       21.1       2.2       85.8       23.1         FL98300A       39.7       74.5       37.8       237.1       14.8       39.0       145.9       4.4       39.4         FL98300B       270.5       73.4       37.7       74.7       16.0       38.7       166.0       4.3       39.1         FL2 (II)       FL	FL98290B	341.6	81.6	19.3	161.6	8.4	20.2	151.4	46.1	20.3
FL98300A       39.7       74.5       37.8       237.1       14.8       39.0       145.9       4.4       39.4         FL98300B       270.5       73.4       37.7       74.7       16.0       38.7       166.0       4.3       39.1         FL2 (II)       FL98319B       102.2       73.5       5.7       249.1       13.9       6.6       341.3       8.6       7.1         FL98296A       263.7       71.6       -3.5       166.6       2.4       -2.9       75.8       18.3       -2.6         FL98296C       185.9       80.7       2.5       73.6       3.6       3.2       343.1       8.6       3.5         FL98299B       232.1       58.5       5.1       83.1       27.7       5.7       345.7       13.8       6.4         FL98299B       232.1       58.5       5.1       83.1       27.7       5.7       345.7       13.8       6.4         FL98297B       270.0       90.0       -9.6       270.0       90.0       -9.2       270.0       90.0       -8.8         FL98297B       171.0       74.1       -9.8       70.1       3.1       -9.6       339.2       15.5       -8.8	FL98290C	221.2	3.3	20.2	131.0	2.7	21.1	2.2	85.8	23.1
FL98300B       270.5       73.4       37.7       74.7       16.0       38.7       166.0       4.3       39.1         FL2 (II)       FL98319B       102.2       73.5       5.7       249.1       13.9       6.6       341.3       8.6       7.1         FL98296A       263.7       71.6       -3.5       166.6       2.4       -2.9       75.8       18.3       -2.6         FL98296C       185.9       80.7       2.5       73.6       3.6       3.2       343.1       8.6       3.5         FL98299B       232.1       58.5       5.1       83.1       27.7       5.7       345.7       13.8       6.4         FL98299C       294.7       74.5       6.4       122.0       15.4       6.9       31.5       1.9       7.3         FL98297B       270.0       90.0       -9.6       270.0       90.0       -9.2       270.0       90.0       -8.8         FL98297B       171.0       74.1       -9.8       70.1       3.1       -9.6       339.2       15.5       -8.8         FL98298A       78.6       51.3       -10.4       217.3       31.0       -10.1       320.4       20.7       -9.5	FL98300A	39.7	74.5	37.8	237.1	14.8	39.0	145.9	4.4	39.4
FL2 (II)         FL98319B       102.2       73.5       5.7       249.1       13.9       6.6       341.3       8.6       7.1         FL98296A       263.7       71.6       -3.5       166.6       2.4       -2.9       75.8       18.3       -2.6         FL98296C       185.9       80.7       2.5       73.6       3.6       3.2       343.1       8.6       3.5         FL98299B       232.1       58.5       5.1       83.1       27.7       5.7       345.7       13.8       6.4         FL98299C       294.7       74.5       6.4       122.0       15.4       6.9       31.5       1.9       7.3         FL98297B       270.0       90.0       -9.6       270.0       90.0       -9.8       70.1       3.1       -9.6       339.2       15.5       -8.8         FL98297B       171.0       74.1       -9.8       70.1       3.1       -9.6       339.2       15.5       -8.8         FL98297C       160.5       26.0       -5.8       335.8       64.0       -5.6       69.6       1.8       -4.8         FL98298A       78.6       51.3       -10.4       217.3       31.0       -10.	FL98300B	270.5	73.4	37.7	74.7	16.0	38.7	166.0	4.3	39.1
FL98319B       102.2       73.5       5.7       249.1       13.9       6.6       341.3       8.6       7.1         FL98296A       263.7       71.6       -3.5       166.6       2.4       -2.9       75.8       18.3       -2.6         FL98296C       185.9       80.7       2.5       73.6       3.6       3.2       343.1       8.6       3.5         FL98299B       232.1       58.5       5.1       83.1       27.7       5.7       345.7       13.8       6.4         FL98299C       294.7       74.5       6.4       122.0       15.4       6.9       31.5       1.9       7.3         FL98297B       270.0       90.0       -9.6       270.0       90.0       -9.2       270.0       90.0       -8.8         FL98297B       171.0       74.1       -9.8       70.1       3.1       -9.6       339.2       15.5       -8.8         FL98297C       160.5       26.0       -5.8       335.8       64.0       -5.6       69.6       1.8       -4.8         FL98298C       40.4       62.8       -11.6       270.0       18.4       -11.0       173.3       19.3       -10.9         FL98	FL2 (II)									
FL98296A263.771.6-3.5166.62.4-2.975.818.3-2.6FL98296C185.980.72.573.63.63.2343.18.63.5FL98299B232.158.55.183.127.75.7345.713.86.4FL98299C294.774.56.4122.015.46.931.51.97.3FL98297B270.090.0-9.6270.090.0-9.2270.090.0-8.8FL98297B171.074.1-9.870.13.1-9.6339.215.5-8.8FL98297C160.526.0-5.8335.864.0-5.669.61.8-4.8FL98298A78.651.3-10.4217.331.0-10.1320.420.7-9.5FL98298C40.462.8-11.6270.018.4-11.0173.319.3-10.9FL98318A315.766.53.0124.423.14.1216.24.14.8FL98318B90.090.0-4.890.090.0-4.7270.090.0-3.9FL98318B174.03.9-6.183.48.3-4.5288.980.83.6	FL98319B	102.2	73.5	5.7	249.1	13.9	6.6	341.3	8.6	7.1
FL98296C185.980.72.573.63.63.2343.18.63.5FL98299B232.158.55.183.127.75.7345.713.86.4FL98299C294.774.56.4122.015.46.931.51.97.3FL98297B270.090.0-9.6270.090.0-9.2270.090.0-8.8FL98297B171.074.1-9.870.13.1-9.6339.215.5-8.8FL98297C160.526.0-5.8335.864.0-5.669.61.8-4.8FL98298A78.651.3-10.4217.331.0-10.1320.420.7-9.5FL98298C40.462.8-11.6270.018.4-11.0173.319.3-10.9FL98318A315.766.53.0124.423.14.1216.24.14.8FL98318B90.090.0-4.890.090.0-4.7270.090.0-3.9FL98318B174.03.9-6.183.48.3-4.5288.980.83.6	FL98296A	263.7	71.6	-3.5	166.6	2.4	-2.9	75.8	18.3	-2.6
FL98299B232.158.55.183.127.75.7345.713.86.4FL98299C294.774.56.4122.015.46.931.51.97.3FL98297B270.090.0-9.6270.090.0-9.2270.090.0-8.8FL98297B171.074.1-9.870.13.1-9.6339.215.5-8.8FL98297C160.526.0-5.8335.864.0-5.669.61.8-4.8FL98298A78.651.3-10.4217.331.0-10.1320.420.7-9.5FL98298C40.462.8-11.6270.018.4-11.0173.319.3-10.9FL98318A315.766.53.0124.423.14.1216.24.14.8FL98318B90.090.0-4.890.090.0-4.7270.090.0-3.9FL98318B174.03.9-6.183.48.3-4.5288.980.83.6	FL98296C	185.9	80.7	2.5	73.6	3.6	3.2	343.1	8.6	3.5
FL98299C294.774.56.4122.015.46.931.51.97.3FL98297B270.090.0-9.6270.090.0-9.2270.090.0-8.8FL98297B171.074.1-9.870.13.1-9.6339.215.5-8.8FL98297C160.526.0-5.8335.864.0-5.669.61.8-4.8FL98298A78.651.3-10.4217.331.0-10.1320.420.7-9.5FL98298C40.462.8-11.6270.018.4-11.0173.319.3-10.9FL98318A315.766.53.0124.423.14.1216.24.14.8FL98318B90.090.0-4.890.090.0-4.7270.090.0-3.9FL98318B174.03.9-6.183.48.3-4.5288.980.83.6	FL98299B	232.1	58.5	5.1	83.1	27.7	5.7	345.7	13.8	6.4
FL98297B270.090.0-9.6270.090.0-9.2270.090.0-8.8FL98297B171.074.1-9.870.13.1-9.6339.215.5-8.8FL98297C160.526.0-5.8335.864.0-5.669.61.8-4.8FL98298A78.651.3-10.4217.331.0-10.1320.420.7-9.5FL98298C40.462.8-11.6270.018.4-11.0173.319.3-10.9FL98318A315.766.53.0124.423.14.1216.24.14.8FL98318B90.090.0-4.890.090.0-4.7270.090.0-3.9FL98318B174.03.9-6.183.48.3-4.5288.980.83.6	FL98299C	294.7	74.5	6.4	122.0	15.4	6.9	31.5	1.9	7.3
FL98297B       171.0       74.1       -9.8       70.1       3.1       -9.6       339.2       15.5       -8.8         FL98297C       160.5       26.0       -5.8       335.8       64.0       -5.6       69.6       1.8       -4.8         FL98298A       78.6       51.3       -10.4       217.3       31.0       -10.1       320.4       20.7       -9.5         FL98298C       40.4       62.8       -11.6       270.0       18.4       -11.0       173.3       19.3       -10.9         FL98318A       315.7       66.5       3.0       124.4       23.1       4.1       216.2       4.1       4.8         FL98318B       90.0       90.0       -4.8       90.0       90.0       -4.7       270.0       90.0       -3.9         FL98318B       174.0       3.9       -6.1       83.4       8.3       -4.5       288.9       80.8       3.6	FL98297B	270.0	90.0	-9.6	270.0	90.0	-9.2	270.0	90.0	-8.8
FL98297C       160.5       26.0       -5.8       335.8       64.0       -5.6       69.6       1.8       -4.8         FL98298A       78.6       51.3       -10.4       217.3       31.0       -10.1       320.4       20.7       -9.5         FL98298C       40.4       62.8       -11.6       270.0       18.4       -11.0       173.3       19.3       -10.9         FL98318A       315.7       66.5       3.0       124.4       23.1       4.1       216.2       4.1       4.8         FL98318B       90.0       90.0       -4.8       90.0       90.0       -4.7       270.0       90.0       -3.9         FL98318B       174.0       3.9       -6.1       83.4       8.3       -4.5       288.9       80.8       3.6	FL98297B	171.0	74.1	-9.8	70.1	3.1	-9.6	339.2	15.5	-8.8
FL98298A       78.6       51.3       -10.4       217.3       31.0       -10.1       320.4       20.7       -9.5         FL98298C       40.4       62.8       -11.6       270.0       18.4       -11.0       173.3       19.3       -10.9         FL98318A       315.7       66.5       3.0       124.4       23.1       4.1       216.2       4.1       4.8         FL98318B       90.0       90.0       -4.8       90.0       90.0       -4.7       270.0       90.0       -3.9         FL98318B       174.0       3.9       -6.1       83.4       8.3       -4.5       288.9       80.8       3.6	FL98297C	160.5	26.0	-5.8	335.8	64.0	-5.6	69.6	1.8	-4.8
FL98298C       40.4       62.8       -11.6       270.0       18.4       -11.0       173.3       19.3       -10.9         FL98318A       315.7       66.5       3.0       124.4       23.1       4.1       216.2       4.1       4.8         FL98318B       90.0       90.0       -4.8       90.0       90.0       -4.7       270.0       90.0       -3.9         FL98318B       174.0       3.9       -6.1       83.4       8.3       -4.5       288.9       80.8       3.6	FL98298A	78.6	51.3	-10.4	217.3	31.0	-10.1	320.4	20.7	-9.5
FL98318A       315.7       66.5       3.0       124.4       23.1       4.1       216.2       4.1       4.8         FL98318B       90.0       90.0       -4.8       90.0       90.0       -4.7       270.0       90.0       -3.9         FL98318B       174.0       3.9       -6.1       83.4       8.3       -4.5       288.9       80.8       3.6	FL98298C	40.4	62.8	-11.6	270.0	18.4	-11.0	173.3	19.3	-10.9
FL98318B       90.0       90.0       -4.8       90.0       90.0       -4.7       270.0       90.0       -3.9         FL98318B       174.0       3.9       -6.1       83.4       8.3       -4.5       288.9       80.8       3.6	FL98318A	315.7	66.5	3.0	124.4	23.1	4.1	216.2	4.1	4.8
FL98318B 174 0 3.0 _6.1 83.4 8.3 _4.5 288.0 80.8 3.6	FL98318B	90.0	90.0	-4.8	90.0	90.0	-4.7	270.0	90.0	-3.9
	FL98318B	174.0	3.9	-6.1	83.4	8.3	-4.5	288.9	80.8	-3.6

Appendix 5	- Regional	Magnetic	Fabric	Data

		Minimum			Intermediate		Maximum		
Sample	Declination	Inclination	Intensity	Dec.	Inc.	Intensity	Dec.	Inc.	Intensity
CY9725A	97.0	31.1	-20.4	305.1	55.6	-19.9	195.1	13.2	-19.5
CY9725B	95.6	38.1	-21.1	247.6	48.4	-20.4	354.2	14.2	-19.9
CY9725C	93.4	17.8	-22.5	310.6	68.1	-22.0	187.5	12.4	-21.6
CY9725D	133.3	5.1	-22.0	233.4	62.9	-21.7	40.8	26.6	-21.0
CY9725E	82.8	62.3	-22.7	272.3	27.4	-22.5	180.3	3.9	-21.6
CY9726A	90.0	23.2	-12.0	197.9	35.7	-11.6	334.4	45.2	-11.1
CY9726B	94.5	29.5	-11.4	250.9	58.3	-11.1	358.4	10.5	-10.3
CY9726B	180.0	79.4	-11.3	180.0	74.5	-11.0	360.0	15.5	-10.4
CY9726C	284.2	44.1	-13.3	90.0	45.0	-13.2	187.2	7.1	-12.7
CY9726D	90.0	45.0	-13.6	278.6	44.7	-13.2	184.3	4.3	-12.2
CY9726E	255.0	32.7	-6.9	126.5	44.1	-6.2	5.2	28.2	-5.1
CY9726F	92.8	19.2	-14.2	234.6	66.1	-13.7	358.0	13.7	-13.1
CY9727A1	260.3	41.6	11.5	67.3	47.6	11.8	164.5	6.5	12.4
CY9727A2	296.7	41.8	12.2	90.0	45.0	12.6	194 1	13.7	13.4
CY9727A2	270.0	90.0	10.7	90.0	90.0	12.7	90.0	90.0	14 7
CY9727A3	108.3	59.1	10.0	250.0	25.2	10.2	348 1	16.8	10.5
CY9727A4	96.0	99	13.9	188.4	13.3	15.2	330.2	73.3	15.6
CY9727A5	278.0	217	12.2	149 9	57.2	12.5	17.9	23.4	13.1
FI 98255A	38	79 7	8.3	247.2	47	94	156.5	92	96
FL 98255B	307.0	39.1	14 5	152.3	48.8	14 9	47 5	11 1	15.8
FI 98317B	159.9	77.3	11.0	22.9	93	11 0	291.5	85	12.3
FL98317C	81 7	62.9	99	319 5	15.0	11 Q	201.0	21 0	12.0
FL 98317D	307.6	77.0	9.5 9.7	117.0	12.2	10.2	207.5	21.0	10.5
FL 98256A	71.2	73.5	21.8	267.0	15.9	23.0	175.8	2.3 4 3	23.6
FL 98256B	184.0	99	17.1	86 3	37 4	20.0	286.3	50 Q	34.2
FL 98256B	107.0	5.2	22.0	00.0	63 /	24.0	285.2	26.0	26.7
FL98256C	351 5	<u>л</u> Л5 Л	20.6	168.6	11 5	27.2	260.0	20.0	20.7
FL 98256C	60 5	10	20.0	328.7	60.5	22.2	151 0	20.5	27.2
FL98305B	219.3	58.6	34.6	0 7	26.1	25.5	100.9	16.2	22.0
FL 98305C	350.5	82.1	30.1	18/ 1	77	30.0	03.0	10.2	<i>A</i> 0.5
FL 98257C	162.6	02.1	22	71 3	546	24	90.9 253 3	35 /	17
EL 08306A	266.3	65 1	10.2	100.7	24.0	-2. <del>4</del> 0.4	200.0	55.4	-1.7 Q.Q
EL 08206P	127.2	40.2	9.5	20.1	24.2	-3.4	270.2	120	-0.0
FL90300D	137.3 90.4	40.5	-0.0	29.1 100 0	20.2	-0.1	219.2	42.0	-1.4
FL90300C	00.4 252.2	10.5	-10.7	190.0	16	-9.7	345.1	20.0	-9.0 10 E
FL90209D	302.3	60.0	-21.0	100.2	1.0	-19.7	190.5	3.0 14.0	-10.0
FL90103D	39.Z	09.9	404.7	200.0	14.1	200 4	1/2.4	14.0	410.2
FL90103C	00.0	74.0	242.7	339.7	4.0	350.4	240.0	15.5	393.0
FL90103D	09.4	00.2	343.7	302.2	4.1	303.0	212.0	2.0	304.0
FL96307B	240.1	33.4	-10.4	27.5	49.0	-9.7	143.5	20.9	-9.2
FL98307C	88.1	63.5	-11.7	255.2	25.9	-11.1	347.7	5.1	-10.6
FL98181B	114.0	63.4	4.1	19.1	2.4	5.4	287.9	26.5	6.1
FL98182A	141.6	41.5	8.2	290.9	44.2	9.3	36.9	15.9	9.9
FL98184A	258.3	29.1	7.3	164.2	1.5	1.1	61.2	59.7	8.3
FL98184B	258.5	41.3	-5.2	113.9	42.9	-5.1	5.7	18.6	-4.1
FL98184C	277.3	52.5	81.8	168.2	14.1	83.9	68.4	33.9	86.2
FL98315B	295.1	69.4	4.6	198.8	2.4	6.4	107.9	20.5	6.8
FL98185B	49.8	60.8	67.4	256.6	26.5	68.8	160.9	11.4	69.4
FL98185C	8.8	84.1	63.5	171.8	5.7	65.3	262.0	1.7	65.6

• · · · ·	Maximum	
Sample Declination Inclination Intensity Dec. Inc. Intensity Dec. Inc. Ir	ntensity	
FL98316A 252.9 55.8 3.8 97.1 31.7 5.0 0.0 11.3 5	.1	
FL98316B 219.2 39.6 2.4 319.0 11.6 3.4 62.3 48.0 3	.7	
FL98309B 36.0 64.4 -12.7 250.6 21.5 -11.9 155.3 13.2 -	11.4	
FL98310A 308.0 73.7 19.5 89.7 12.9 19.9 181.9 9.7 2	1.8	
FL98310B 220.8 67.9 11.3 128.2 1.1 11.7 37.8 22.1 1	2.7	
FL98311B 130.5 56.9 4.4 296.9 32.3 5.1 30.8 6.2 5	.9	
FL98312A 316.1 81.2 83.6 121.1 8.5 84.6 211.5 2.2 8	5.9	
FL98312B 16.8 82.2 85.3 274.1 1.7 86.9 183.9 7.6 8	8.2	
FL98186A 152.6 6.5 48.5 57.4 38.9 49.1 250.6 50.3 5	2.1	
FL98186B 170.5 64.1 47.2 23.1 22.2 48.3 287.9 12.6 4	8.7	
FL98186C 29.4 71.1 46.5 282.2 5.8 48.2 190.3 17.9 5	0.6	
FL98308A 237.4 63.3 -14.7 108.4 17.5 -14.3 12.0 19.4 -	13.5	
FL98308B 291.8 6.3 -9.6 198.6 26.7 -9.5 34.0 62.5 -4	3.6	
FL98308C 65.1 26.8 -14.2 317.5 31.0 -13.7 187.6 46.8 -	13.3	
FL98308D 222.0 12.6 -9.1 315.0 13.3 -8.4 90.0 71.6 -4	3.1	
FL98288A 184.0 40.3 -6.4 279.0 5.8 -5.5 15.7 49.1 -	5.2	
FL98288B 266.4 10.8 -4.7 107.5 78.5 -4.5 357.2 4.0 -	4.0	
FL98288C 283.0 54.5 -6.4 93.7 35.2 -5.9 186.8 4.4 -	3.7	
FL98288D 29.2 26.0 -6.3 270.0 45.0 -5.5 138.2 33.7 -	5.0	
FL98288D 207.0 50.8 -5.7 312.5 12.3 -5.3 51.7 36.5 -	5.3	
CY9724A 42.2 80.3 16.9 287.3 4.1 18.0 196.7 8.7 1	8.6	
CY9724B 335.2 81.8 20.0 107.0 5.5 21.0 197.5 6.1 2	1.6	
CY9724B 270.0 86.4 19.7 90.0 3.6 20.9 90.0 86.1 2	2.0	
CY9724C 121.7 87.5 20.0 266.3 2.0 21.0 356.4 1.4 2	1.6	
CY9724D 299.5 80.1 15.3 115.2 9.9 16.6 205.3 0.7 1	7.1	
CY9724E 90.0 78.4 20.6 270.0 11.6 22.1 270.0 59.0 2	2.5	
CY9724E 188.2 85.2 20.4 291.2 1.1 22.1 21.3 4.7 2	2.7	
CY9724F 292.0 75.1 19.7 97.3 14.5 20.7 188.3 3.6 2	1.6	
CY9724G 180.0 87.7 21.6 180.0 79.4 23.1 0.0 2.3 2	3.5	
CY9724G 42.9 82.4 21.7 291.1 2.8 22.9 200.8 7.0 2	3.9	
FL98313B 128.7 46.3 -13.3 225.8 6.7 -12.9 322.1 42.9 -	12.5	
FL98170A 0.5 61.8 9.5 212.9 24.4 10.3 116.7 13.3 1	0.7	
FL98170D 234.0 38.4 13.7 73.5 49.9 14.2 331.8 9.7 1	4.8	
FL98287B 108.8 43.4 -10.2 270.0 45.0 -10.1 9.7 9.5 -	9.0	
CY9723A 88.5 18.3 7.5 246.2 70.3 8.1 356.2 7.0 8	.5	
CY9723B 92.2 10.1 11.5 308.2 77.6 13.0 183.4 7.1 1	4.0	
CY9723C 81.2 16.7 14.7 294.6 70.2 15.2 174.4 10.3 1	6.0	
CY9723D 322.9 61.9 11.5 94.6 19.6 11.6 191.8 19.4 1	2.6	
CY9723E 103.2 61.8 12.8 284.5 28.2 13.2 194.2 0.5 1	3.9	
CY9723F 246.8 75.0 8.4 66.8 15.0 9.5 25.2 62.2 1	0.2	
CY9723G 103.0 25.3 11.7 322.9 57.5 12.2 202.2 18.0 1	2.4	
CY9723G 90.0 90.0 12.1 270.0 90.0 12.1 270.0 90.0 1	3.1	
CY9723H 73.8 23.6 12.7 224.1 63.5 13.6 338.1 13.4 1	4.2	
CY9723I 12.3 78.2 8.0 113.3 2.3 8.2 203.8 11.6 8	6	
FL98187A 130.8 0.2 12.3 40.7 9.5 13.0 222.1 80.5 1	3.3	
FL98187B 333.8 53.6 8.0 65.5 1.3 13.0 156.5 36.4 1	5.0	
FL98187C 203.5 32.0 10.9 84.5 37.8 11.8 320.4 35.8 1	3.8	
FL98169B 248.2 86.8 17.4 92.3 2.9 18.1 2.2 1.3 1	9.1	

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		Minimum			Intermediate		Maximum		
Sample	Declination	Inclination	Intensity	Dec.	Inc.	Intensity	Dec.	Inc.	Intensity
FL98169C	142.9	68.4	19.1	277.0	15.4	20.1	11.1	14.8	21.4
FL98167B	322.7	55.8	22.1	92.2	23.4	23.7	193.1	23.4	25.6
FL98167C	204.7	74.2	22.9	62.7	12.6	24.3	330.6	9.4	24.8
FL98168A	39.8	77.0	24.5	192.0	11.6	26.2	283.2	5.9	27.2
FL98168B	30.3	68.3	27.1	174.6	17.9	29.3	268.5	11.9	29.8
FL98168C	329.4	76.3	25.7	215.6	5.6	27.1	124.4	12.4	27.9
FL98188A	112.8	4.1	16.4	21.0	23.9	18.3	212.0	65.8	19.2
FL98188B	295.2	69.1	11.3	159.6	15.2	13.1	65.7	13.9	14.1
FL98179B	96.3	23.8	-13.6	290.3	65.5	-13.4	188.7	5.3	-12.5
FL98180A	195.0	31.4	-12.8	61.5	48.4	-12.5	300.9	24.3	-11.5
FL98180B	256.8	57.3	-14.7	156.9	6.3	-14.0	63.0	31.9	-13.6
FL98166A	3.3	74.8	37.3	243.6	7.6	39.3	151.8	13.0	39.9
FL98166B	23.3	40.4	38.4	143.4	30.5	39.8	257.4	34.6	40.8
FL98166C	180.0	83.5	32.7	180.0	63.4	33.7	0.0	6.5	34.0
FL98166C	184.1	88.0	32.0	54.5	1.3	34.0	324.4	1.5	34.3
FL98285B	31.9	32.8	-8.0	261.8	45.0	-7.5	141.0	27.0	-6.1
FL98285C	50.6	82.0	-5.1	273.1	5.9	-4.8	182.6	5.4	-3.9
FL98286A	321.1	66.8	-11.6	61.7	4.5	-10.7	153.6	22.7	-10.1
FL98286B	134.0	78.7	-7.2	262.1	7.0	-5.4	353.2	8.8	-4.7
FL98286C	77.5	68.7	-7.1	277.3	20.1	-6.4	184.8	6.6	-6.2
FL98190A	194.3	32.9	13.9	70.1	41.0	14.5	307.7	31.6	15.4
FL98190B	149.8	72.0	6.6	311.5	17.1	7.4	43.1	5.3	7.9
FL98282C	188.5	85.5	10.8	21.2	4.4	11.8	291.1	1.0	12.4
FL98283B	97.7	71.5	-4.6	268.5	18.3	-3.8	359.4	2.8	-2.9
FL98283D	226.0	64.6	-3.9	70.9	23.3	-3.0	336.8	9.5	-2.3
FL98284A	167.3	68.5	-6.2	52.1	9.5	-5.7	318.8	19.1	-5.2
FL98284B	141.0	75.0	-4.8	256.4	6.6	-4.5	347.9	13.4	-3.7
FL98370A	143.0	42.4	13.6	253.3	20.8	14.4	2.2	40.4	15.1
FL98370B	176.9	23.9	18.2	22.3	63.8	19.5	271.4	10.0	20.5
FL98191B	199.3	63.2	32.9	340.7	21.5	34.3	76.9	15.1	36.9
FL98369B	3.3	36.4	-14.4	121.3	32.4	-14.0	239.7	36.9	-13.7
FL98369C	150.7	81.0	-15.7	306.1	8.2	-15.0	36.6	3.7	-14.6
FL98192A	113.4	35.0	-3.6	250.0	46.0	-2.7	6.1	23.0	-1.3
FL98162A	270.0	78.9	-10.2	90.0	0.0	-9.1	90.0	11.1	-9.0
FL98162A	227.3	50.5	-9.7	16.0	35.2	-9.5	117.4	15.7	-9.3
FL98281C	259.1	61.2	22.8	80.7	28.8	23.7	350.3	0.7	24.0
FL98193B	277.3	7.9	5.8	165.0	69.8	6.1	9.9	18.5	6.9
FL98371B	354.8	68.0	46.8	198.3	20.3	47.5	105.3	8.0	48.5
FL98371C	2.4	49.4	48.8	233.8	28.1	49.8	128.2	26.7	50.3
FL98372A	153.4	29.6	11.8	153.4	0.0	12.0	333.4	60.4	12.6
FL98372B	38.3	72.3	14.6	216.5	17.7	14.8	306.7	0.5	15.4
FL98372C	292.8	69.4	14.0	175.9	9.8	14.4	82.7	18.5	15.5
FL98259C	307.1	81.9	3.5	98.5	7.1	5.3	189.0	3.8	5.9
FL98260B	114.2	71.9	-3.9	227.9	7.5	-34	320.1	16.4	-3.0
FL98261B	249.7	72.0	-2.6	68.2	18.0	-2.2	158.3	0.4	-1.7
FL98280C	18.0	55.1	21.9	232.2	29.9	23.7	132.6	16.2	24.1
FL98194A	47.3	35.1	12	199 7	51.6	5.9	307.5	13.6	69
FL98194A	179.0	65.9	4.5	21.7	22.4	5.1	288.2	8.4	5.6

		Minimum			Intermediate		Maximum		
Sample	Declination	Inclination	Intensity	Dec.	Inc.	Intensity	Dec.	Inc.	Intensity
FL98279B	348.3	75.8	2.4	79.5	0.3	3.0	169.5	14.2	3.2
FL98160A	90.0	90.0	25.0	270.0	90.0	26.0	270.0	90.0	26.5
FL98160A	94.2	76.4	25.0	245.4	11.9	26.0	336.7	6.4	26.9
FL98160B	230.8	78.9	24.7	90.2	8.6	25.9	359.1	6.9	26.8
FL98161B	237.9	32.4	25.4	5.1	43.6	27.2	127.2	29.2	28.4
FL98195B	109.4	20.8	14.6	233.3	55.7	14.9	8.8	25.9	15.4
FL98195C	266.4	74.9	13.0	121.5	12.5	13.4	29.6	8.4	14.0
FL98196B	208.9	68.9	6.4	306.5	2.9	7.4	37.6	20.9	7.7
FL98196C	335.9	83.7	4.9	101.3	21.4	6.9	167.9	82.5	8.9
FL98225B	145.7	81.7	54.3	299.7	7.5	55.8	30.2	3.6	56.0
FL98275C	286.5	61.6	<b>-2</b> .7	74.5	24.6	-2.3	170.7	13.2	-2.2
FL98198A	57.5	80.6	23.3	165.3	2.9	24.0	255.8	8.9	24.4
FL98198B	82.2	51.0	18.4	330.2	16.9	26.6	228.4	33.9	35.4
FL98272B	118.9	20.0	16.7	3.9	49.2	17.2	223.0	33.8	18.0
FL98158A	93.6	84.6	37.7	280.4	5.4	38.5	190.4	0.7	38.9
FL98158B	132.7	84.4	38.4	297.2	5.4	39.5	27.3	1.5	39.6
FL98159B	91.6	87.4	34.2	288.8	2.4	39.1	198.8	0.9	39.6
FL98273B	90.0	90.0	-17.9	90.0	90.0	-17.7	270.0	90.0	-17.1
FL98273B	121.2	29.7	-17.8	270.0	56.3	-17.7	22.8	14.5	-17.1
FI 98273B	74 1	39.4	-17.8	289.4	44.8	-17.3	180.0	18.4	-17.0
FL 98273C	265.5	55.8	-15.8	110.7	31.6	-15.5	13.3	11.8	-14.8
FL 98273D	271.0	51.4	-17 7	78.1	37.9	-17.2	173.0	6.3	-16.6
FI 98199B	344 7	18.8	22.8	93.4	43.3	26.0	237.6	40.7	28.1
FL98199C	145.2	10.0	27.1	288.3	77.5	27.5	53.9	7.3	28.7
FI 98223B	53.2	82.9	28.6	257.8	64	29.4	167.5	29	29.7
FL 98223C	311.1	84.9	36.6	51 1	0.4	37.3	141 1	5.1	37.8
FI 982228	292.3	77 4	40.2	199.5	0.0	41.8	109.3	12.5	42.1
FL 98222C	202.0	76.0	40.2	49 7	13.2	42.2	140.7	4.6	42.1
FI 3 (III)	240.0	10.0	40.7	-U.1	10.2	76.6	140.7	4.0	76,7
FI 982204	133 3	84.0	35 3	265.6	40	36.2	355 9	A A	37 4
FL 98220R	285.2	74 9	40.3	57 5	10.3	41 2	149 5	10 0	416
FL 982200	58 9	86.1	30.0	166.4	10.0	41.2	256 5	37	41.0
FI 98213B	60.2	65.8	-8.6	200.4	12 0	_7 Q	200.0	20.1	-73
FL 9821/A	158.3	66.6	-0.0	200.0	16.0	-11.0	204.7	15 7	-10.6
FL 98214R	314.6	4.6	-12.0	232.0 51 Q	57.5	-10.0	27.7	32.1	-8.8
FI 98214C	235 /	63.2	-10.5	07.7	21.0	-10.0	356.6	1/ 7	-0.0
EL 082120	200.4 A1 0	50.4		2215	21.5	86	137.3	5 1	- <u>2</u> .0 8.0
FL 08212R	260.5	10.4	0.0 8 1	132.5	59.1 60.3	8.8	358.5	0.1 01 7	0.9
EL 09210B	200.5	19.4	0.1 59.6	270.9	60.5	0.0 50.2	190 /	21.7	9.1 50.0
FL90219D	62.2	70.4	7.0	270.0	16.7	J9.J 70	100.4	10.0	09.9
FL90217D	00.0	70.4	7.0	2/0.1	10.7	1.0	240.0	10.0	0.0
FL90217C	90.0	71.0	9.0 40 F	200.9	10.1	9.9	349.9	3.3	10.0
FL90210A	323.1	12.4	40.0	105.6	14.0	41.9	190.4	10.4	42.0
FL90210D	13.3	01.2	55.7	201.0	3.3	54.5	17 1.1	0.1	00.0
FL90218C	93.9	4/.0	38.7 E.C	203.4 202.0	42.1	59.0 50	109.1	4.0	00.9
FLY0210A	139.9	/0.0 51.0	-0.0 • 7	202.0 02.0	9.1 27 7	-D.Z	13.7	0.0	-4.1
LAQTURE	200.2	0.10	-1.4	93.Z	31.1	-0.0	100.1	0.3	-5.8 7.0
FL98216C	135.0	82.8	-1.8	135.0	/6./	-/.4	315.0	1.2	-7.0
FL98216C	90.2	57.0	-8.3	251.8	31.6	-1.4	347.0	8.4	-6.3
Appendix	5 -	- Reg	ional	Magn	etic	Fabric	Data		
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		Minimum			Interm	ediate		Maxim	um
Sample	Declination	Inclination	Intensity	Dec.	Inc.	Intensity	Dec.	Inc.	Intensity
FL98215B	244.7	35.7	14.0	117.4	40.1	14.1	358.8	29.6	14.8
FL98157B	108.4	43.5	23.4	347.9	28.2	23.5	237.1	33.4	24.0
FL98211B	11.9	57.9	11.8	275.8	3.8	12.4	183.5	31.8	13.1
FL98211C	126.2	52.4	11.7	287.8	36.1	12.7	24.4	8.9	12.8
FL98177B	259.6	67.1	4.4	51.8	20.5	5.7	145.5	9.8	6.0
FL98210A	306.2	83.5	48.5	73.3	3.9	50.0	163.6	5.2	50.6
FL98210B	30.9	77.7	44.3	259.4	8.2	45.9	168.1	9.1	46.5
FL98175B	272.3	40.1	-16.7	17.8	17.6	-15.5	126.1	44.7	-13.7
FL98175C	318.9	3.9	-16.6	54.4	54.5	-16.3	226.1	35.2	-14.1
FL98209B	28.2	72.2	14.3	271.6	8.2	15.1	179.3	15.7	15.6
FL98209C	49.4	19.2	14.3	161.8	47.6	14.8	304.7	36.1	16.8
FL98174A	162.1	86.9	14.3	32.2	2.0	14.6	302.1	2.3	15.5
FL98174B	275.5	49.7	12.7	56.5	33.4	13.3	160.3	19.9	14.1
CY9715A	23.4	74.6	23.4	273.3	5.4	24.1	181.9	14.4	24.7
CY9715B	112.5	54.0	21.8	284.3	35.7	22.2	17.1	3.9	22.7
CY9715C	270.0	45.0	25.1	40.0	32.7	25.4	149.2	27.1	26.4
CY9715D	287 7	41.5	24.4	100.3	48.3	24.7	194.4	3.7	25.1
CY9715E	104.0	28.2	22.5	224.5	43.5	22.9	353.3	33.5	24.0
FI 98176A	135.0	81.3	26.5	315.0	87	26.9	315.0	84.2	27.4
FI 98176A	16.9	64.8	26.4	225.5	22.5	26.6	130.9	10.9	27.8
FI 98176B	68.1	81.3	16.9	302.3	51	17.9	211.6	70	18 1
FL 98176C	42.2	62 7	33.1	182.6	217	33.5	279.0	15.7	34.3
FL 98176D	342.6	54 7	16.1	200.4	29.2	16.5	99.9	18.0	16.9
FI 98253B	233.3	79 3	<u>10.</u> 1	107.6	6.3	4.3	16.7	86	52
FI 98208A	292.5	63.7	11.5	38.1	76	11.8	131 7	25.0	12.2
FI 98208B	323 5	66 1	13.2	112 1	20.8	14.1	206.5	11 4	14.7
FL 98208C	248.2	76.4	14.4	88.5	12.7	15.3	357.5	4.5	15.8
FI 98154A	201.8	76.7	15.6	64.6	9.8	16.2	333.1	8.8	17.0
FI 98154R	232.2	77 1	28.6	31.3	12 1	29.8	122.3	44	30.1
FL 98154C	202.2	35.6	73	64.4	52.4	17.0	320.4	10.5	17.5
FL 98154C	264 9	63.4	1/2	135 3	17 7	15.1	38.9	19.2	15.8
FL 08154D	204.0	66.7	27.8	125.3	83	28.8	32.0	21.6	31.0
FL 981564	137.8	71 5	13.5	33.1	4.8	14.5	301.6	17.8	14 7
FL 98156R	328.8	70.0	15.6	186 5	15 3	16.5	001.0 03.4	11 1	16.7
FL 98156C	355 1	70.9 66.6	13.0	06 1	10.0	10.5	188.0	22.8	14.6
FL 08156D	301 1	67.9	15.8	50.4	77	16.5	143 3	20.6	16.7
CV9714A	2023	73.6	18.0	102.6	16.2	18.7	193 /	26.0	19.7
CV071/B	202.0 307 A	73.0	16.0	69.2	35	16.4	160.7	16.2	16.7
CV0714B	327. <del>4</del> 45.0	73.4 80.6	10.0	225.0	0.0 0.1	16.7	225.0	54.7	16.0
CV0714D	40.0	84.4	10.1	220.0	5.4 517	16.5	135.0	56	10.5
CV0714C	313.0 45.0	04.4 95 5	16.9	225.0	4.7	10.5	225.0	547	17.6
CY0714C	40.0	00.0	10.0	223.0	4.0	17.0	223.0	J4.1 2 E	17.0
CY0714D	112.7	00.Z	10.0	244.0	5.Z	21.0	256 1	3.0 5.0	17.4
C19/14D	69.1	30.1	20.5	207.0	09.4 7 E	21.1	300.1 259.7	5.Z	21.0
FL9020/0	94.4 205 C	02.0 56.0	9.1	200.0	1.0	1U.D	300./ 400.9	10.2	12.3
FL90250A	290.0	2.ØC	13.4	93.3 400 0	31.0 70	14.3	109.0 45.4	10.3	14.0
FL98250C	215.5	00.0 40.0	24.1	108.3	1.2	20.0 70.7	15.4	21.9	20.1
FL98206A	140.9	43.8	69.2	286.7	40.8	/0./	32.9	17.9	/1.3
FL98206B	161.2	71.0	60.2	276.5	8.4	61.0	9.1	16.9	62.2

Sample Declination Inclination Intensity Dec. Inc. Intensity Dec. Inc.	
	Intensity
FL98153B 163.5 82.8 2.7 49.4 3.0 3.6 319.0 6.6	3.6
FL98153C 272.6 6.0 5.4 22.7 73.1 5.8 180.9 15.7	7.1
FL98153D 306.9 71.0 2.8 75.6 12.2 3.3 168.7 14.4	3.9
FL98249C 6.2 84.1 110.2 147.4 4.6 115.3 237.7 3.7	115.6
CY9722A 307.8 61.7 3.0 103.5 26.1 3.4 198.5 10.1	3.9
CY9722B 270.0 90.0 5.3 90.0 90.0 5.5 90.0 90.0	6.1
CY9722B 225.0 75.3 5.4 45.0 14.7 5.6 45.0 76.7	5.8
CY9722B 45.0 71.2 4.9 225.0 18.8 5.7 225.0 40.3	5.9
CY9722B 235.8 79.0 5.2 66.5 10.8 5.5 336.1 2.0	5.8
CY9722C 95.8 25.3 4.7 341.6 40.8 5.7 208.0 38.6	6.0
CY9722D 149.6 77.4 4.9 250.0 2.3 5.4 340.5 12.3	57
FL98248A 72.5 78.6 20.4 221.8 9.8 21.6 312.8 5.7	22.1
FL98205B 80.7 73.5 43.4 271.7 16.2 44.2 180.8 3.0	44 9
FL98205C 225.1 10.2 50.7 125.8 41.8 52.3 325.9 46.4	52.8
FL98110A 46 4 30.8 -12.0 297.4 28.6 -11.1 173.7 45.5	-10.1
FL98110B 91 0 53 3 -12 0 231 5 29 9 -10 0 333 0 19 3	-96
FL98173B 2857 574 117 769 293 122 1744 131	12.6
FL98173C 2172 732 77 646 150 85 3326 74	87
FL98173D 200.9 44.0 8.8 80.1 27.9 8.9 329.9 33.1	94
CY9712A 90.0 45.0 -19.0 297.8 41.5 -18.7 194.8 14.3	_17 Q
CY9712B 83 1 30.3 -19.5 275 1 59.1 -18.9 176.2 5.3	-18.0
CY9712C 99.7 37.5 -19.2 267.7 51.9 -18.8 5.2 5.9	-18.0
CY9712D 36.7 84.5 -19.4 146.6 1.9 -19.1 236.8 5.1	-18.0
CY9713A 270.0 6.0 -8.1 90.0 81.5 -7.6 90.0 84.0	-7 4
CY9713A 93.9 9.5 -8.1 357.3 34.6 -7.5 197.1 53.8	-71
CY9713B 349.4 40.3 -8.7 134.3 43.9 -8.5 243.0 18.4	-8.2
CY9713C 84.9 10.1 -8.9 180.0 26.6 -8.0 335.8 61.2	-8.0
CY9713C 270.0 90.0 -8.6 90.0 90.0 -8.2 270.0 90.0	-79
CY9713C 270.0 90.0 -8.6 90.0 90.0 -8.3 270.0 90.0	-8.2
CY9713D 228.2 42.3 -9.7 84.0 41.7 -9.1 336.3 18.8	-8.5
CY9713E 279.9 39.9 -9.5 69.3 45.8 -8.8 176.2 15.8	-7.6
FL98246A 229 1 80 4 20 2 75 3 8 6 21 5 344 7 4 2	21.7
FL98246B 90.0 83.0 19.6 270.0 7.0 20.2 270.0 85.2	21.1
FL98246B 37.3 77.1 19.7 245.2 11.4 20.4 154.0 5.9	20.8
FL98245B 90.0 90.0 9.5 90.0 90.0 9.9 90.0 90.0	10.3
FL98245B 276 3 48 5 9 4 65 5 37 2 9 6 167 9 15 7	10.4
FL98152A 11.2 76.7 38.9 246.4 7.7 40.2 154.9 10.8	40.5
FL98152B 195.6 86.7 31.8 71.7 1.9 32.5 341.7 2.8	33.3
FL98244A 139.9 78.6 23.9 282.6 9.1 24.3 13.7 6.8	24.7
FL98244B 69.5 75.7 22.8 265.9 13.7 24.2 174.9 3.9	24.7
FL98244C 264.5 75.5 22.4 106.0 13.5 23.3 14.8 5.1	24.0
CY9709A 340.5 63.2 -12.3 100.0 14.0 -11.7 195.9 22.4	-11.5
CY9709B 263.8 13.5 -12.3 30.6 68.1 -11.8 169.6 16.9	-11.0
CY9709C 237.6 81.1 -12.9 80.9 8.2 -12.6 350.4 3.5	-12 4
CY9709D 319.6 62.4 -12.6 213.3 8.4 -11.9 119.1 26.1	-11 8
CY9709E 22.2 38.4 -12.1 218.9 50.4 -11.7 118.8 8.3	-11 4
CY9709F 239.7 49.0 -12.2 134.3 13.0 -11.8 33.9 38.0	-11.3
CY9710A 69.4 60.3 -9.3 286.6 24.4 -8.9 189.3 15.8	-8.4

		Minimum			Interm	ediate		Maxim	um
Sample	Declination	Inclination	Intensity	Dec.	Inc.	Intensity	Dec.	inc.	Intensity
CY9710B	352.7	78.1	-11.5	228.3	6.8	-11.1	137.1	9.7	-10.9
CY9710C	0.0	73.6	-10.2	0.0	60.6	-9.8	180.0	16.4	-9.4
CY9710C	275.2	14.1	-10.3	72.6	74.8	-10.0	183.8	5.6	-9.3
CY9710D	82.6	14.3	-10.4	296.8	72.8	-10.0	175.0	9.2	-9.6
FL98243B	78.7	77.3	57.4	273.3	12.3	60.1	182.6	3.1	61.5
FL98243C	148.1	59.7	52.4	24.8	17.8	54.7	286.7	23.7	56.1
FL98243D	220.1	74.4	38.8	56.6	15.0	40.6	325.4	4.2	41.5
CY9711A	125.7	30.3	-3.0	0.0	45.0	-2.5	235.2	29.7	-2.3
FL98204A	118.4	57.5	9.4	236.4	16.7	10.4	335.2	27.0	11.3
FL98204B	265.6	71.6	6.7	110.9	16.8	7.6	18.7	7.4	7.7
FL98204C	61.2	41.2	10.7	270.0	45.0	11.1	164.7	14.8	11.8
FL98204C	112.6	67.2	10.7	272.2	21.5	11.4	5.1	7.2	11.8
FL98204D	59.7	78.3	7.5	272.6	9.8	7.9	181.5	6.2	8.2
FL98151B	70.8	75.1	8.3	297.1	10.4	10.0	205.2	10.6	10.5
FL98151C	310.3	79.2	11.5	119.9	10.7	12.4	210.3	1.9	12.8
FL98105B	48.0	23.7	-15.4	241.2	65 7	-14 7	140.2	49	-13.9
FI 98172A	246.9	26.3	-23.6	52	43.9	-23.3	136.9	34.7	-5.5
FI 98104A	131.3	42	-9.3	41.0	4 1	-8.5	267.2	84 1	-78
FI 98104C	267.2	59.2	-8.3	118.0	27.1	-7.9	21.0	13.5	-78
FI 98104D	297.5	22.1	-9.3	139 1	66.4	-9.0	30.7	78	-8.0
FI 98109B	276.3	33.5	-14.5	124.3	53.1	-14 0	15.6	13.6	-13 7
FI 98103A	168.6	26.9	61	49.8	43.5	64	279.0	34.6	6.8
FI 98106A	80.7	72 7	-89	259.5	17.3	-8.0	349.6	0.3	-7 0
FI 98106B	144 8	54.1	-9.3	335.5	35.4	-8.3	241.9	5.0	-7.9
FI 98171B	95.6	<u>41</u> 0	-18.0	293.3	47 7	-17.8	193.4	89	-17 0
FL98171C	90.0	90.0	-20.4	270.0	90.0	-19.6	270.0	90.0	-19.2
FL98171C	268.9	29.0	-20.4	134.9	51.4	-19.9	12.6	23.1	-19.5
FI 981084	214.6	56.8	.24 9	116.2	54	25.8	22.7	32.6	26.6
FL98108B	343 7	85.4	404	242.2	0.4 N 9	42.8	152.2	46	43.4
FI 98203B	328.6	81.2	11 2	186.0	70	12.0	95.3	5.3	12.5
FL98203C	223.0	65.2	17.3	95 5	16.0	18.6	0.0	18.4	19.0
FI 981024	302.2	20.9	-19.7	188.6	46.3	-18.6	48.5	36.3	-17 4
FI 98102R	128 9	20.0	-18.9	14 7	33.3	-18.1	250.8	40.3	-17.8
FL98102C	269.4	69.4	-19.3	73.7	19.9	-18.5	165.6	51	-18.0
FI 982424	284 3	37.0	12.5	104 4	53.0	13.1	14.3	0.1	14 0
FI 98242R	275 0	13.2	12.0	139.1	71.9	13.5	7 9	12 1	14.0
FI 98241B	270.0	58 A	80	145 5	22.9	89	46.4	20.5	9.5
FI 98107B	175.3	76.7	-5.6	318 1	10.6	-5.2	49.6	79	-4.0
EL 08202A	235.3	60.5	-0.0 21 2	120.5	8.8	24.5	34.8	28.0	25.5
FL90202A	233.5	47.3	24.2	123.0	0.0 11 5	24.0	130 8	20.0	22.5
FL90202D	250.9	70.0	17.0	203 1	75	17.0	24.2	0. <del>4</del> 8.0	18 7
EL 082020	257.2	173	11.2	138.6	7.5 56 Q	-1/ 1	27.2	27.2	-137
EL 09240A	201.2	17.5	214.4 21 0	282.2	00.3 00.7	2/ Q	147.2	50 1	95.1
FL90240A	20.0	19.4	04.Z 196	202.2	795	0 <del>4</del> .0 49.9	192.1	51	50.1
FL90240B	31.2 250 A	10.1 53.0	40.0	102.0	21 2	-12 2	100.1 3.2	0.4 16 1	.12 A
EL 00000A	200.4 126.6	03.9	-10.7	100.9	J1.J 45 0	15.0	0.0 212 7	96.9	-12.4 12.0
FL90200A	100.0	0/.I	-17.2	121.0	40.0	-10.Z 17.4	513.7	00.0 E 0	-13.Z 16.0
FL90200B	209.3	50.9	-10.4	39.0 070 F	30.7	-17.4	0.0	5.U 4.0	-10.2
FL98200C	100.7	49.1	-16.1	272.5	40.6	-14.9	0.U	4.0	-14.4

Apr	pendix	5 -	Regional	Magnetic	Fabric Data

		Minimum			Interm	ediate		Maxim	um
Sample	Declination	Inclination	Intensity	Dec.	Inc.	Intensity	Dec.	Inc.	Intensity
CY9706C	298.1	81.7	-11.4	87.8	7.2	-5.4	178.3	4.2	-3.7
CY9706D	241.1	25.8	-8.2	360.0	45.0	-7.7	132.1	33.9	-7.3
CY9706E	270.0	90.0	-7.8	90.0	90.0	-7.7	90.0	90.0	-7.3
CY9706E	8.6	67.6	-8.2	118.2	7.9	-7.5	211.2	20.8	-7.3
CY9704A	306.3	15.3	-4.7	213.9	8.8	-2.3	95.1	72.3	-1.6
CY9704C	234.5	55.8	-2.7	110.8	20.7	-2.3	10.2	25.9	-2.0
CY9704C	315.0	84.4	-2.6	315.0	54.7	-2.1	135.0	5.6	-2.0
FL98232C	311.1	69.2	-8.4	110.3	19.5	-8.0	202.7	6.8	-7.4
FL98229B	225.0	87.4	-2.9	225.0	82.0	-2.1	45.0	2.6	-1.7
FL98148A	316.1	38.9	12.4	105.5	46.9	12.7	213.0	15.7	13.5
FL98148B	102.3	38.6	15.5	342.8	31.6	16.1	226.9	35.4	17.0
FL98148C	243.0	76.2	14.7	61.6	13.8	16.1	151.6	0.3	16.6
FL98148D	331.2	81.2	13.9	138.6	8.6	14.6	228.9	1.9	15.3
FL98228D	273.2	4.1	-28.1	12.4	65.6	-27.5	181.4	24.0	-27.2
FL98147B	184.7	66.9	17.8	289.8	6.3	18.4	22.4	22.2	18.6
FI 98147C	270.0	71.6	14.6	56.3	15.5	15.2	149.0	97	15.7
FL98147D	212 7	74 7	17.8	48.8	14.8	18.2	317.7	41	19.4
FI 98149B	303.7	84.6	22.1	42.1	0.8	27.2	132.2	54	29.5
FL 98149C	331.8	83.9	32.7	94.4	3.3	33.5	184 7	5.1	33.9
FI 98149D	335.1	68.8	28.3	187.8	18.1	29.7	94.3	10.7	30.1
FI 98146B	259.0	19.7	-4.0	17.6	53.3	-37	157 2	29.6	-2.5
FL 98226A	70.3	52 1	_11 Q	330.0	79	-11 8	234.0	25.0	-2.0
FI 98226R	178.2	64.0	-113	341 5	25.0	-10.5	746	66	-10.0
FL 98226C	154 1	35.3	_1/ 0	264.7	26.5	-14.0	22.5	13 1	-3.0
FI 981424	33.6	75.8	23.5	257 1	10.0	2/13	165 /	45.1	25.2
FL 98142A	33.6	75.8	23.5	257.1	10.4	24.0	165.4	9.0	25.2
FI 081/2R	00.0 03.2	74.7	20.0	208.9	6.8	27.0	300.5	3.0 13.7	20.2
CV07030	18 /	82.1	80.0	320.7	50 /	0 /	108 /	70	07
CV0703R	73.3	111	0.5 7 /	205.6	70.0	३. <del>५</del> ७.८	166 5	123	9.7 8.0
CY9703C	241 5	17.4	8.6	255.5	60.0	7.0 8.8	145.2	12.3	0.0
CV0703D	12 0	60.8	73	244.8	12.8	7.5	140.2	20.0	9.0
	270.0	77 0	60	244.0	12.0	7.0	00.0	10.4	0.0 9.0
CY0703D	270.0	00.0	72	270.0	41.0	7.0	90.0	12.1	0.0
	30.0	90.0 65.9	7.0	270.0	120	7.5	90.0 47 E	90.0	0.2
EL 08140R	200.4	55.2	7.0 5.4	142.1	34.2	0.1 5.7	204.0	20.7	6.0
FL90140D	16.9	90.0	2.4	265.0	24.2	0.7 2 A	204.0	0.0	0.1
FL90141D	10.0	72.0	-0.0	203.0	J.4 140	-2.4	174.5	0.0	-2.1
FL90141C	40.1	73.9	3.0	201.7	14.0	3.0 10.6	100.1	0.0	4.2
FL90130A	03.1	10.0	10.0	213.9	12.9		103.3	2.4	12.0
FL90130D	70.7	44.7	1.2	220.7	43.1	7.4	329.4	11.2	8.3
FL98138C	0.0	81.7	9.4	300.0	03.4	10.1	180.0	8.3	10.4
FL98138C	90.0	83.0	9.1	270.0	1.0	9.8	270.0	85.2	10.6
FL98138C	301.2	70.9	9.0	83.5	15.3	9.9	1/6.6	11.1	10.1
FL98139B	254.0	/5./	7.0	107.2	12.0	8.0	15.5	7.6	9.9
FL9813/A	180.0	69.4	9.3	180.0	65.8	9.4	360.0	24.2	10.0
FL9813/A	331.6	63.6	8.5	/0.4	4.3	9.2	162.5	26.0	9.6
FL98137B	82.5	/2.9	9.0	288.1	15.5	9.2	196.1	7.0	9.8
FL98136A	113.2	76.4	13.1	287.7	13.5	13.9	18.0	1.2	14.3
FL98136B	10.4	82.7	15.0	252.5	3.4	15.4	162.2	6.4	15.6

Appendix	5 - Regi	onal Mac	inetic F	abric	Data

		Minimum			Interm	ediate		Maxim	um
Sample	Declination	Inclination	Intensity	Dec.	Inc.	Intensity	Dec.	Inc.	Intensity
FL98088A	92.7	51.4	-16.8	275.9	38.5	-16.0	184.7	1.6	-13.8
FL98088B	66.5	40.8	-13.8	303.4	32.3	-13.4	189.8	32.4	-12.8
FL98089B	141.3	54.2	-11.8	355.9	30.7	-11.3	255.7	16.6	-11.0
FL98087B	39.9	63.8	-17.9	230.4	25.8	-16.9	138.4	4.2	-16.7
FL98090A	78.9	76.3	3.3	286.6	12.1	4.0	195.3	6.2	4.8
FL98090C	270.0	71.6	11.7	94.2	18.4	11.8	3.8	1.3	13.5
FL98090D	172.5	39.4	11.0	329.4	48.2	11.5	72.8	11.7	13.4
FL98091B	238.1	57.3	9.8	94.3	27.4	10.1	355.5	16.5	11.1
FL98091C	274.6	66.3	8.6	82.6	23.3	9.5	174.5	4.4	11.6
FL98093B	234.2	60.4	13.6	121.0	12.6	14.8	24.7	26.3	15.0
FL98093C	45.8	65.9	14.9	272.2	17.1	15.5	177.0	16.4	16.1
FL98093D	250.7	71.9	12.2	49.2	17.1	12.8	141.1	7.0	13.5
FL98128A	70.5	45.4	8.1	317.2	21.4	8.7	210.1	36.9	8.9
FL98128B	281.4	20.0	9.0	66.3	66.0	9.8	186.7	12.7	10.6
FL98094A	107.7	55.5	2.3	242.3	25.8	3.0	343.1	21.3	3.9
FL98094B	130.2	43.4	2.8	235.1	15.2	4.0	339.6	42.6	4.2
FL98094C	316.2	83.0	5.5	106.0	6.1	6.1	196.4	3.5	7.1
FL98095B	355.1	10.0	6.9	238.9	68.3	92	88.6	19.1	10.8
FI 98095C	174.2	71.5	10.4	267.8	12	11.2	358.3	18.4	12.8
FI 98095C	174.2	71.5	10.4	267.8	12	11.2	358.3	18.4	12.8
FI 98096A	107.4	22.5	9.5	326.5	62 0	97	204.2	15.9	10.6
FI 98096B	327.2	36.0	86	141.3	53.9	87	235.1	2.8	10.6
FI 98097B	115.9	57.3	19.2	321 7	30.0	197	224.8	11 7	21.4
FL98097C	102.8	61.6	21.9	248 7	24 1	22.5	345.1	14.1	22.6
FI 98097D	224.2	60.0	17.8	26.9	28.9	18.1	121.0	7.5	18.9
FL 98100A	315.0	86.4	47.0	315.0	54 7	47.8	135.0	3.6	47.9
FL 98100A	106.9	70.7	46.8	272 0	18 7	47.0 47.9	3.5	4.6	48.6
FI 98100B	254.0	29.3	34.9	102 1	57.6	35.3	351.3	12 7	35.8
FI 98098A	282.4	54.0	37.6	126.6	33.6	39.4	28.8	11.6	40.7
FL98098B	169.7	47 7	56.4	356.3	42 1	57 2	263.3	22	58.6
FI 98099B	135.1	10.3	28	22.6	64.5	34	229.6	23.1	<u>4</u> 9
CY9752A	54 4	76.3	2.0	286.0	87	25 1	194 4	10.6	25.6
CY9752B	92.6	66.4	24.1	276.6	23.2	25.2	186.0	15	25.9
CY9752C	87.0	14.0	26.9	338.5	51 7	28.3	187.0	34.8	28.6
CY9752D	216.8	61 5	20.0	77 1	22.5	20.0	340.1	16.6	20.0
CY9702A	200	33.1	Q /	151.2	22.0	9.7	273 7	33.7	10.2
CY9702R	Q1 3	57.0	5.4	252 4	31.6	61	347.8	86	63
CV9702C	313 5	52.0	6.0	84 4	27.1	64	187.0	24.5	6.8
EL 98054A	222 4	52.0	0.0 /3 3	321 1	56 7	11 C	107.9	297	45.7
FL08054R	222.4	571	45.5	07 1	20.7	44.Z 25.0	120.1	32.7	40.7
	222.1	57.1	20.1	97.1	20.5	20.9	307.3	24.1	20.7
CV0701A	82 4	47.0	60	216 1	20 0	64	208 5	20 7	60
CV0701A	02.4	47.0	6.0	270.0	20.9	0.4	208.5	20.7	0.9
CV0701P	30.0 202 A	30.0 71 5	0.0	210.0 16.7	50.0 1 A	0.0 7 0	30.0 107.0	30.U	7.5
CV0704C	202.4 212 A	7 1.0 90 E	U.J 6.0	10.7	1.4	1.Z 7.6	107.2	10.4	(.) 0 0
CV0704D	J12.4	00.0 16 7	0.9 10.0	120.0	9.4 10.2	1.0	210.0	0.0	0.U 11 E
	342.0	10.7	10.9	231.9 120 A	40.3	11.3	30.0	40.0	11.0
	344.0	12.0	9.0	129.4	14.2	9.9	221.0 470.5	9.5	10.2
LA99320A	308.5	39.0	-24.9	59.4	23.8	-24.5	1/2.5	41.6	-24.2

		Minimum			Interm	ediate		Maximum		
Sample	Declination	Inclination	Intensity	Dec.	Inc.	Intensity	Dec.	Inc.	Intensity	
FL98350B	245.3	71.3	-31.0	68.1	18.7	-30.4	337.8	0.9	-30.1	
FL98119B	280.7	67.2	16.6	39.7	11.5	17.6	133.7	19.4	18.7	
FL98119C	264.8	53.1	13.6	87.8	36.9	14.3	356.7	1.5	14.6	
FL98122A	90.4	41.3	-24.9	331.7	28.7	-23.9	218.8	35.3	-20.1	
CY9766A	102.1	22.9	7.4	335.8	54.5	7.8	203.8	25.5	8.3	
CY9766B	92.5	20.1	5.2	297.3	68.0	6.0	185.7	8.5	6.8	
CY9766C	101.2	46.5	3.4	260.9	41.7	3.8	0.2	10.2	4.7	
FL98113B	120.2	68.2	-8.5	313.8	21.2	<b>-</b> 7.7	222.0	4.7	-7.3	
FL98116A	177.0	36.5	6.9	50.3	38.9	9.4	292.4	30.1	10.0	
FI 98116B	232 5	59.8	6.2	19.9	26.1	6.8	116.9	14.1	7.6	
FI 98116C	93	79.9	3.4	188.1	10.1	6.1	278.2	0.2	6.5	
FI 98115B	66.8	57.6	43	225.8	30.6	4.8	321.5	9.5	5.3	
FL98115D	246.6	80.5	4.0	77.1	9.4	4.6	346.8	1.7	5.9	
FI 98121C	88.9	32.8	-18 4	257 5	56.7	-17.9	355 5	52	-17.1	
FL98121D	259.4	35.1	-18.0	78.3	55 7	-17.8	169 1	0.9	-16.3	
FI 980044	234 7	67.9	3.8	139.9	19	46	49 1	22.0	49	
FL98005B	<u>45</u> 1	67.3	45.2	179.0	16.2	46.2	273.6	15.5	46.8	
FI 981264	159.2	14	21.8	61.8	79.1	22.0	249.5	10.0	22.6	
FL 98126R	299.8	7.0	37.8	46.4	66.8	38.8	207.0	22.0	39.2	
FL 9811/4	1/3 5	84.8	14 5	-0 244 7	1 0	17.8	334.8	51	18 1	
FL08114R	288.5	78.8	16.0	43.6	4.8	16.6	134 4	10.1	17.6	
EL 980064	200.5	70.0	10.0 A 1	73 3	16.0	4.6	220 0	11.6	18	
EL 98006A	215.5	70.0	<del>4</del> .1	73.3	16.0	4.0	330 0	11.0	18	
FL98117B	210.0	55.3	56	132 4	0.0	<del>4</del> .0 6 1	222 Q	34.7	9.5	
EL08118A	275 2	0.0 0.1	10.2	120.4	80.0	19.6	58	12	20.7	
EL09119R	213.2	80.8	20.1	23.5	8.0	22.5	114.2	ч. <u>с</u> 15	20.7	
FL90110D	255.5	48.2	16.2	20.0	32.0	16.0	1/4.2	4.J 24.0	18.2	
FL90110C	203.7	40.2	10.2 25 A	265 7	115	27.2	162.6	13.0	27.6	
EL08016A	41.0	25.8	15 Q	185.3	59.2	16.2	303.2	15.0	17 /	
EL08016R	41.0	70 /	17.8	271 4	10.5	18.0	16	10.0	10.3	
FL98010D	83.0 83.7	15.4	10.5	271.4	26.4	10.0	213.0	32.1	19.0	
FL90013D	02.2 117 A	40.2	20.2	310 1	120.4	20.7	213.0	11 2	21 /	
FL90332A	106.6	40.7	20.2	0.4	12.6	20.7	210.0	35.7	21.4	
FL90302D	100.0	72.0	20.0	0.4 25.0	10.0	21.0	201.1	12.0	37.Z 33.5	
FL90352C	104.9	73.0	20.9	20.9	10.9	21. <del>3</del> 11.6	293.3	12.9	ZZ.0 42.0	
FL90352D	141.0	00.0 42.7	40.7	200.4	2.0	41.0	010.0	25.0	42.0	
CY0748A	31.4	43.7	3. I A E	120.1	3.9 35.3	J.J A 0	219.1	40.0	১.৩ ৮০	
CY9748E	27.3	30.3	4.0	201.3	30.3 6 E	4.0	147.3	30.3	D.Z	
CY9749A	19.7	76.4	95.7	137.0	0.0	102.4	229.2	11.9	103.9	
C19749B	38.9	71.2	88.7	295.0	4.7	93.1	203.5	18.2	94.2	
CY9749C	15.8	74.5	64.7	141.5	9.1	69.Z	233.5	12.3	70.0	
CY9749D	13.2	68.5	84.9	169.9	19.9	89.5	262.8	7.8	91.9	
CY9750A	117.4	58.1	62.5	8.2	11.6	66.3	2/1.6	29.3	67.1	
CY9750B	128.1	48.5	62.9	338.9	37.2	/1./	236.6	15.7	/3.4	
CY9750C	118.6	60.2	55.4	318.8	28.3	59.0	224.1	8.7	59.6	
CY9750D	106.6	65.0	76.9	303.2	24.1	82.0	210.4	6.3	82.3	
CY9750E	108.7	65.3	72.4	260.3	22.1	77.5	354.7	10.6	77.6	
FL98036A	332.6	12.1	9.7	75.8	46.7	10.1	232.0	40.7	10.6	
FL98027B	293.7	41.5	16.4	27.6	4.5	17.0	122.6	48.1	17.4	

		Minimum	nimum			ediate	Maximum		
Sample	<b>Declination</b>	Inclination	Intensity	Dec.	inc.	Intensity	Dec.	Inc.	Intensity
FL98027C	240.2	42.3	13.6	119.3	29.4	14.1	7.3	33.6	14.5
FL98027D	276.4	25.8	12.4	95.3	64.2	13.1	186.2	0.4	14.3
FL98353B	61.9	76.8	43.1	220.8	12.4	44.3	311.8	4.6	44.7
FL98031B	87.2	41.2	1.9	308.9	40.5	2.4	198.3	22.4	3.1
FL98354A	254.0	16.5	-17.9	12.3	57.9	-17.3	155.5	26.6	-16.6
FL98354B	275.8	57.5	-17.0	121.3	30.0	-15.8	24.5	11.5	-15.1
FL98355A	343.8	25.7	-29.2	94.5	36.3	-28.7	227.3	42.8	-27.7
FL98355B	70.9	16.9	-24.9	328.0	36.3	-24.2	181.2	48.7	-23.5
FL98355C	162.7	82.0	-27.8	11.0	7.0	-27.3	280.5	3.8	-26.5
FL98355D	112.6	24.6	-27.6	345.3	52.9	-27.3	215.4	25.9	-26.2
FL98001B	33.0	75.3	48.3	251.1	11.7	50.0	159.3	8.8	50.9
FL98373B	289.5	62.7	7.1	83.2	24.9	8.1	178.2	10.7	9.2
FL98373C	171.4	76.4	7.9	22.9	11.6	9.3	291.5	6.9	9.9
FL98374B	347.2	66.7	5.8	160.3	23.1	6.3	251.3	2.5	8.1
CY9751A	261.9	52.6	153.3	84.1	37.4	158.8	353.3	1.0	161.2
CY9751B	264.4	54.7	132.1	97.1	34.6	137.5	2.9	6.0	139.5
CY9751C	255.4	46.0	143.0	74.5	44.0	147.6	164.9	0.5	149.2
FL5 (V)									
FL98390A	223.0	84.8	39.7	318.1	0.5	41.2	48.1	5.2	42.1
FL98379B	286.6	78.3	11.5	73.6	9.8	12.2	164.7	6.2	13.6
FL98389B	322.9	36.1	12.8	70.6	22.6	17.1	185.4	45.3	17.5
FL98388B	276.9	41.4	-6.3	100.8	44.5	-59	88	21	-5.0
FL98061B	161.4	75.9	-9.5	14.3	11.9	-6.7	282 7	74	-6.3
FL98383B	83.7	74.7	4.5	252.8	2.6	53	343 5	62	5.9
FL98060B	306.0	60.0	13.8	136.0	29.6	14.6	43.5	43	15.3
FL98083B	230.8	86.2	14.0	103.9	2.3	15.4	13.8	3.0	15.7
FL98084A	55.7	79.6	32.9	283.3	7.1	33.9	192.3	76	34.3
FL98084B	305.6	80.4	43.4	43.4	1.3	45.3	133.6	9.6	45 7
FL98084C	7.3	80.3	33.2	105 5	1.4	34.6	195 7	9.6	34.8
FL98086A	252.3	80.9	14.5	73 7	91	16.0	343.7	0.2	16.8
FL98086B	235.0	76.0	19.8	32.2	12.9	20.5	123.4	5.2	20.8
FL98085B	212.2	84.9	20.0	327.9	22	20.7	58.1	4.6	21.3
FI 98082A	166 1	72 0	22.2	313.6	15.3	23.9	46.2	92	25.3
FI 98082B	129.4	66.4	25.2	258 7	15.5	26.3	353.7	17.4	26.9
FL98082C	303.7	81.6	20.2	123.7	0.0	22.0	123 7	84	22.0
FL98080A	334.1	74.1	-23.0	242.3	0.5	-22.6	152.2	15.9	-22.4
FL98080B	73 1	48.3	-21.6	273.9	39.8	-20.6	175.1	10.5	-18.4
FI 98075A	115 1	66.8	-29	290.4	23.1	-2.0	21.2	17	-17
FL 98074A	149.5	61.6	-7.8	318.5	28.0	-6.5	51.0	4.6	-6.2
FL 98070B	141 7	75.4	8.1	285.5	11 9	9.5	17.3	84	10.1
FI 98067B	126.4	15.7	5.6	19.5	45.9	6.0	229.9	30.7	72
GBEL005B	32.4	82.2	14.2	168.8	57	16.2	220.0	54	16.3
GBEL005C	92.7	72 7	12.6	284.0	16.7	13.0	193.0	3.1	14.2
GREL004A	30.2	78.3	72	287.1	27	70	106.5	11 /	87
GRELOU-A	147.8	62.3	86	270 3	15 7	9.0 Q. <b>/</b>	690.0	22.2	10.1
GRELOUAD	100.2	82.0	62	265.0	76	7.0	355 3	<u>~~</u> .~ 2∩	75
GREI MARC	288 4	65 1	24 R	<u>18</u> 9	13.0	25.2	144 0	2.0	27.2
GRELOUSO	283 7	74 7	20.2	95.7	15.2	20.2	186.3	20.1	21.0
	200.1	17.1	£0.£	50.1	10.2	<u> </u>	100.0	∠.∪	<b>∠</b> 1.7

		Minimum			Interm	ediate		Maxim	um
Sample	Declination	Inclination	Intensity	Dec.	Inc.	Intensity	Dec.	Inc.	Intensity
GBFL006A	241.9	76.1	16.1	71.0	13.7	16.7	340.5	2.1	18.0
GBFL006B	307.6	74.8	13.6	114.2	14.8	14.6	205.1	3.4	15.2
GBFL002A	114.1	62.4	9.4	280.1	26.9	10.1	13.0	5.7	10.5
GBFL002B	176.5	81.6	6.3	300.9	4.8	8.6	31.5	6.9	9.0
GBFL002C	222.1	60.0	8.0	122.6	5.4	8.8	29.5	29.4	9.1
GBFL001B	90.0	90.0	-10.5	90.0	90.0	-10.4	90.0	90.0	-9.5
GBFL001B	278.8	16.7	-10.8	65.4	70.2	-10.2	185.6	10.3	-9.5
GBFL001C	282.2	31.2	-11.8	116.8	58.0	-11.6	16.2	6.6	-10.5
GBFL007B	126.6	80.1	18.9	274.2	8.4	19.7	4.9	5.3	20.0
GBFL008A	270.0	71.6	-6.1	36.2	11.1	-5.6	129.1	14.5	-5.4
GBFL008B	298.7	63.2	-4.6	81.7	21.9	-4.2	177.7	14.6	-3.3
GBFL008C	140.3	50.2	-4.6	293.0	36.5	-4.1	33.4	13.6	-3.8
GBFL010A	241.2	55.3	6.2	100.3	28.3	6.7	0.0	18.4	7.1
GBFL010B	37.0	80.4	11.7	257.0	7.4	12.2	166.2	6.1	12.7
GBFL010C	335.7	77.9	9.8	86.6	4.4	10.7	177.5	11.3	11.0

## Appendix 6 - Hysteresis Data

Sample	Туре	Hc (mT)	Hcr (mT)	Hcr/Hc	Mrs/Ms	Slope Correction (MAm2/T*kg)
GBCY06B1	PELAGIC	8.33	18.93	2.27	0.12	7.35
GBCY06B2	PELAGIC	8.28	20.95	2.53	0.13	8.07
GBCY06C1	PELAGIC	7.84	11.04	1.41	0.16	7.68
GBCY06C2	PELAGIC	3.73	10.98	2.95	0.05	8.12
GBCY08A1	PELAGIC	4.10	10.47	2.56	0.06	6.04
GBCY08A2	PELAGIC	3.69	13.28	3.60	0.06	6.32
GBCY12A1	PELAGIC	4.51	17.23	3.82	0.06	3.23
GBCY12A2	PELAGIC	3.31	11.49	3.47	0.06	1.84
GBCY12B1	PELAGIC	8.22	4.27	0.52	0.06	1.32
GBCY12B2	PELAGIC	6.16	26.05	4.23	0.07	1.05
GBCY12C1	PELAGIC	5.20	2.60	0.50	0.07	1.64
GBCY12C2	PELAGIC	7.49	3.06	0.41	0.06	1.45
GBCY12D1	PELAGIC	5.38	12.92	2.40	0.06	2.99
GBCY12D2	PELAGIC	5.85	23.07	3.94	0.08	2.80
GBCY23B1	PELAGIC	2.99	2.17	0.73	0.02	3.12
GBCY23B2	PELAGIC	4.80	18.51	3.86	0.06	7.21
GBCY23C1	PELAGIC	4 02	18.55	4 62	0.05	5 11
GBCY23C2	PELAGIC	4 50	17.86	3.97	0.05	5 70
GBCY23D1	PELAGIC	8.83	19.79	2 24	0.00	4 84
GBCY23D2		11.63	40.27	3 46	0.00	1 24
GBPOL 03B		7 14	19.50	2 73	0.10	6.20
GBPOLOJE		14 70	21 50	1 46	0.00	-5 74
		10.40	14.00	1 35	0.10	-0.98
GBPOL07B		18.00	23 70	1.30	0.11	-28 70
GBPOLU/B		10.00	18 30	1.52	0.10	2 81
GBPOLISC GBPOLISE		23.00	10.30	1.73	0.11	1.01
CPPOL 10C		23.90	40.20	1.93	0.23	1.21
GBFUL 19C		9.21	14.00	0.52	0.11	4.56
		20.03	14.01	0.55	0.20	-20.00
GBPUL25B		19.21	10.20	0.54	0.24	2.39
GBPOL34C		19.30	27.01	1.44	0.20	-3.79
GBPOL35B		25.05	21.20	0.85	0.23	-1.20
GBPOL36B	PELAGIC	10.23	21.58	1.33	0.32	0.48
GBPUL3/B	PELAGIC	14.92	18.96	1.27	0.19	1.71
GBPOL38C	PELAGIC	11.02	10.30	0.93	0.19	2.47
GBPOL39B	PELAGIC	13.88	35.84	2.58	0.16	2.46
GBPOL40B	PELAGIC	14.60	28.64	1.96	0.17	-6.28
GBPOL41B	PELAGIC	14.67	31.81	2.17	0.17	-7.98
GBPOL46B	PELAGIC	23.37	52.76	2.26	0.22	-25.71
GBPOL50C	PELAGIC	20.18	38.49	1.91	0.24	-33.73
GBPOL52B	PELAGIC	13.09	8.90	0.68	0.17	-0.85
GBPOL53E	PELAGIC	16.34	22.51	1.38	0.24	-9.09
GBPOL56C	PELAGIC	15.23	23.25	1.53	0.18	-7.51
GBPOL61B	PELAGIC	11.27	13.20	1.17	0.15	-1.09
GBCY03A	NON-PELAGIC	4.41	27.47	6.23	0.07	0.14
GBCY03B	NON-PELAGIC	5.25	22.97	4.38	0.07	-1.28
GBCY03C	NON-PELAGIC	3.73	10.98	2.95	0.05	-0.27
GBCY03D	NON-PELAGIC	6.85	34.40	5.02	0.11	-1.72
GBCY04A	NON-PELAGIC	2.81	16.18	5.76	0.04	-0.30
GBCY04C	NON-PELAGIC	1.71	24.70	14.43	0.03	-0.07

## Appendix 6 - Hysteresis Data

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Sample	Туре	Hc (mT)	Hcr (mT)	Hcr/Hc	Mr/Ms	Slope Correction (MAm2/T*kg)
GBCY04D	NON-PELAGIC	0.31	42.13	135.90	0.01	-0.07
GBCY05A	NON-PELAGIC	3.22	23.01	7.14	0.06	1.25
GBCY09A	NON-PELAGIC	3.97	5.43	1.37	0.08	4.04
GBCY09B	NON-PELAGIC	5.89	25.77	4.37	0.10	4.63
GBCY09C	NON-PELAGIC	4.82	8.81	1.83	0.09	4.76
GBCY10C	NON-PELAGIC	7.47	22.24	2.98	0.16	0.17
GBCY13A	NON-PELAGIC	10.95	42.19	3.85	0.15	-9.02
GBCY13B	NON-PELAGIC	2.43	15.07	6.21	0.04	2.18
GBCY13D	NON-PELAGIC	9.85	43.17	4.38	0.15	-4.42
GBCY14A	NON-PELAGIC	4.90	22.65	4.62	0.06	-1.37
GBCY14B	NON-PELAGIC	11.54	48.40	4.19	0.21	-2.98
GBCY14C	NON-PELAGIC	6.30	33.24	<b>5.2</b> 7	0.07	-0.45
GBCY14D	NON-PELAGIC	5.89	30.48	5,18	0.08	-0.90
GBCY17B	NON-PELAGIC	9 93	29.34	2.95	0.19	-2.43
GBCY17C	NON-PELAGIC	7 81	40.20	5.15	0.15	-4.34
GBCY19A	NON-PELAGIC	5 30	28.62	5 40	0.11	-2.52
GBCY19B	NON-PELAGIC	5 19	45.07	8.68	0.09	-0.89
GBCY21C	NON-PELAGIC	7 09	32.58	4 60	0.00	1.77
GBCY21D	NON-PELAGIC	5 25	43 11	8.21	0.09	2 16
GBCY24A	NON-PELAGIC	6.03	30.78	5 11	0.00	2 27
GBCV24R	NON-PELAGIC	5 94	31 19	5 25	0.10	2.80
GBCY24C		12 57	28.64	2.28	0.12	4.35
GBCV24D		11.67	44 60	3.82	0.20	4.85
GBCV24E		9.95	47.00	4 74	0.22	5.50
GBCV24E		11 47	30.01	2.62	0.10	4 08
GBCV01B		9.23	6 38	0.69	0.20	2 87
GBCV10A		7.61	47 75	6.28	0.10	_0.89
GBCT IOA		11 56	50.08	∆ 33	0.12	-4.31
GBCV15A		10.10	70.31	6.96	0.17	4.01
GBCT15A GBCV15B		7 70	13 32	1 73	0.14	4.51
GBCTISD		12.18	33.02	270	0.10	0.99
GBCV01A		8 99	24.82	2.75	0.16	3 24
GBCY05D	NON PELAGIC	8 79	14 64	1.67	0.10	5 37
GBC103D		14 30	24.10	1.07	0.14	5.37
GBF0L00B	NON PELAGIC	7.58	78.30	10.33	0.14	A 31
	NON PELAGIC	29.50	36.00	1 25	0.10	-15 10
GBPOLITE CBDOL21C	NON PELAGIC	29.30	14 74	0.48	0.00	-30.71
GBF0L21C	NON PELAGIC	22.01	0.65	0.40	0.20	2 12
CPDOL27D	NON PELAGIC	22.31	12.00	0.42	0.52	2.12
GBF0L27B	NON PELAGIC	22.30	12.35	0.00	0.00	1 76
GBF0L29B	NON PELAGIC	22.10	12.00	0.30	0.20	1.70
CPDOL 21P	NON PELAGIC	19.03	0.44	0.70	0.27	3.08
GBPOLSIB	NON-FELAGIC	20.71	9.44 12.70	0.52	0.23	0.21
GBPUL32B	NON-PELAGIC	20.71	13.79	0.07	0.24	2.06
GBPUL33B	NON-PELAGIC	10.00	13.02	0.09	0.22	24.36
GBPUL43B	NON-PELAGIC	20.14	41.54	2.00	0.20	-24.30
GBPUL4/C	NON-PELAGIC	13.5/	19.39	1.43	U. 10	CO.U 22.02
GBPUL48B	NON-PELAGIC	21.31	53.58	2.51	0.21	-32. <del>3</del> 2
GBPOL49B	NON-PELAGIC	22.03	44.40	2.02	0.19	-40.00
GBPOL51B	NON-PELAGIC	13.3/	13.45	1.01	0.16	1.23
GBPOL54C	NON-PELAGIC	11.15	22.82	2.05	0.15	-1.13

Appendix 7 - Magnetic Properties Data										
		μSI	mA/m	mA/m	<b>mA/</b> m		mA/m	mA/m		
Sample	Order	Bulk K	Bulk A	SIRM	SIRM200	SIRM200/SIRM	"Magnetite"	T <b>M</b> 60	%Mgt	%T <b>M</b> 60
TH01B	56	55.10	0.26	418.37	319.62	0.76	319.62	98.75	76.40	23.60
TH02E	58	160.40	1.14	4036.95	3232.49	0.80	3232.49	804.46	80.07	19.93
TH03B	58	118.30	0.77	3193.20	2520.02	0.79	2520.02	673.18	78.92	21.08
TH07B	47	29.60	0.03	64.26	44.05	0.69	44.05	20.21	68.55	31.45
TH08C	46	15.50	0.03	37.95	28.25	0.74	28.25	9.70	74.44	25.56
TH09B	45	13.10	0.03	38.10	28.30	0.74	28.30	9.80	74.28	25.72
TH10B	48	36.60	0.05	104.25	74.76	0.72	74.76	29. <b>4</b> 9	71.71	28.29
TH11B	44	13.40	0.02	32.07	22.61	0.70	22.61	9.46	70.49	29.51
TH12B	43	31.50	0.04	93.53	64.09	0.69	64.09	29.44	68.52	31.48
TH13B	42	21.70	0.03	88.13	57.52	0.65	57.52	30.61	65.27	34.73
TH14B	39	26.60	0.04	136.66	99.65	0.73	99.65	37.00	72.92	27.08
TH15B	38	36.70	0.03	216.01	168.02	0.78	168.02	47.99	77.78	22.22
TH16B	37	35.70	0.03	244.40	189.15	0.77	189.15	55.25	77.39	22.61
TH17B	36	23.90	0.04	171.00	137.34	0.80	137.34	33.67	80.31	19.69
TH18B	35	16.30	0.03	90.81	74.06	0.82	74.06	16.75	81.55	18.45
TH19E	34	15.50	0.03	68.98	56.74	0.82	56.74	12.25	82.25	17.75
TH20B	33	18.60	0.03	85.50	69.36	0.81	69.36	16.15	81.12	18.88
TH21E	32	25.60	0.05	345.02	291.00	0.84	291.00	54.02	84.34	15.66
TH22C	31	34.70	0.07	478.56	379.08	0.79	379.08	99.48	79.21	20.79
TH23B	22	16.70	0.03	25.51	16.22	0.64	16.22	9.29	63.58	36.42
TH24E	21	8.90	0.03	15.50	12.22	0.79	12.22	3,29	78.79	21.21
TH25B	20	35.70	0.02	36.23	25.66	0.71	25.66	10.57	70.83	29.17
TH26B	19	25.60	0.03	46.01	35.70	0.78	35,70	10.30	77.61	22.39
TH27C	18	21.30	0.03	33.63	25.63	0.76	25.63	7.99	76.23	23.77
TH28A	17	19.60	0.03	31.46	16.61	0.53	16.61	14.86	52.78	47.22
TH29E	16	10.70	0.03	49.71	30.20	0.61	30.20	19.51	60.76	39.24
TH30A	15	20.60	0.03	34.82	24.73	0.71	24.73	10.09	71.02	28.98
TH31D	14	78.20	0.14	407.59	293.31	0.72	293.31	114.29	71.96	28.04
TH32C	13	85.90	0.12	426.51	311.01	0.73	311.01	115.50	72.92	27.08
TH33B	12	19.80	0.03	20.60	13.70	0.67	13.70	6.90	66.51	33.49
TH34B	11	30.80	0.04	42.75	31.66	0.74	31.66	11.09	74.06	25.94
TH35B	10	14.20	0.04	16.20	10.56	0.65	10.56	5.64	65.18	34.82
TH36B	9	18 90	0.04	27.63	17 40	0.63	17.40	10.23	62.98	37.02
TH37B	8	12.60	0.03	26.75	17.95	0.67	17.95	8.80	67.11	32.89
TH38E	7	15.70	0.02	44.15	29.41	0.67	29.41	14.75	66.60	33.40
TH39A	6	18.00	0.04	22.17	15.21	0.69	15.21	6.96	68.59	31.41
TH40B	5	61.60	0.02	147 03	116.54	0.79	116 54	30.48	79.27	20.73
TH41B	4	44.60	0.04	152 04	118.71	0.78	118.71	33.33	78.08	21 92
TH42B	3	30.20	0.04	55.91	37 02	0.66	37.02	18 89	66 21	33 79
TH43B	2	19.40	0.02	28.90	18.95	0.66	18.95	9.95	65.58	34 42
TH44B	1	31.50	0.04	97.58	63 23	0.65	63.23	34.35	64 80	35.20
TH50B	50	23.10	0.03	27.80	19 46	0.00	19.46	8.33	70.02	29.98
TH51C	49	40.10	0.00	151.00	103.40	01.0 0 0 0	103.43	47 10	68.82	31 18
TH52C	54	56.40	0.00	107.00	77 41	0.00	77 41	30 31	71.86	28.14
TH53C	55	23.60	0.00	71 85	52 57	0.72	50 57	10.28	73 17	26.83
TH54C	53	62 60	0.00	361 10	289 79	0.75 0.80	280 70	71 40	80.23	10.00
TH55C	52	32.60	0.10	124 56	88 14	0.00	200.79 88 1/	26 43	70 75	29.25
TH56C	51	48 10	0.02	411 DA	204 08	0.71	20/ 08	116 06	71 55	28.25
TH57C	40	62 10	0.03	600.62	207.00 218 53	0.72	234.00 218.53	182.00	69.68	30 32
110/0		UL. (U	0.10	000.02	-10.00	0.70	410.00	102.03	00.00	JU.JZ

Appendix 7 - Magnetic Properties Data										
	μSI	mA/m	mA/m	mA/m		mA/m	mA/m			
Order	Bulk K	Bulk A	SIRM	SIRM200	SIRM200/SIRM	MTG	TM60	%Mgt	%TM60	
32	23.60	0.04	58.38	39.59	0.68	39.59	18.80	67.81	32.19	
28	19.80	0.04	96.66	72.15	0.75	72.15	24.51	74.64	25.36	
27	28.00	0.04	114.75	83.71	0.73	83.71	31.04	72.95	27.05	
26	31.00	0.05	82.49	56.84	0.69	56.84	25.65	68.90	31.10	
25	21.70	0.04	69.47	46.10	0.66	46.10	23.37	66.36	33.64	
	Order 32 28 27 26 25	μSI Order Bulk K 32 23.60 28 19.80 27 28.00 26 31.00 25 21.70	μSImA/mOrderBulk KBulk A3223.600.042819.800.042728.000.042631.000.052521.700.04	Appendix       µSI     mA/m     mA/m       Order     Bulk K     Bulk A     SIRM       32     23.60     0.04     58.38       28     19.80     0.04     96.66       27     28.00     0.04     114.75       26     31.00     0.05     82.49       25     21.70     0.04     69.47	Appendix 7 - Magneti       µSI     mA/m     mA/m     mA/m       Order     Bulk K     Bulk A     SIRM     SIRM200       32     23.60     0.04     58.38     39.59       28     19.80     0.04     96.66     72.15       27     28.00     0.04     114.75     83.71       26     31.00     0.05     82.49     56.84       25     21.70     0.04     69.47     46.10	Appendix 7 - Magnetic Properties Da       µSI     mA/m     mA/m     mA/m       Order     Bulk K     Bulk A     SIRM     SIRM200     SIRM200/SIRM       32     23.60     0.04     58.38     39.59     0.68       28     19.80     0.04     96.66     72.15     0.75       27     28.00     0.04     114.75     83.71     0.73       26     31.00     0.05     82.49     56.84     0.69       25     21.70     0.04     69.47     46.10     0.66	Appendix 7 - Magnetic Properties Data       µSI     mA/m     mA/m     mA/m     mA/m       Order     Bulk K     Bulk A     SIRM     SIRM200     SIRM200/SIRM     MTG       32     23.60     0.04     58.38     39.59     0.68     39.59       28     19.80     0.04     96.66     72.15     0.75     72.15       27     28.00     0.04     114.75     83.71     0.73     83.71       26     31.00     0.05     82.49     56.84     0.69     56.84       25     21.70     0.04     69.47     46.10     0.66     46.10	Appendix 7 - Magnetic Properties Data       µSI     mA/m     mA/m	Appendix 7 - Magnetic Properties Data       µSI     mA/m     mA	

# Limestones distinguished by magnetic hysteresis in three-dimensional projections

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[1] Magnetic hysteresis data determine the suitability of rocks for paleomagnetic work, provide clues to paleoenvironment and paleo-climate and they may characterize depositional environments for limestones. However, the variables chosen for conventional two-dimensional hysteresis plots, such as that of Day et al. [1977], are not always suitable to discriminate between samples. Distinguishing samples by their regression surfaces in 3D hysteresis space may be more successful in some cases [Borradaile and Lagroix, 2000] but a 2D projection with a less arbitrary viewing axis is preferable for routine reporting. We show that limestone samples are simply discriminated in a new 2D projection produced by projecting hysteresis data from three dimensions (x, y, z = Mr/Ms, Bcr, Bc) onto a plane containing the Mr/Ms axis. The orientation of the plane is controlled by its x-axis that is defined by a suitably selected Bcr/Bc ratio, most often in the magnetite PSD range, 2 < (Bcr/Bc) < 4. INDEX TERMS: 1527 Geomagnetism and Paleomagnetism: Paleomagnetism applied to geologic processes; 1533 Geomagnetism and Paleomagnetism: Remagnetization; 1540 Geomagnetism and Paleomagnetism: Rock and mineral magnetism; 1594 Geomagnetism and Paleomagnetism: Instruments and techniques. Citation: Borradaile, G. J., and T. Hamilton, Limestones distinguished by magnetic hysteresis in three-dimensional projections, Geophys. Res. Lett., 30(18), 1973, doi:10.1029/ 2003GL017892, 2003.

### 1. Introduction

[2] The magnetic properties of sediments are valuable and efficient indicators of grain size and environmental conditions [Banerjee et al., 1981; King et al., 1982; Thompson and Oldfield, 1986]. This is directly due to the predominance of magnetite, which forms approximately 2 wt% of the crust on a modal basis, and the predominant role of grain-size controlling its magnetic domain structure. However, other physical factors for magnetite and other minerals are easily considered where necessary [Dunlop and Özdemir, 1997]. Attention is focused on limestones due to sedimentological and biogenic constraints and on the grain-size and low-stress state of its magnetite [Freeman, 1986; Henshaw and Merrill, 1980; Lowrie and Heller, 1982], which permits limestones depositional facies to be characterized by their hysteresis response [Borradaile et al., 1993]. Hysteresis properties may also diagnose hard-remagnetization in carbonates [Channell and McCabe, 1994; Jackson, 1990; Jackson et

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al., 1992; McCabe et al., 1984], a serious complication in paleomagnetic work.

### 2. Magnetic Characterization

[3] A rock's remanence-bearing properties are characterized by saturation isothermal remanence (SIRM = Mr) after exposure to a large field or Ms in the presence of a large field. Similarly, the tenacity of remanence is important, measured by coercivity (Bc), coercivity of remanence (Bcr) or the ease of demagnetization in alternating field (AF). *Cisowski* [1981] plots decaying remanence with AF against progressive acquisition of IRM, and determination of SIRM to infer magnetite grain-size and separation. *Wasilewski* [1973] plots Bc against Bcr; and most popular, *Day et al.* [1977] plot Mr/Ms against Bcr/Bc. The latter has now become synonymous with "hysteresis plot".

[4] The success of the Day plot comes from its ability to separate behavior according to the presence of singledomain (SD), pseudo-single domain (PSD) or multidomain (MD) magnetite, especially where the specimens contain magnetite in just one of these categories. These are traditionally shown as rectangular fields (Figure 1a) but, as Dunlop [2002a, 2000b] shows the reality of mixed grainsize distributions that encompass more than one type of domain-behavior, including superparamagnetic (SP) makes its use less clear-cut. Moreover, clear SD domain behavior is unlikely to be isolated [Lanci and Kent, 2003]. Viewing the data set along a less arbitrary axis through hysteresis space provides an ad hoc solution to magnetic discrimination. Linear discrimination functional analysis does this formally but with so few variables, it suffices to re-examine the data-set using a changed coordinate system. Since hysteresis experiments determine Bcr and Bc separately, it is profitable to make a three-dimensional hysteresis plot of Mr/Ms against Bcr, and Bc (Figure 1b). This plot successfully separates some data-sets but the choice of view is limited by the data-distribution and effective visual discrimination is not always possible, although regressionsurfaces were always distinct [Borradaile and Lagroix, 2000].

[5] Without recourse to regression surfaces or other statistics that impede visual appreciation, it is possible to retain the information from the three variables (Bcr, Bc and Mr/Ms) and yet avoid the data-superposition of the traditional Day plot (Figure 1a). The simple principle is to project the data from 3D-hysteresis space onto a pre-selected plane, which contains the Ms/Mr axis. For example, two such planes are shown in Figure 1b, designated as the Bcr = 10Bc and the Bcr = Bc planes. Experience with approximately 500 hysteresis x-y-z points obtained from limestones using the

**SDE** 11 - 1



Figure 1. (a) The traditional two-dimensional hysteresis plot may fail to discriminate samples on the basis of hysteresis ratios. Here pelagic limestones are compared with shelf limestones, from sampling projects in UK and Israel. (b) A 3D plot of Bcr and Bc individually against Mr/Ms spaces may be more successful but data-points must be categorized by regression surfaces for recognition purposes. We will show that projecting the 3D data onto a vertical plane containing the Mr/Ms axis produces a 2D graph that successfully discriminates the data of (a). SD, PSD and MD refer to domain-size ranges for single, pseudo-single and multi-domain magnetite. SP = superparamagnetic behavior.

Princeton Measurements MicroMag 2900 shows us that suitably sensitive factors of Bc range from 1.5 to 5.0.

## 3. [4] The 2-D Projection Plane in 3D Hysteresis Space

[6] The approach is so simple that we were able to choose the optimum projection plane until the best visual discrimination was obtained. The calculations were simply performed in a spreadsheet in which we varied the orientation of the vertical projection plane. The choice was made less subjective by comparing the 95% confidence region for the bivariate distribution on the projection plane. For example, consider the small sample of shallow-water lime-stones (Figure 2); the bivariate data-set has y = Mr/Ms and x defined by the coordinate of the hysteresis data projected onto the plane Bcr = 1.8Bc. Calculations were simplified by standardizing x and y according to traditional statistics, e.g.,

$$z_x = \frac{x - \bar{x}}{s_x}$$
 where  $s_x =$  standard deviation.

With the data distributed about their centroid in equal units of standard deviations (Figure 2a), one may simply calculate the eigenvalues and eigenvectors of the distributions from

Figure 2. (opposite) (a) Further visual simplification for the bivariate distribution of the 3D data projected on to some particular projection plane is achieved by plotting 95% confidence regions. (a) Coordinates of the points on the projection plane are standardized in units of standard deviations, centered on the data-centroid; the eigenvalues and eigenvectors calculated from the variance-covariance matrix determine the elliptical confidence region. (b) Standardized values are back-transformed to show confidence regions on the hysteresis projection plane. (c) 95% confidence regions for three formations of the progressively shallowing post-Cretaceous limestone cover to the Troodos ophiolite of Cyprus on a 2D hysteresis-projection plane.





Figure 3. (a, b) The projection plane Bcr = 1.8Bc in 3D hysteresis- space (Figure 1b, c) appears to discriminate the pelagic and non-pelagic limestones that were almost indistinguishable on the conventional Day Plot (Figure 1a). (c, d) different projection planes showing the overlap of 95% confidence regions for the pelagic and non-pelagic limestones of Figure 1a.

the variance-covariance matrix [e.g., *Davis*, 2002]. The coordinates of the confidence region may then be back-transformed to the original hysteresis scales (Figure 2b). For example, samples of three different and progressively shallower limestone formations, used by *Borradaile and Lagroix* [2000] in their 3D projection are shown in Figure 2c. The earlier 3D projection provided their precise inter-sample discrimination but only by viewing regression surfaces along an appropriate axis. The present 2D projection in hysteresis space has the advantage of simpler reporting as a plane-diagram (Figure 2c). Moreover, the plane's orientation is described by a Bcr/Bc ratio that itself may be characteristic of some magnetite domain-structure, since the upper and lower PSD limits are 2 < (Bcr/Bc) < 4 [*Dunlop*, 2002a, 2000b].

[7] On the plot of *Day et al.* [1977], the initial example of limestone hysteresis data shows almost complete overlap of pelagic and non-pelagic data (Figure 1a) although it is reasonable to expect some differences in magnetic properties. These limestones, like most others, have quite simple constraints on their magnetic mineralogy. For example, fossil-bacterial magnetite may be expected to dominate pelagic limestones whereas clastic, aerial-volcanic and other organic sources may dominate shelf carbonates. Day-plot space shows a similar broad trend from PSD to SD due to broad grain-size distributions [*Dunlop*, 2002a]. However, projected onto an arbitrary "suitable" vertical plane through 3D hysteresis space (Figure 1b) the difference between the data clusters is maximized (Figure 3a and 3b). For these two samples this is achieved by a vertical projection plane close to the lower bound of PSD space (Figure 1b), e.g., Bcr = 1.8Bc. The confidence regions for differently chosen projection planes are presented in Figure 3c and 3d.

[8] Why should the use of a projection plane with Bcr  $\sim$  2Bc successfully separate the hysteresis data of pelagic versus non-pelagic samples (Figure 3)? Consideration of Figures 1a and 1b indicates this vertical plane lies close to the lower size-limit of PSD magnetite, and biogenic magnetite may show Bcr/Bc < 1.8 [Moskowitz et al., 1993]. Evidently, such a plane separates the two samples with pelagic specimens (Figure 3b) lying low in the plane, projected from the SD field of 3D-space (Figure 1b) and non-pelagic specimens plotting higher, projected from the PSD 3-space. The broad swathe of superparamagnetic behavior [Dunlop, 2002a, 2000b] shown on Figure 1a acts most effectively at high Mr/Ms which helps to emphasize the definition of the non-pelagic sample higher in the 2D projection (Figure 3a). Organic magnetite may play different roles in pelagic and non-pelagic environments [Kirschvink and Chang, 1984; Moskowitz et al., 1989] and the effects of mixing with magnetite of aerial-volcanic and detrital origin are difficult to model. However, the pelagic sample here seems to be dominated more by SD whereas the nonpelagic sample projects from the PSD field, higher on the Mr/Ms axis indicating some SP behavior.

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## Magnetic fabrics may proxy as neotectonic stress trajectories, Polis rift, Cyprus

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[1] The Miocene Polis rift opened along a NNW axis, obviously in response to WSW relative extension and relative tension starting  $\sim 5$  Myr ago. However, geologically young plate movements are believed to be closing the rift by sinistral transpression producing minor younger faults since 1 Ma. Modern earthquake solutions give E-W compression compatible with the younger faults. Magnetic fabrics using anisotropy of low field magnetic susceptibility (AMS) and anisotropy of anhysteretic remanent magnetization are kinematically compatible with stress axes required by the fault and rift geometry and thus were acquired in <5 Ma. However, by different statistical treatments and selecting samples from different subareas it is possible to reveal sedimentary-depositional fabrics and perhaps also a composite AMS fabric related to young transpression (<1 Ma).INDEX TERMS: 1518 Geomagnetism and Paleomagnetism: Magnetic fabrics and anisotropy; 8107 Tectonophysics: Continental neotectonics; 8123 Tectonophysics: Dynamics, seismotectonics; KEYWORDS: magnetic fabrics, stress trajectories, neotectonics. Citation: Borradaile, G. J., and T. Hamilton (2004), Magnetic fabrics may proxy as neotectonic stress trajectories, Polis rift, Cyprus, Tectonics, 23, TC1001, doi:10.1029/2002TC001434.

## 1. Introduction: Polis Rift, Cyprus, and its Tectonic History

[2] The Polis rift is a mid-Miocene fault valley, bounded by normal faults with throws of  $\leq 100$  m [Payne and Robertson, 1995; Robertson, 1990] (Figure 1). The NNW trending rift evidently formed above a northward dipping subduction zone, although it is argued that the northward component of motion is now stalled in favor of WSW subduction [Arvidsson et al., 1998; Ben-Avraham et al., 1988; Papazachos and Papaioannou, 1999; Robertson et al., 1995] (Figure 2). The rift disrupts subhorizontal Miocene strata at the surface and its basin is filled with subhorizontal Pliocene sediments. Penetrative tectonic fabrics are not visible but the fracture orientations permit crude estimates of the orientations of paleostress trajectories according to traditional structural geology. A WSW-ENE minimum compressive stress trajectory is required for the

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formation of the Polis rift, using accepted structural interpretation. However, fault solutions for the 1995 earthquakes indicate that the rift is instead being compressed EW to close the rift with sinistral transpression (Figure 1).

[3] Modern seismicity has been quite hazardous and is of concern to Cypriots. Historically, the region was devastated by earthquakes, causing abandonment of classical cities in the first few centuries before and after Christ. Present-day seismic events are monitored attentively. The modern seismic record, mainly from offshore events, shows a Benioff zone descending northward and northeastward from the south and southwest of Cyprus (Figure 2). The depths of the foci show that deeper subduction is now mostly to the WSW, compatible with the geodetically determined vectors of relative plate motion [Arvidsson et al., 1998; Papazachos and Papaioannou, 1999]. Thus, recent seismicity and plate motion both indicate that the Polis rift is now undergoing transpressive closure with EW compression. Recently, however, the Polis region experienced onshore seismic events with body wave magnitudes of 5.8 and 5.3 respectively on 1995/02/23 and 1995/05/29, (Figure 1). The epicenters lay in the center and east of the rift but most injury and damage occurred on the western margin. Foci were shallow, at  $\sim$ 15 km. The centroid moment tensor (CMT; catalog available from http://www.seismology.harvard.edu/) for the two events yields almost indistinguishable fault plane solutions giving east plunging compression (trend and plunge  $\sim 102/$ 29; see Harvard online seismology catalog, available at http:// www.seismology.harvard.edu/projects/CMT/2001; see also online catalog from International Seismological Centre, Thatcham, UK, available at http://www.isc.ac.uk/) (Figures 1 and 6c). This is not compatible with the WSW extension required to create the WNW trending rift ( $\sim 5$  Ma) but more compatible with younger fault orientations (<1 Ma). This switch in stress axis orientation may be due to changes in plate tectonic geometry.

### 2. May Magnetic Fabric Axes Proxy for Geologically Significant Paleostress Trajectories?

[4] Originally, paleomagnetism introduced measurements of anisotropy of induced magnetic susceptibility in low fields (AMS) in order to reject strongly anisotropic specimens [Fuller, 1963; Uyeda et al., 1963]. Such materials would be unsuitable for paleomagnetism because the intrinsic anisotropy may have deflected the paleofield from its true orientation. Subsequently, AMS was found to be a

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Figure 1. Location of the Polis rift in NW Cyprus. Pliocene sediments fill the valley between faulted Miocene and pre-Miocene rocks on the flanks. Although the bounding faults to the rift (~5 Ma) are Normal, recent seismic events give fault plane solutions with sinistral transpression across the rift. (Two events of 1995/02/23 mb = 5.8 event number 56311987; 1995/05/29 mb = 5.3 event number 052995A; see Harvard Seismology Bulletin, available from the online CMT catalog at http://www.seismology. harvard.edu/projects/CMT/; see also International Seismological Centre online bulletin, available at http://www.isc.ac.uk/); these are compatible with the orientations of younger faults ( $\leq 1$  Ma).

sensitive indicator of the average preferred orientation of mineral grains and was applied to determine mineral alignment whether by tectonic, sedimentary or magmatic flow [Borradaile and Henry, 1997; Hrouda, 1982; Tarling and Hrouda, 1993]. The technique is sufficiently sensitive to detect the feeble strains and fabrics in neotectonic environments, although initially the literature may have overstated the simplicity of interpretation of magnetic fabrics. In fact, AMS blends contributions from different minerals, of different ages, with different orientation distributions and for which the physical response may also be either paramagnetic, diamagnetic or "ferro"-magnetic [Jackson and Tauxe, 1991; Rochette et al., 1992]. Moreover, the minerals' AMS axes only map onto the orientation of crystallographic axes if the crystals are of high symmetry (e.g., orthorhombic, trigonal) due to fundamental symmetry relations [Nye, 1957] and, unfortunately, most paramagnetic rock forming minerals are monoclinic at best. Furthermore, ferromagnetic inclusions may disturb or completely mask the relationship between crystallographic axes of the host grain and its AMS ellipsoid. Thus, at the single-crystal level, AMS axes and crystal axes rarely show a one-to-one correspondence [Borradaile, 1994; Borradaile and Werner, 1994; Lagroix and Borradaile, 2000a]. As if confounding of these different geological and magnetic factors was not troublesome enough, some minerals may even yield "inverse" fabrics in which AMS counter-intuitively represents their fabric orientation-distribution ellipsoids [Rochette, 1987, 1988; Rochette et al., 1992, 1999]. In this study, calcite is the main cause of inverse fabrics [Rochette, 1988] and its largest negative susceptibility corresponds with its crystallographic c axis, permitting a simple interpretation of calcite-dominated specimens that respond diamagnetically. However, single domain magnetite (SD) is the most often cited cause of inverse fabrics, or of mixed SD-MD "blended" fabrics (e.g., the "intermediate" fabrics of Rochette [1987]; Rochette et al. [1999]). The SD inverse contribution to a magnetic fabric arises because the spontaneous mag-



Figure 2. Depths to earthquake foci of seismic events (1963–1999) (see International Seismological Centre online bulletin, available at http://www.isc.ac.uk/), indicate a northward dipping Benioff zone. However, the deepest foci occur just to the west of Cyprus, which together with the geodetically determined plate vectors, confirms that current subduction is more toward the NE. It will be shown that this geological young compression and closure of the Polis rift is also detectable from cryptic magnetic fabrics. The pre-Pliocene, northward subduction is stalled by the obstruction of the Eratosthene seamount, giving rise to the present ESE-WNW compression [Arvidsson et al., 1998; Papzachos and Papaioannu, 1999; Ben-Avraham et al., 1988; Robertson et al., 1995].

netization of a single domain must be parallel to its long axis, which cannot be enhanced during induced magnetization, when AMS is measured. In contrast, during the measurement of AMS, the induced magnetization may be increased perpendicular to the long axis. Thus the AMS magnitude-ellipsoid's long-axis will be perpendicular to the SD long-axis. Fortunately, anisotropy of remanent magnetization is congruent with shape, so that maximum remanence is parallel to grain long-axes. Therefore axes of anisotropy of anhysteretic remanent magnetization (AARM) correspond to the orientation-distribution for all magnetite grain sizes [Jackson, 1991; McCabe et al., 1985; Stephenson et al., 1986]. AARM is the most secure means by which to determine the true shape-fabric of magnetite, although data processing methods may help [Borradaile and Gauthier, 2001]. Our study found that complications due to the SD effect were negligible in these carbonate rocks. Thus the fabric contribution of magnetite is relatively straightforward, especially since its interpretation is simplified by the AARM technique.

[5] For the purposes of magnetic mineralogy, the limestones fall broadly into clay-bearing varieties that are invariably paramagnetic, and more pure limestones that may be diamagnetic or have feeble paramagnetic susceptibilities. Both types have subordinate ferromagnetic responses due to ferrimagnetic magnetite and the distribution of their hysteresis parameters on a Day plot is similar (Figure 3a). The hysteresis response, determined using our Princeton Measurements MicroMag alternating gradient force magnetometer, is that of single domain (SD) or pseudo-single domain (PSD) magnetite with ferromagnetic susceptibilities and saturation remanences compatible with SD/PSD magnetite (Figures 3a and 3b) [Dunlop and Özdemir, 1997]. The lithologies and the fine grain size of the magnetite favor a fossil-bacterial origin for the magnetite, rather than clastic contamination [Borradaile and Lagroix, 2000; Lagroix and Borradaile, 2000b]. Furthermore, the frequency distribution of bulk susceptibility supports the partial control of magnetic anisotropy due to the magnetite traces. Any dilute concentration of high value, such as accessory, high susceptibility magnetite, tends to form a lognormal distribution (Figures 3c and 3d). Thus we see a competition between the diamagnetic matrix ( $\sim -14 \times 10^{-6}$  SI), paramagnetic clay



**Figure 3.** Rock magnetic experiments reveal that the limestones magnetic fabrics are due to a diamagnetic carbonate matrix, traces of paramagnetic clays and ferrimagnetic magnetite of single domain to pseudo-single-domain size. (a) Day et al. [1977] plot of hysteresis data showing the fine domain structure of the magnetite, perhaps due to fossil bacterial sources [Borradaile and Lagroix, 2000; Dunlop and Özdemir, 1997]. (Ms = saturation magnetization in applied field; Mr = zero-field remanence; Hcr = coercivity of remanence; Hc = coercivity). (b) Ferromagnetic susceptibility and saturation magnetization show ratios typical for fine-grained magnetite [Dunlop and Özdemir, 1997]. (c) Frequency distribution of bulk susceptibility combined with petrographic observations may attribute the susceptibility to the diamagnetic matrix (for calcite approx.  $\sim -14 \times 10^{-6}$  SI), and traces of paramagnetic clay and fine-grained, single domain magnetite, probably of bacterial rather than clastic origin. Modal bulk susceptibility is  $+16.1 \pm 7.1 \times 10^{-6}$  SI (n = 205). (d) The lognormal frequency distribution of bulk susceptibility is characteristic of a dilute concentration of a rare fraction with high values.

contamination in some specimens that gives susceptibilities up to  $\sim +120 \times 10^{-6}$  SI, and the traces of magnetite that keep the net modal bulk susceptibility positive at  $+16.1 \pm 7.1$  (s.e.)  $\times 10^{-6}$  SI (n = 205). [6] The AMS signal of PSD magnetite and clays provides a normal fabric contribution, the AMS magnitude-ellipsoid being congruent with the combined orientation-distribution ellipsoid of magnetite-grain-shapes and clay-mineral pre-



 $\sigma_{\rm C} \geq \sigma_{\rm N} \geq \sigma_{\rm T}$  Seismic notation for principal stress with fault-plane solution

 Maximum, intermediate and minimum axes of mean AMS tensor (with 95% confidence cones)



density contours of specimen tensors in multiples of expected uniform density

Figure 4. Pliocene sediment infill of the Polis rift; anisotropy of low field magnetic susceptibility (AMS) in (All stereograms in this paper are equal-area, lower hemisphere.) The mean tensor accounts for the magnitudes as well as the orientations of the individual specimen tensors. Thus different orientation distributions of the mean tensor result from standardizing or not standardizing the specimen tensors to a unit-bulk susceptibility [Jelinek, 1978; Borradaile, 2001]. The mean tensor, with 95% confidence limits on the orientations of its principal axes [Jelinek, 1978] is a powerful tool in interpreting magnetic petrofabrics, whereas traditional orientation distributions of AMS axes, shown by the density contours in Figure 4c may be more limited because they ignore the magnitudes of susceptibility axes.

ferred crystallographic orientation. Thus maximum susceptibility  $(k_{MAX})$  defines the orientation of magnetite and clay mineral alignment whereas the minimum susceptibility  $(k_{MIN})$  defines the mean normal to the planar fabric defined by the minerals. In specimens bearing SD magnetite, its concentration is too low to form inverse fabrics because the clay fraction's paramagnetic normal fabric dominates.

[7] Despite the presence of trace amounts of fine-grained magnetite and of clay, the limestones' diamagnetic calcite matrix dominates the AMS signature in some specimens



Figure 5. The faulted margins of the Polis rift; different data processing treatments of data for anisotropy of low field magnetic susceptibility (AMS).

(Figures 4c and 4d). Examples of net-paramagnetic specimens whose AMS axes are directly interpretable in terms of kinematics are shown in Figures 4b, 4d, and 5b. All samples are combined in Figures 4a, 4c, 5a, and 5c, including the majority of dominantly diamagnetic specimens whose maximum and minimum axes were switched. The orientation of susceptibility axes for individual specimens is shown in Figure 4c in the form of density contours. Of course, the traditional interpretation of the AMS orientations using individual specimens loses the information contained in the magnitudes of the susceptibility axes. Although the magnitudes and shapes of magnetic fabric ellipsoids rarely bears any direct relation to a causative process such as strain or flow [Borradaile and Henry, 1997; Hrouda, 1982; Tarling and Hrouda, 1993], the magnitudes do affect the interpretation of the orientation-distribution since the magnitudes may weight the significance of different specimens in different ways [Borradaile, 2001; Henry, 1989; Hrouda and Jelinek, 1999; Hrouda and Schulmann, 1990; Jelinek, 1978]. For this reason, the mean tensor of a sample of specimens need not correspond closely to the traditional density-distribution of individual specimen axes, and any comparison is only valid with mean tensors for the sample, disregarding magnitudes (e.g., Figures 4c, 5c, and 6b).

[8] Magnetically determined orientation-distributions are interpreted in terms of finite strain or recrystallization fabrics in tectonically deformed or metamorphic rocks. In those cases, the magnetic anisotropy tensors correspond in orientation to the tensor-of-state that describes finite strain, in its broadest sense. In contrast, neotectonic environments lack penetrative deformation fabrics due to finite strain: they are affected by small strains which structural geologists would interpret due to incremental, almost infinitesimal strains [Ramsay, 1967; Ramsay and Huber, 1983]. Infinitesimal strain axes are traditionally associated with certain arrangements of fractures, calcite-twinning, and vein-mineral fibers. These strains are so small that the possibilities for changes in stress orientations are limited and the incremental strain axes are subparallel to the principal-stress trajectories. Thus the fracture pattern ties the incremental

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Figure 6. Polis rift faulted margins; (a) raw AMS compatible with rift closure; (b) AARM compatible with rift opening; (c) faults all compared with the centroid moment tensor solutions for the recent earthquakes. (1995/02/23 mb = 5.8; 1995/05/29 mb = 5.3; see Harvard Seismology Bulletin, available at http://www.seismology.harvard.edu/projects/CMT/).

strains and paleostress trajectories in a simple coaxial framework that is closely related to the fault plane solution of the 1995 earthquake, south of Polis (event number 052995A; see Harvard online seismology catalog, available from http://www.seismology.harvard.edu/projects/ CMT/). Unfortunately, the structural geologist's traditional interpretation of mean stress trajectory orientations from fault orientations provides only a global and imprecise regional estimate. In contrast, magnetic fabrics may be obtained from almost any individual rock specimen, they sum the effects of thousands of events and, as we will see below from the literature and current observations, they help to strengthen the link between paleostress in any outcrop with the rift structure and with the 1995 earthquakes.

[9] Experimental work shows that magnetite's magnetic properties are sensitive to stresses of tectonic and subtectonic magnitude [Carmichael, 1968, 1969; Domen, 1962; Borradaile and Alford, 1987; Borradaile and Jackson, 1993; Jackson et al., 1993; Hamano et al., 1989; Kinoshita, 1968; Kalashkinov and Kapitsa, 1952; Kapicka, 1992; Nagata, 1966a, 1966b, 1970]. In particular, the maximum susceptibility of polydomain magnetite is deflected away from the maximum compressive stress axis, mostly due to nonreversible, domain wall rearrangements. However, bulk strains of  $\leq 5\%$  may produce microscopic heterogeneous deformation in which grainscale strain is capable of rigid-grain rotation. Much of the experimental work attempted to predict earthquakes from geomagnetic field variation due to susceptibility changes [e.g., Revol et al., 1977; Stacey, 1964]. Reports of experimental studies, involving a variety of deformation mechanisms, all show that maximum susceptibility  $(k_{MAX})$  tends to align with minimum compressive stress direction under modest differential stress. Most studies concerned specimens in which the AMS was dominated by polydomain magnetite but under most circumstances the subtle realignment of paramagnetic grains also requires that  $k_{MAX}$  aligns with  $\sigma_{MIN}$ .

[10] It is understandable that very few field studies have the possibility to confirm a relationship between AMS and "stress," as opposed to "strain." They are mostly confined to Quaternary neotectonic environments where simple stratigraphy and single-event brittle tectonics permit a relatively unambiguous association between AMS fabrics and stress axes inferred from fracture patterns [Facenna et al., 1994; Mattei et al., 1997, 1999; Sagnotti and Speranza, 1993; Sagnotti et al., 1994; Winkler and Sagnotti, 1994]. Their advantage, as in the present study is that a young stratigraphy, devoid of penetrative deformation permits an association of magnetic fabrics with events that cannot endure more than a few Ma. In some neotectonic studies, stratigraphy constrains the acquisition of AMS fabrics to intervals of not more than several hundred thousand years. Even in more complicated geological environments, fortunate geological conditions may permit us to associate AMS axes with stress trajectories [Lagroix and Borradaile, 2000b; Borradaile and Kehlenbeck, 1996], rather than its much more common use as a finite strain marker [Tarling and Hrouda, 1993]. However, neotectonic environments have the advantage of fine biostratigraphic control, rock types with simple preexisting petrofabrics and close temporal relationships to contemporary ground stresses.

[11] In this study, AMS combines fabric contributions from diamagnetic calcite, paramagnetic clays and PSD magnetite in Miocene and Pliocene limestones. Isolating the petrofabric contribution of the magnetite subfabric by determining the specimens' anisotropy to the acquisition of anhysteretic remanence (AARM) is a relatively recent development in magnetic fabrics [Jackson,1991; McCabe et al., 1985]. AARM responds only to the orientationdistribution of magnetite in our rocks, ignoring the fabrics of the paramagnetic clays and diamagnetic calcite. Of course, the matrix may dictate the orientation-distribution of magnetite, if it occurs as inclusions or mimetic overgrowths on the matrix grains. Regardless of magnetite grain size or domain structure, AARM gives a unique interpretation of magnetite preferred dimensional orientation (Figure 6), more simply interpreted kinematically than some AMS fabrics [Jackson, 1991; Jackson and Tauxe, 1991].

[12] Where all minerals produce normal fabrics, results of experimental and field studies indicate the following correspondence between AMS principal axes (k > 0), incremental extension (e), and compressive stress ( $\sigma$ ):  $k_{MAX}$  parallel to  $e_{MAX}$  parallel to minimum compression,  $\sigma_{MIN}$  ( $\sigma_T$ ); and  $k_{MIN}$  parallel to  $e_{MIN}$  parallel to maximum compression  $\sigma_{MAX}$  ( $\sigma_C$ ). (By the convention of seismologists the principal stresses would be  $\sigma_C \ge \sigma_N \ge \sigma_T$ ).

[13] Of course, the kinematic significance of the maximum and minimum susceptibility axes must be considered carefully for diamagnetic calcite crystals because their most "negative" susceptibility corresponds to the c axis, which aligns with the shortening or maximum compression direction.

### 3. Magnetic Fabrics: Methods

[14] We measured anisotropies of low field susceptibility (AMS) of 205 cores and anisotropy of anhysteretic remanent magnetization (AARM) for 45 cores, from 62 sites in the fault affected Miocene and younger strata of the Polis rift and from sediments unaffected by faulting in the rift basin (Figure 1). Cores were right cylinders 25 mm in diameter and 22 mm high prepared from oriented field specimens that were re oriented in a tilting-vice arrangement under a laboratory drill press. AMS was determined using a Sapphire Instruments SI2B device operating at 19,200 Hz and ~0.1 mT. The anisotropy measurement utilized the seven-orientation system [Nye, 1957; Borradaile and Stupavsky, 1995], which includes four body-diagonal measurements, improving precision over the traditional orientations confined to coordinate axes and their symmetry planes [e.g., Girdler, 1961]. Instrument control and real-time data processing were performed using the SI2B01 software package. A complete AMS determination and analysis requires less than 4 min per core. AARM was applied with a Sapphire Instruments three-axis, alternating field (AF) demagnetizer with supplementary DC coil to apply a bias field of 0.05 mT while the AF decayed from 60 MT down to zero. The initial or peak AF was 80 or 100 mT. Because of the use of the same seven-axis anisotropy scheme as in the AMS measurements, each ARM application was applied at 45° or 35.3° to the previous one. We have found that this effectively cleans out the ARM acquired in each preceding treatment for many rocks, although we verify this with full

three-axis demagnetization in new measurement campaigns. This tested technique speeds AARM measurement as the specimen does not always need to be completely three-axis cleaned between each ARM application, although it must be demagnetized before the first treatment [Werner and Borradaile, 1996]. The results of each ARM application were determined by measuring the remanence in a JR5a automatic spinner magnetometer (sensitivity 0.03 mA/m). Instrument control, measurement and simultaneous data reductions were performed using the SPIN01 software package. Complete AARM determination and analysis requires 18 min per core. Some specimens were rejected because of low ARM-intensities that yield poor precision for the tensor's determination, and occasionally some specimens are too anisotropic, deflecting remanence from the desired application direction. In these limestones, 30% of specimens were rejected when attempting to determine AARM [Lagroix and Borradaile, 2000b].

### 4. Magnetic Fabrics: Interpretation

[15] Magnetic fabrics, whether of AMS or AARM, are conveniently described by the magnitude ellipsoid of the second-rank anisotropy tensor. It is rarely possible to make a simple interpretation of the magnitudes of the ellipsoid axes as these usually blend contributions from diamagnetic, paramagnetic and ferromagnetic responses from different minerals that may even have different orientation distributions. Geologists now accept that interpretations of magnitudes in terms of a causative process are unduly optimistic, whether the mechanism is magmatic or depositional flow, finite strain, or stress-controlled metamorphic recrystallization [Borradaile and Henry, 1997; Hrouda, 1982; Tarling and Hrouda, 1993]. However, the orientations of the principal susceptibility directions usually do have some kinematic significance.

[16] For reconnaissance interpretations, orientations of the maximum, intermediate and minimum axes of individual specimens are usually presented on stereograms as points or density contours, just as with poles or axes in structural geology (e.g., Figures 4c and 5c). However, such plots may be of limited use. First, the peak concentrations of maximum, of intermediate and of minimum susceptibilities will not usually be orthogonal; the mean tensor of *Jelinek* [1978] is superior here. Second, if multiple subfabrics are present, the sample size may be insufficient to distinguish them and a blend of subfabric orientations may be illustrated. Third, the orientation-distribution represented by density contours ignores the relative importance of different mineral susceptibilities to the fabric, it is in fact a disguised "standardized tensor" distribution.

[17] Statistical characterization of an orientation-distribution of tensors is preferable to inspection of density contours but it is far more complex than for single-axis features such as used in structural geology [Scheidegger, 1965; Woodcock, 1977] because the orientations of the mean principal axes must be orthogonal, just as they are for individual specimens. This problem arises rarely with some traditional field-structural data [e.g., Lisle, 1989] but it is unavoidable where the individual observations are of tensors, leading to some nontrivial considerations in the interpretation of orientation distributions of properties like AMS or AARM [Henry, 1989; Hrouda, 1982; Hrouda and Jelinek, 1999; Hrouda and Schulmann, 1990]. For this purpose, Jelinek [1978] devised a sophisticated statistical approach that permits mean orientations of a sample of specimen tensors to be meaningfully averaged and to determine their confidence cones, subject to some reasonable assumptions that are met here, as in most studies.

[18] Provided the underlying orientation distributions have unimodal concentrations of maximum, of intermediate and of minimum axes, the Jelinek mean tensor will usually provide a more meaningful characterization of the fabric. The 95% confidence cones around the mean axes indicate the symmetry of the orientation distribution, i.e., whether it is an L, L-S or S-tectonite in the terminology of structural geology [Flinn, 1965]. It is important to realize that this is unrelated to the shapes of the individual tensor ellipsoids; instead, they describe the shape of the orientation-distribution ellipsoid. Moreover, and perhaps appearing counterintuitive, the confidence cones need not show orthorhombic symmetry with respect to the mean axes and the "foliation" that contains the mean-maximum and mean-intermediate axes [Borradaile, 2001]. This may provide important clues to the presence of differently oriented subfabrics.

[19] Although it is now realized that the magnitudes and shapes of individual specimen tensors have little kinematic significance due to the complex merging of multiple mineralogical responses, specimen magnitudes do affect the calculation of the orientation of the mean tensor. The mean tensor's orientation may be strongly deflected toward the orientation of a few large-magnitude specimen tensors. However, high susceptibility specimens need not be considered as outliers in the pejorative statistical sense. They may provide useful information from a subfabric or second population of grains with a different orientation-distribution. That is the case in this study where specimens with larger concentrations of paramagnetic accessory clay minerals may strongly influence the orientation of the mean tensor for a subsample. We investigated the influence of such high susceptibility specimens and detected possible kinematically distinct subfabrics by two techniques [Borradaile, 2001]. One approach is to calculate the mean tensor for subsamples that exclude specimens of anomalous susceptibility. A less arbitrary approach is to recalculate the mean tensor using standardized specimen tensors. One may standardize specimen tensors by dividing each of their principal magnitudes (maximum, intermediate, and minimum) by the specimen mean susceptibility; this weights all specimens equally, regardless of their bulk susceptibility. Whereas this is the usual initial approach, it is not mandatory and nonstandardized mean tensors may yield useful information. If a subfabric of higher susceptibility and conflicting orientation is present, its contribution to the entire population of specimens is suppressed by standardization.

[20] Mean tensors are presented for nonstandardized and for the standardized specimen tensors for AMS of the rift basin (Figure 4) and for the faulted margins of the rift (Figure 5), and for AARM (Figure 6). A further complication in the interpretation of the orientation-distribution of AMS arises where some specimens show a net paramagnetic AMS response whereas other specimens in the sample are more strongly influenced by the diamagnetic calcite matrix that produces an inverse fabric.

### 5. Rift Infill

[21] The sediments in the center of the rift valley were sampled as a control group, to avoid the proximity of fault influenced AMS fabrics. They show features compatible with undeformed horizontal sediments and some due to a feeble tectonic strain overprint. Taking the raw AMS specimen tensors, i.e., not standardizing them to unit susceptibility gives a sample weighted by the contribution of orientations of more highly susceptible specimens. Thus, in Figures 4c and 4d the magnetic foliation ( $k_{MAX} - k_{INT}$ ) defines the bedding fabric. Moreover,  $k_{MAX}$ , corresponding to aligned clays, may define a current flow lineation since it is parallel to the rift axis (NW-SE).

[22] Standardizing the specimen tensors emphasizes the contribution from weakly susceptible specimens and thus emphasizes the role of the diamagnetic calcite matrix (Figure 4a); excluding purely diamagnetic specimens switches the roles of  $k_{\rm INT}$  and  $k_{\rm MIN}$  (Figure 4b), a feature commonly recognized from permutations of inverse fabrics and normal fabrics [Rochette et al., 1992]. Clearly, the standardized, "diamagnetic-dominant" fabrics hint at the role of a weak calcite petrofabric that is a compromise between the AMS principal susceptibilities and the principal stress trajectories, superimposed on Figure 4a, which are due to recent seismicity with sinistral transpression along the rift axis. The  $k_{\rm MAX}$  represents an alignment or extensional fabric NNE-SSW, which is compatible with rift genesis.

### 6. Faulted Margins of the Rift

[23] Outcrops along the faulted margins of the Polis rift are more fractured and whereas they show no penetrative petrofabrics their AMS fabrics are different from those of the sediments in the rift's center. This attests to at least a partial tectonic signature in the AMS fabrics. Standardized specimen tensors, whether they include or exclude the purely diamagnetic specimens (Figures 5a and 5b), reveal a shallow plunging NE extension fabric, compatible with rift opening. However, they show some association with the symmetry of the earthquake stress tensors. Nonstandardized specimen tensors emphasize the role of clays and associated fine magnetite, perhaps most sensitive indicators of incremental strains associated with Holocene and Pleistocene seismic activity. These show that the extension, defined by  $k_{MAX}$  is down to the SW (Figure 5c), similarly oriented to the earthquake tensional stresses (Figure 5a).

[24] The AARM technique isolates the contribution of a subfabric of remanence-bearing minerals and it is most successful with magnetite. These limestones are known to carry fine PSD magnetite of volcaniclastic or fossil origin [Borradaile and Lagroix, 2000; Borradaile and Hamilton, 2003], but whereas all our specimens (152) yielded AMS fabrics, only 45 specimens carried sufficient remanencebearing mineral grains to yield well-defined AARM subfabrics. A simple comparison of standardized AMS fabrics and of AARM fabrics (Figures 6a and 6b) indicates that both fabrics are similarly oriented near faults, with their maximum susceptibility NE-SW, in the extension direction expected during rifting with the intermediate axis parallel to the rift axis.

### 7. Conclusions

[25] By processing the AMS data differently and from different subareas, we have identified sedimentary depositional fabrics (Figure 4d) and rift opening fabrics with NE-SW extension (Figures 5a and 5b). AARM subfabrics corroborate the rift-opening event, with their NNE lineation (Figure 6b). Clearly, these petrofabrics developed in <5 Ma with grain alignments that would be much more difficult to discern by any other method. However, nonstandardized AMS fabrics may be modified by the effects of young sinistral transpression producing a blended fabric with magnetic lineation  $(k_{MAX})$  oriented plunging SW, close to the extensional stresses associated with modern earthquakes (Figure 5c). This suggests that some magnetic fabrics are so sensitive that they may be reset in <1 Ma. The symmetry of all magnetic fabrics is generally compatible with the orientations of the actual faults (Figure 6c). Faults belong to two generations (~1 Ma and ~5 Ma); both the AMS and AARM fabrics are most compatible with the Pliocene major rift faults whereas the earthquake stress system is more compatible with the Pleistocene faults and sinistral transpression of the rift system due to E-W compression (Figure 6c).

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## Sub-fabric identification by standardization of AMS: an example of inferred neotectonic structures from Cyprus

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Abstract: Calcite petrofabrics are sensitive to weak strains, possibly being the most sensitive classical petrofabric indicator. Thus, calcareous sediments may reveal stress trajectories in neotectonic environments. Calcite aligns by crystal-plastic deformation and pressure solution produce corresponding alignments in accessory clay minerals and magnetite (possibly fossilbacterial). Their alignments are rapidly and precisely detected by anisotropy of low field magnetic susceptibility (AMS) with net magnetic fabrics, which blend diamagnetic contributions from matrix calcite (diamagnetic bulk susceptibility  $\kappa \sim -14 \,\mu\text{SI}$ ), accessory clay minerals ( $\kappa = 100$  to 500 µSI) and sometimes trace magnetite ( $\kappa > 2$ SI). Their relative abundances and different anisotropies must be considered in interpreting AMS orientations, nevertheless our study reveals orientation distributions of AMS axes in sub-areas and regions that are sensibly interpreted as palaeostress trajectories in Neogene and Quaternary strata. The AMS axes may be correlated with the orientation of faults, plate-motion vectors and seismic solutions. Large samples (1090 specimens from 419 sites) are treated by different statistical approaches ('standardization') to emphasize or suppress the contribution of subfabrics with anomalous mean susceptibility. A sub-sample of 254 specimens from 219 sites, from different sub-areas was investigated by anisotropy of anhysteretic remanence (AARM), which isolates the orientation distributions of magnetite. Magnetic fabrics are mostly of the L-S kind with the magnetic lineations compatible with gravitational stretching of the sedimentary cover away from the Troodos massif and orthogonal to the principal faults and graben. The L-direction  $(k_{max})$  shows a smooth variation in orientation, through the sub-areas, directed radially from the Troodos massif and the S-components of the magnetic fabrics are inclined gently to the bedding, compatible with vergence toward the Cyprean Arc to the S and SW of Cyprus.

Magnetic fabric analysis, most commonly using anisotropy of low-field magnetic susceptibility (AMS). is now well established as a non-destructive technique to isolate the mean orientationdistribution of crystals in an anisotropic rock. AMS blends contributions from different minerals that have different magnetic responses, i.e. paramagnetic, diamagnetic or 'ferro'magnetic (Rochette et al. 1992). In turn, the principal AMS axes may proxy for the principal axes of the orientation distribution ellipsoid of crystals (Henry 1989; Borradaile 2001) which, in turn, may reveal the finite strain axes in tectonically deformed rock (Tarling & Hrouda 1993: Borradaile & Henry 1997). In deformed calcite matrices, interpretation is somewhat complicated by an intrinsic counterintuitive arrangement of crystallographic and AMS axes, a socalled 'inverse fabric' (Rochette 1988). which nevertheless still permits sensible interpretations of their finite strain axes (Ihmlé et al. 1989; de Wall et al. 2000).

However, recent studies show that in neotectonic environments, with imperceptible penetrative strain. AMS axial orientations may be sensibly related to the orientations of joints or faults, for which stress axes are reliably inferred (Sagnotti et al. 1994, 1998; Mattei et al. 1999; Cifelli et al. 2004). In some instances, AMS axes may correlate with modern seismic solutions and plate movements (Kissel et al. 1986; Mattei et al. 1999; Borradaile & Hamilton 2004). Thus, AMS may proxy for stress trajectories under limited circumstances.

Our goal is to examine a large sample of AMS and AARM data from post-Palaeogene strata in Cyprus that correlate with the orientations of neotectonic structures or events (faults, rifts. Tertiary uplift). It will be shown that their orientations are consistent with stress trajectories inferred from those structures and recent plate motion trajectories. Sampling at two density levels verifies the homogeneity of the regional domains and the validity of the regional conclusions. Local

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sub-areas (I–VI) were structurally homogenous and sampled with as little lithological variation as possible over areas  $\leq 30 \, \mathrm{km}^2$ . The regional-scale domains (I–V) have an average area of  $\sim 400 \, \mathrm{km}^2$ .

### **Tectonic background**

Our study concentrates on the limestone and marl sedimentary cover to the Cretaceous Troodos ophiolite. We exclude from this discussion the juxtaposed older allochthonous Mamonia and Kyrenia terranes, which include exotic formations as old as Triassic and perhaps even Carboniferous (Robertson 1990) (Fig. 1a). The Troodos terrane exposes an integral ophiolite sequence with mantle harzburgite and lherzolite at the base overlain by layered gabbros and dunite, sheeted dykes, a transitional sheeted-dyke to pillowed unit and a thick pillow basalt sequence (Malpas et al. 1990). Supra-Troodos sedimentation commenced in the Maastrichtian (~68 Ma) with a pelagic chalk blanket, to form a relatively continuous sequence to the present (Lord et al. 2000). Northwards subduction stalled in the Eocene, with southward thrusting of the Kyrenia Range. Subduction then retreated southwards to its present location off the south shore of Cyprus in the Miocene, initiating the present stress regime (Fig. 1b). Miocene extensional basins, most prominently the Polis graben, formed in response to changing stress trajectories during the retreat of the subduction zone's hinge away from the Troodos microplate. Subduction continued during the Pliocene, until the Eratosthenes Seamount reached the trench in the Pleistocene when serpentitization-driven diapirism continued to uplift the Troodos dome (Robertson 2000). These events drastically changed the neotectonic regime in the last 5 Ma, which is evident from studies of structure (Robertson et al. 1995), earthquakes (Ben-Avraham et al. 1988; Arvidsson et al. 1998; Papazachos & Papaioannou 1999; Borradaile & Hamilton 2004) and global plate motion (Reilinger et al. 1997). The tectonic events, their principal plategeometrical consequences and the reasonably inferred principal tensile or compressive stress trajectories are summarized in Figure 2.

Our previous studies indicated the potential for AMS (anisotropy of low field magnetic susceptibility) to indicate very weak strains and weak orientation distributions of minerals. like those accompanying calcite-crystal plastic mechanisms in neotectonic environments. AMS shows neotectonic potential in the limestone cover from the Palaeogene Lefkara Formation through the Neogene Pakhna Formation to the

localized Pleistocene cover. Without regard to detailed stratigraphic level within the Troodos Cover sequence, Lagroix and Borradaile (2000) showed that the AMS principal axes correspond to kinematic patterns.  $k_{max}$  defines down-slope gravitational stretching away from the Troodos dome and locally into tectonic/depositional basins. In the Polis Rift Valley, AMS and AARM (anisotropy of anhysteretic remanent magnetization) axes correlate with principal stress trajectories inferred from Miocene and younger fault-orientations and by modern seismic fault-plane solutions (Borradaile & Hamilton 2004, Fig. 6).

## Neotectonic interpretation potential of AMS?

The presence of consistently oriented AMS axes in young sedimentary rocks that are not related to depositional fabrics, itself argues for some subtle tectonic imprint (e.g. Sagnotti et al. 1994). In such environments, AMS axes may be oriented consistently and simply with respect to faults or joints. These structures have orientations uniquely associated with their cogentic stress trajectories and thus by induction, the AMS axes may proxy as stress trajectories. Of course, AMS axes may proxy for stress trajectories in ancient rocks too, but their recognition requires fortunate circumstances (e.g. Borradaile & Kehlenbeck 1996). Usually, in ancient or severely deformed rocks, the association of AMS with finite strain axes with earlier tectonic events will mask any young and feeble AMS overprint associated with late stress increments. Note that we use Flinn's L-S scheme (1965) equally to describe tensor magnitude ellipsoid shapes, whether they are for strain, AMS, stress or mineral ODs (petrofabrics).

Calcite twinning and other crystal-plastic deformation have long been used in petrofabrics as sensitive indicators of incremental strain axes, which are essentially parallel to the causative palaeostress axes. Indeed, the association of calcite petrofabrics, their causative stress axial orientations and magnetic fabrics have been shown in some other studies (Owens & Bamford 1976; Owens & Rutter 1978; Jackson et al. 1989; Borradaile et al. 1989). The Neogene and Quaternary limestone and marl that covers the Troodos microplate shows evidence of weak to moderate strain, expressed by calcite twinning and, rarely, a feeble stylolitic cleavage. Calcite, accessory clay and magnetite traces are aligned and readily detectable in the AMS signal (Lagroix & Borradaile 2000). These minerals



Fig. 1. Geology of Cyprus. (a) Major lithological units of Cyprus (Geological Survey Department, Cyprus, 1979). (b) Major Tectonic features of Cyprus (Robertson 1990; Arvidsson *et al.* 1998; Borradaile & Hamilton 2004).

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Fig. 2. Simplified stratigraphic and tectonic events for the Troodos terrane. and its sedimentary cover rocks.

contribute quite differently to AMS and to bulk susceptibility. Calcite is diamagnetic (usually quoted as  $\kappa \sim -14 \,\mu\text{SI}$ ) but it has a large anisotropy and comprises >97% of the rocks' volumes. Its crystal-plastic deformation aligns the paramagnetic accessory clay minerals (100-500  $\mu$ SI,  $\leq$ 3% by rock volume) and the scarce traces of magnetite. However, the latter may contribute significantly to AMS due to magnetite's high bulk susceptibility (~1.0-2.7 SI) (Hunt et al. 1995); and the grains may align either as overgrowths or inclusions associated with clay grains or as independent grains. Magnetite grains may be of clastic or bacterial origins; their hysteresis properties are compatible with the latter hypothesis (Borradaile & Lagroix 2000; Borradaile & Hamilton 2003).

The specimen's bulk susceptibilities  $(\kappa = \sqrt[3]{(k_{max}k_{im}k_{min})})$  are a first guide to the mineralogical controls on AMS. We present these for rather homogenous sub-areas (Fig. 3a), which justifies the subsequent interpretation of larger sampling schemes in regional domains (I-V) (Fig. 3b). The positive susceptibility sections of the histograms are scaled logarithmically and, to a first approximation, it appears that the weakly positive  $\kappa$  specimens have susceptibilities with a lognormal distribution, with most sub-areas and regional domains having modal  $\kappa$  in

the range  $+15 \mu SI \le \kappa \le +35 \mu SI$ . Only very low concentrations of accessory clay ( $\leq 1000 \,\mu$ SI) and trace magnetite ( $\sim 2.0$  SI) are required to raise the specimens'  $\kappa$  from the level of a pure calcite diamagnetic matrix (assumed to be  $\sim -14\,\mu\text{SI}$ ) to the levels of the positive  $\kappa$  specimens shown in Figure 3a, b. In the complete absence of magnetite, only 3% by volume of clay would be required to justify the positive  $\kappa$ values. Many specimens are truly diamagnetic and the linear scale for the diamagnetic part of the histogram clarifies the frequency distributions. For calcite  $\kappa$  is commonly quoted at  $\sim -14 \mu SI$ (Voight & Kinoshita 1907) or -7.5 to  $-39 \mu$ SI. (Hunt et al. 1995). Whereas there are fairly modern high precision torque measurements for anisotropy (i.e.  $k_{max} - k_{min}$ ; Hellwege & Hellwege 1967; Owens & Rutter 1978) there are apparently no recent high-precision measurements for the bulk value ( $\kappa$ ), which hinders modelling and interpretation of AMS. Values for synthetic calcite would be preferable for modelling work (e.g. in Borradaile 1988) whereas measurements from natural calcite are contaminated by non-diamagnetic impurities. Our instrument has a low-drift environment ( $<0.05 \mu$ SI) and is calibrated with  $MnO_2$  (~1654 µSI). Due to the small range of diamagnetic susceptibilities there may be some slight bin boundary bias in that part of the histogram.



Fig. 3. Frequency distribution of bulk magnetic susceptibility ( $\kappa$ ) for (a) sub-areas (~30 km<sup>2</sup>) and (b) regional domains (~400 km<sup>2</sup>). Data in the shaded box on the left represent diamagnetic specimens and their scale is linear. Data with  $\kappa > 0$  represent paramagnetic specimens and are shown with a logarithmic scale.

The susceptibility frequency-distribution indicates that paramagnetic limestone is more common and it confirms that the rocks' susceptibilities, whether paramagnetic or diamagnetic are mostly bimineralic in origin. Interpreting AMS axes in such rocks necessitates the evaluation of the competition between weak paramagnetism and weak diamagnetism in the same specimens, and between weakly dia/paramagnetic specimens within a sample of several different specimens, for example from a sub-area. A new plot of fabric anisotropy parameters, introduced by Borradaile & Jackson (this volume), simplifies the interpretation in this context. Jelinek's (1981) anisotropy parameters  $(P_j, T)$  are usually presented on Cartesian axes. Consequently, for weak degree of anisotropy (low-eccentricity ellipsoids with  $P_j \sim 1.0$ ) the difference between T-values that describe ellipsoid shape is exaggerated. In the extreme case, the sphere (isotropic case,  $P_j = 1.0$ ), which should plot at *onc point* on the diagram actually spread along the entire axis from T = +1(prolate) to T = -1 (oblate). This biases the presentation and interpretation of all low- $P_j$  anisotropies that are essentially near-isotropic, a matter of considerable relevance here where specimens straddle the diamagnetic-paramagnetic boundary. The new polar plot presents  $P_j$ radially and T along arcs; thus, all spheres plot uniquely at the origin and the difference in shape between weak anisotropies is not exaggerated. Moreover, the plot facilitates the simultaneous presentation and comparison of positive and diamagnetic susceptibilities (Fig. 4). When working with anisotropies of diamagnetic rocks and weakly paramagnetic rocks it is also important not to overlook some non-trivial issues that



Fig. 4. Polar plots (see Borradaile & Jackson, this volume) of four select sub-areas (a)-(d) and two select regional domains (e, f). Shaded area represents diamagnetic specimens and white area represents paramagnetic specimens.

software must manage carefully:

- (1) Anisotropy is indeterminate for a specimen if some axes have positive susceptibility and others have negative susceptibility (Borradaile 2003). This occurs in some limestone specimens.
- (2)  $k_{\text{max}}$  is obviously the largest absolute value for a paramagnetic material but for a diamagnetic material the most negative value represents the long axis of the magnitude ellipsoid.
- (3) Regardless of the convention for defining the ellipsoid in (2) above, the common diamagnetic minerals, quartz and calcite have the idiosyncrasy that under most metamorphic conditions their c axes tend to align parallel to the shortening axis (but see Borradaile & Jackson, this volume). Thus, c axes are parallel to the most negative susceptibility, which may be perpendicular to the rock's S-fabric. Calcite exhibits a strong prolate diamagnetic anisotropy with  $(k_{max} - k_{min})$ estimated at 1.39 µSI (Krishnan et al. 1933; Hellwege & Hellwege 1967, p. 143) or  $1.172 \pm 0.028 \,\mu$ SI (Owens & Rutter 1978). If we accept the much less certain but commonly quoted bulk susceptibility  $\kappa \sim -14 \,\mu$ SI. these precise anisotropy determinations indicate a large anisotropy of ~10%.
- (4) Since most deformation mechanisms align calcite with its c axis (most negative susceptibility) parallel to shortening it produces an 'inverse fabric' (Rochette 1988; Ihmlé et al. 1989).

Examples of the anisotropies of both local-scale samples (Fig. 4a-d) and regional domains (Fig. 4e, f) indicate that the anisotropy degree  $(P_i)$  is similar for diamagnetic and paramagnetic limestones and that ellipsoid shape tends slightly toward the oblate case (T > 0) for both diamagnetic and paramagnetic specimens. Anisotropies are remarkably similar for the diamagnetic and paramagnetic fields and diamagnetic limestones are only absent in marl Formations in the Omodhos and Lefkara sub-areas (Fig. 4c, d).

#### Interpreting AMS

AMS orientations and magnitudes would reflect the orientation distribution of a monomineralic rock with a unique petrofabric. However, for rocks with multiple minerals with similar contributions to the net susceptibility or with multiple subfabrics some care is required in evaluating the influence of mineral abundances and subfabrics (Borradaile 1988; Borradaile & Henry 1997). For rocks of high mean susceptibility ( $\kappa$ ), AMS axes may be controlled by one or two or a few minerals (Henry 1983, 1990, 1992; Borradaile et al. 1986; Borradaile & Kehlenbeck 1996; Borradaile & Lagroix 2001; Nakamura & Borradaile 2001). In our limestones however, sub-equal competition from the diamagnetic matrix and paramagnetic clay complicate the issue. To illustrate the argument with hypothetical but not unrealistic values chosen for arithmetic simplicity, disperse a concentration of 5% clay (assume  $\kappa = 266 \,\mu\text{SI}$ ) in a calcite matrix (assume  $\kappa = -14 \,\mu\text{SI}$ ). The limestone's net susceptibility is approximately zero and the specimen may also be isotropic. It is for this reason that some AMS data from limestone must be examined carefully because the AMS directions are simply too unstable; their anisotropy is too low to define stable orientations of principal axes as itemized in the list above (Borradaile & Jackson, this volume). In worse cases, the principal susceptibilities may not all be of the same sign so that the AMS tensor may not be represented by any magnitude ellipsoid.

Although it is now realized that the magnitude ellipsoids of individual specimen tensors have little kinematic significance due to the complex blend of multiple mineralogical responses, specimen magnitudes do affect the calculation of the orientation of the mean tensor. The mean tensor's orientation may be strongly deflected toward the orientation of a few large-magnitude specimen tensors. However, high susceptibility specimens need not be considered as outliers in the disparaging statistical sense. They may provide useful information from a subfabric or second population of grains with a different orientation distribution. That is the case in this study where specimens with larger concentrations of paramagnetic accessory clay minerals may strongly influence the orientation of the mean tensor for a sub-sample. By recalculating the mean tensor using standardized specimen tensors, the influence of high susceptibility specimens and kinematically distinct subfabrics may be isolated, or emphasized (Borradaile 2001, 2003). Specimen tensors are standardized by dividing each of the principal magnitudes for a specimen  $(k_{\text{max}}, k_{\text{int}}, k_{\text{min}})$  by  $\kappa$ ; this weights all specimens equally, regardless of their bulk susceptibility. Consequently the contribution high- $\kappa$  subfabrics to the orientation distribution will be subdued in the net-AMS. On the other hand, the mean tensor for non-standardized specimens emphasizes the role of such subfabrics (Borradaile 2001, 2003).



Fig. 5. Idealized symmetry of confidence cones about the mean orientations of the principal axes of the mean tensor for a petrofabrically homogeneous group of specimens. The shapes of confidence cones for tensor-mean principal axes may be used for other petrofabrically significant axes (as in orientation distributions of crystals), for finite strain axes and for principal stresses. The shape of the confidence cones may also be related to the relative magnitudes of the three principal mean axes: (a) elongate confidence ellipses in the maximum-intermediate plane define an ellipsoid with oblate symmetry (S > L) whereas (c) elongate confidence ellipses in the plane perpendicular to the maximum axis are associated with prolate symmetry (L > S). Flinn's (1965) L-S notation was initially introduced to describe finite strain ellipsoids or fabric ellipsoids but it is a useful shorthand for any anisotropy.

The following comparison of mean tensors for standardized versus non-standardized specimens in regional-scale and local-scale samples, display different AMS axes that reveal a rapidly changing tectonic regime, especially in the last 5 Ma. Sample mean tensors for standardized and non-standardized specimens are also compared profitably to previously determined AARM tensors.

### Processing AMS data from low- $\kappa$ specimens

The tectonic significance of AMS data in limestone having weak susceptibilities depends on a careful assessment of the mineralogical origins of AMS and the effects of specimen variation within the sample suite. Jelinek (1978) showed that the orientation distribution (OD) of a suite of tensors ('AMS ellipsoids') must be treated by a special statistical procedure so that the sample's mean tensor retains orthogonal axes, just like individual specimen tensors. Applying Jelínek statistics permits us to characterize a sample of AMS tensors much more effectively than with density contours, although the latter still have their use (Borradaile 2001, 2003). The shape and symmetry of the 95% confidence regions around the mean tensor's principal axes define the orientation distribution of specimen tensors in the L-S fabric scheme (Flinn 1965): thus regional suites of AMS ellipsoids define the regional variation from S through L tectonites (Fig. 5).

Confidence cones for the mean tensor's principal axes reflect the shape of the orientationdistribution (OD) ellipsoid for the sample, not of individual tensors. For example, individual prolate ellipsoids scattered with their long axes in a plane define a sample with an orientation distribution described by an oblate ellipsoid (e.g. Borradaile 2003. pp. 286–287). Thus in AMS studies, if the mean  $T_j > 0$  for specimens. it does not necessarily mean that their orientation distribution, described by the mean tensor, is also oblate (Borradaile 2001).

The sample's mean tensor and its confidence cones may be biased toward the orientation of specimens of anomalous  $\kappa$ . In this study, the anomalous specimen may be a diamagnetic one or a paramagnetic one in a contrasting matrix. The standardization technique described (dividing  $k_{max}$  etc.) suppresses this bias. Whereas it may change the orientation of the mean tensor, it may also change the shape of the confidence regions about the mean tensor's axes. Thus one may re-evaluate the OD of the mean tensor as an L > S rather than S > L fabric.

#### **AMS measurements**

AMS was determined using a Sapphire Instruments SI2B device operating at 19200 Hz and
$\sim 0.1$  mT. The anisotropy measurement utilized the seven-orientation system (Borradaile & Stupavsky 1995), which includes four body-diagonal measurements, improving precision over the more commonly used orientations confined to coordinate axes and their symmetry planes (e.g. Girdler 1961). Instrument control and real-time data processing were performed using the SI2B01 software package developed by G. J. Borradaile. A complete AMS determination and analysis requires less than four minutes per core. The low-field AMS was determined on 360 cores from 121 specimens of the local sampling campaign and 730 cores from 298 specimens of the regional sampling campaign of Lagroix and Borradaile (2000).

# AARM: Anisotropy of anhysteretic remanent magnetization

AARM was determined using the same seven-axis anisotropy scheme as for AMS measurements. The specimen is fully demagnetized and then the seven differently oriented ARMs are applied and measured, in a sequence such that each ARM is inclined at 45° or 35.3° to the previous one. For many rock types, this effectively cleans the ARM acquired in each preceding treatment. This tested technique greatly reduces the measurement time because 3-axis AF cleaning between each ARM application is no longer necessary (Werner & Borradaile 1996). However, the success of this short-cut must be verified with each new measurement campaign and each new lithology. ARMs were imposed with a Sapphire Instruments three-axis Alternating Field (AF) demagnetizer outfitted with a supplementary d.c. coil applying a bias field of 0.05 mT. The AF decayed from a peak field of 80 or 100 mT to zero while the d.c. bias field was turned on from 60 mT to zero. The imposed ARM was measured in a JR5a automatic spinner magnetometer (sensitivity 0.03 mA/m). Instrument control. measurement and simultaneous data-reductions were performed using the SPIN01 software package developed by G. J. Borradaile. Complete AARM determination and analysis requires 18 minutes per core. We have only included AARM results from regional-scale sampling suite in this study. Of the original sample (n = 1170). Lagroix & Borradaile 2000). 201 cores were rejected for AARM determination. The criteria for accepting or rejecting the AARM results occur during measurement; results were rejected if intensities were <1 mA/m when measured in orientation 1 of the AARM scheme or if the AMS ellipsoid for the sample had a negative  $\kappa$ . In the present

study. for AARM we selected 254 cores from 229 specimens from the original suite published by Lagroix and Borradaile (2000).

### Sampling strategy

The first level of sampling focused on structurally and lithologically homogenous sub-areas  $\leq 30 \text{ km}^2$  that were densely sampled (Fig. 6). They include the Polis Rift Margins, Polis Basin, Galataria, Omodhos-Pakhna, Lefkara and Lymbia, designated sub-areas I-VI, respectively, yielding n = 360 cores from N = 121sites. These areas include formations from the Lefkara up to the Athalassa Formation. The homogeneity of fabrics in these sub-areas justified the larger scale interpretation from the next level of sampling.

The second level of sampling was a diluted regional-scale campaign. The limestone specimens covered a wide age-range of the sedimentary cover, from the Lefkara Formation up to the Nicosia Formation (Lagroix & Borradaile 2000). Of the original sample suite (cores n = 1170, sites N = 434), a sub-sample (n = 730, N = 298) was analysed in five regional domains of similar tectonic style and trend (Fig. 7), each with an area of ~400 km<sup>2</sup>.

All hand specimens were oriented in the field and three to six cores (25 mm in diameter and 22 mm high) were drilled in the laboratory from each specimen, restored to geographic coordinates.

# Localized sampling: Polis Rift Region (sub-areas I, II, III)

Non-standardized AMS in this, the Polis Rift region, differs from the other areas (Fig. 6a). From the faulted margins they exhibit an S > Lfabric as shown by the elongate confidence cones for  $k_{max}$  and  $k_{int}$ , and a small  $k_{min}$  confidence cone (Fig. 6a, sub-area I). The AMS axes are symmetrically compatible with stress directions of the last 5 Ma verified from fault orientations and from seismic data (Payne & Robertson 2000; Borradaile & Hamilton 2004).

In the basin, non-standardized data permit straightforward fabric interpretations (Fig. 6a, sub-area II). These younger strata have S > Ldepositional fabric as shown by the elongate confidence cones for  $k_{max}$  and  $k_{int}$  in the foliation and a tight, near-vertical  $k_{min}$  confidence cone. The magnetic foliation is parallel to the bedding.  $k_{max}$  and  $k_{int}$  lie within the bedding plane and  $k_{max}$  is possibly a flow-alignment, since it is

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Fig. 6. Sub-areas of Cyprus (I–VI) and their magnetic fabrics as discriminated by standardization (specimen tensors standardized dividing by each specimen's  $\kappa$ ). (a) Non-standardized AMS orientation distributions are biased by anomalously oriented subfabrics, especially with anomalously high- $\kappa$ . (b) Standardized AMS fabrics usually suppress the contribution of specimens with anomalous orientations.

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Fig. 7. Regional domains of Cyprus (1-V) and their magnetic fabrics. (a) Non-standardized AMS. (b) Standardized AMS. (c) Standardized AARM. AARM isolates the magnetite subfabric and when standardized, the contribution of anomalously oriented specimens is subdued.

parallel to the rift axis (cf. Sagnotti et al. 1994). Raw, non-standardized AMS data demonstrates the effects of higher susceptibility specimens in which depositional-controlled AMS fabrics dominate.

In the Galataria region, non-standardized specimens exhibit an  $L \approx S$  fabric, which appears nearly isotropic from its large, overlapping confidence cones (Fig. 6a, sub-area III). Nevertheless, the mean tensor axes are similar to the other two preceding localities in this region.

How are these low- $\kappa$  samples affected by relatively high- $\kappa$  specimens? Standardizing the specimen AMS to  $\kappa$  reveals similar susceptibility directions overall but demonstrate progressively different confidence cone shapes (Fig. 6b, subareas I-III). All show  $L \gg S$  ODs. The progressive increase in size of the confidence cones from west to east may be due to the smaller sample sizes (n = 152 to n = 25). The NEtrending  $k_{max}L \gg S$  fabric agrees with the crustal tension axis required for the paired normal faults defining the Polis Graben and the normal fault zone defining the Pegia fault system (Payne & Robertson 2000). The  $L \gg S$ fabric of the AMS data are also symmetrically compatible with the current tectonic stress regime deduced from earthquake data (Borradaile & Hamilton 2004, Fig. 2).

## Localized sampling: Southern slopes of Troodos (sub-areas IV, V, VI)

The three easternmost detailed sub-areas show little difference between standardized and nonstandardized samples (Fig. 6, sub-areas IV-VI). The Omodhos-Pakhna sub-area (IV) displays an  $L \approx S$  OD fabric with a shallow northward dipping 'foliation'. The Lefkara and Lymbia (sub-areas V and VI) localities display an S > LOD fabric as shown by the elongate confidence cones  $k_{\max}$  and  $k_{int}$  and a tight  $\bar{k}_{\min}$  confidence cone with a shallow NNE dipping foliation. These OD fabrics in the eastern localities represent a dominant sedimentary fabric with some secondary tectonic control. However, all are compatible with a south-directed movement (southerly vergence) within the limestone cover.

## **Regional-scale AMS**

Non-standardized AMS data of the five regionalscale domains (Fig. 7a, sub-areas I–V) exhibit similar ODs for all areas. All five groups exhibit an  $S \gg L$  fabric as shown by the elongate confidence cones for  $k_{max}$  and  $k_{int}$  and a tight  $k_{min}$  confidence cone near vertical (Borradaile 2001). This OD is similar to the results exhibited in the density-contoured data in Lagroix and Borradaile (2000). The S-component of the fabric is bedding controlled and  $k_{max}$  is kinematically compatible with N–S extension, parallel to the aligned phyllosilicates caused by the stretching of the sedimentary cover (Lagroix & Borradaile 2000).

But how are these low susceptibility samples affected by relatively high susceptibility samples that may be considered as statistical outliers? Standardizing the specimen ellipsoids to  $\kappa$ . AMS data of the five regional-scale groups (Fig. 7b) reveals similar overall AMS axes but different confidence-cone shapes and, thus, different fabric ODs in the *L*-S range. These differences change progressively from  $L \approx S$  in the east to

L > S in the west. This corresponds to the increasing tectonic strain from east to west, inferred from earthquake data (Ben-Avraham *et al.* 1988; Arvidsson *et al.* 1998; Papazachos & Papaioannou 1999; Borradaile & Hamilton 2004) and overall structural trends (Robertson 2000; Borradaile & Hamilton 2004). In contrast, raw data (non-standardized) are weighted by higher susceptibility depositional subfabrics rather than the weak tectonic ones compatible with supra-subduction SW-directed shortening (Lagroix & Borradaile 2000).

### **Regional scale AARM**

Only standardized data are presented for AARM to avoid the spurious effects due to the large variance in remanence intensity. Domains I, II & V (Fig. 7c) show similar overall AARM axes to standardized AMS (Fig. 7b). This verifies the important contribution of magnetite to some AMS fabrics. They show an  $L \approx S$  OD similar to the easternmost standardized AMS, perhaps due to a near-uniaxial shape of magnetite, which when arranged in a weak planar fabric has a strong Amin zone-axis girdle. Thus, the N-S extensional trend (seen in the AMS) is less effectively expressed but the fabric axes are kinematically compatible with movement directed toward the SW (or subduction to the NE). AARM fabrics for the other two sub-areas (Fig. 7c, sub-areas III & IV) exhibit  $S \gg L$  fabrics; AARM axes indicate a more southerly directed movement. The AARM fabric may be a composite of the stylolitic cleavage incompletely overprinting the bedding fabric (Lagroix & Borradaile 2000).

#### Conclusions

- Low-κ rocks such as limestone commonly show unstable AMS axes due to sub-equal competition from subfabrics of diamagnetic calcite and paramagnetic clays, with traces of magnetite. These subfabrics commonly represent weak tectonic overprints on depositional fabrics, as in the limestone cover of the Troodos terrane.
- Standardizing AMS principal values of specimens to their  $\kappa$  equalizes the contributions of subfabrics/specimens with different  $\kappa$  in the overall sample mean tensor. Thus, one subfabric may be emphasized or neutralized. This has a similar effect to determining a PSD magnetite subfabric with AARM (Lagroix & Borradaile 2000), although it is not a satisfactory substitute for AARM.

- Applying this methodology to the limestone cover of Troodos, standardized and nonstandardized AMS reveal depositional fabrics, neotectonic fabrics associated with NNE subduction, neotectonic fabrics associated with rifting and composite fabrics from feeble stylolitic foliation imprints on bedding.
- Standardizing AMS data for petrofabrically homogenous sub-areas or domains reveals fabrics compatible with neotectonic stress trajectories in post-Paleogene strata. This is well shown in the Polis basin (<5 Ma) and the Galataria sub-area (43-62 Ma) (Figure 6b, sub-areas II and III respectively), which show nearly identical fabrics in rocks with 40 million years age difference, but relatively little geographic difference.
- Examination of AMS tensors for sub-areas, and even larger regions may reveal tectonically significant axes, related to stress rather than finite strain. The orientation distribution of the mean tensor has an ellipsoid shape that may reveal the relative magnitudes of the principal stresses.

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